Connacher Performance Presentation - 2019





Forward Looking Information and Advisories



This Presentation contains forward looking information including, expectations for future production and total bitumen recovery, estimates of reserves, future development of the **SAGD+®** process commercial project at Algar and mini-steam expansion at Pod One and the anticipated impact thereof, growth potential associated with certain additional capital investment options and development projects to be undertaken at Algar, sustainability of production, well and plant performance, the steam to oil ratio ("SOR"), and plant reliability.

Forward looking information is based on management's expectations regarding the Company's future growth and financial position; results of operations and production, future commodity prices and foreign exchange rates; future capital and other expenditures (including the amount, nature, and sources of funding thereof), plans for and results of drilling activity; environmental matters; business prospects and opportunities; and future economic conditions. Forward looking information involves significant known and unknown risks and uncertainties, which could cause actual results to differ materially from those anticipated. These risks include, but are not limited to: the risks associated with the oil and gas industry (e.g., operational risks in development, exploration and production; delays or changes in plans with respect to exploration or development projects or capital expenditures; the uncertainty of reserve and resource estimates; the uncertainty of geological interpretations; the uncertainty of estimates and projections relating to production, costs and expenses; and health, safety and environmental risks), risk of commodity price and foreign exchange rate fluctuations, risks associated with the impact of general economic conditions, risks and uncertainties associated with maintaining the necessary regulatory approvals and securing the financing to proceed with the operation and continued expansion of the Great Divide oil sands project.

This presentation includes information pertaining to the reserves as at December 31, 2016, as evaluated by GLJ Petroleum Consultants Ltd., in their report for the year ended December 31, 2016 (the "GLJ Report"). Statements relating to reserves are deemed to be forward looking statements, as they involve the implied assessment, based on certain estimates and assumptions, that the reserves described exist in the quantities predicted or estimated, and can be profitably produced in the future. Certain information and assumptions relating to the reserves reported herein are set out in the Corporation's Statement of Reserves Data and Other Oil and Gas Information for the year ended December 31, 2016, which is available on the System for Electronic Document Analysis and Retrieval (SEDAR) at www.sedar.com. There is no assurance that the forecast price and cost assumptions contained in the GLJ Report will be attained and variances could be material. The reserves estimates of Connacher's properties described herein are estimates only. The actual reserves on Connacher's properties may be greater or less than those calculated.

Design capacity is not necessarily indicative of the stabilized production levels or steam generation capacity that may ultimately be achieved at Connacher's SAGD project sites. Reported average production levels may not be reflective of sustainable production rates and future production rates may differ materially from the production rates reflected in this presentation due to, among other factors, difficulties or interruptions encountered during the production of bitumen.

Although Connacher believes that the expectations in such forward looking information are reasonable, there can be no assurance that such expectations shall prove to be correct. The forward looking information included in this presentation is expressly qualified in its entirety by this cautionary statement. The forward looking information included herein is made as of the date of this presentation and Connacher assumes no obligation to update or revise any forward looking information to reflect new events or circumstances, except as required by law.

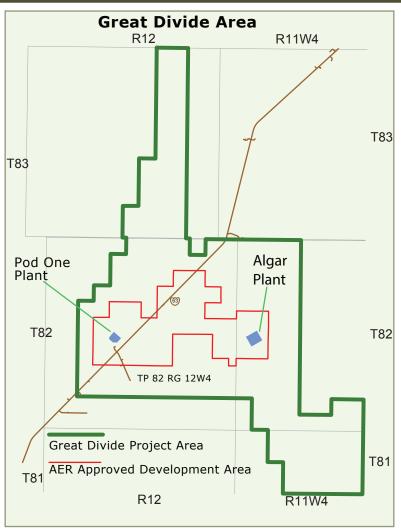


Subsurface - Background

Assets



- Connacher is a focused developer, producer, and bitumen marketer from its in-situ oil sands projects in Alberta's Athabasca oil sands.
- Primary driver of value is the continued development of its bitumen production at its Great Divide oil sands operations using in-situ recovery methods
- Oil sands reserves and resources include 443,996 Mbbl of 2P reserves (as of 31 December 2018 per GLJ Petroleum Consultants) (1)



⁽¹⁾ See Slide AppendixB for Reserve Definitions

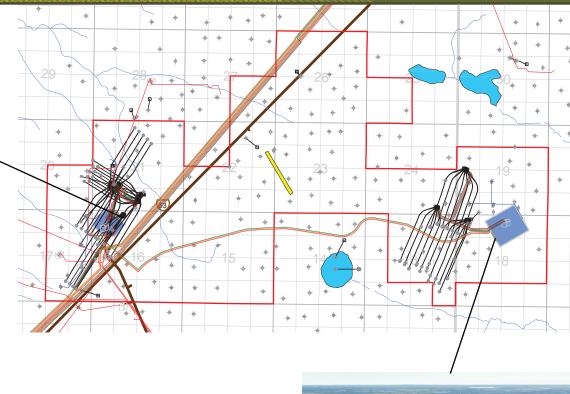
Great Divide Assets





Pod One

- First Steam September 2007
- First Bitumen October 2007



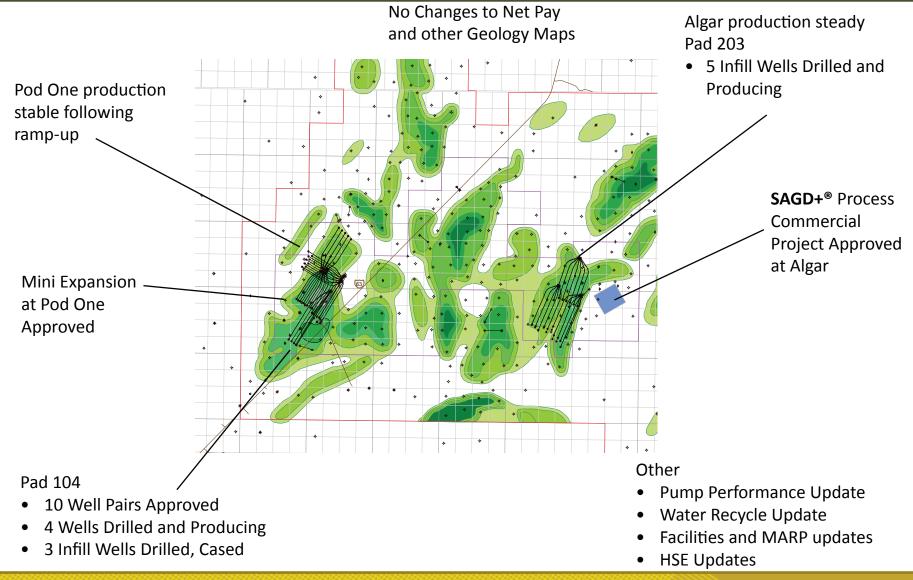
Algar

- First Steam May 2010
- First Bitumen July 2010



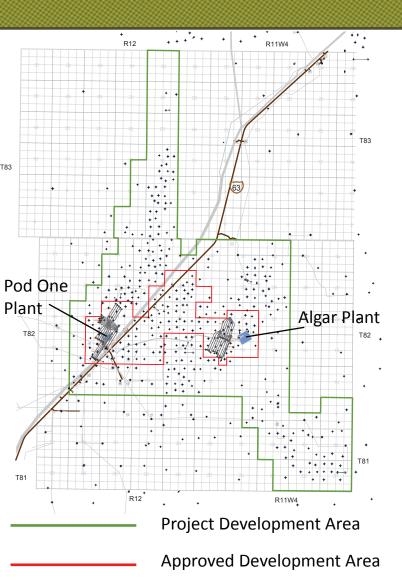
Highlights - 2019 Connacher Presentation





Great Divide (Approval 10587) Development





Pod One Current Development

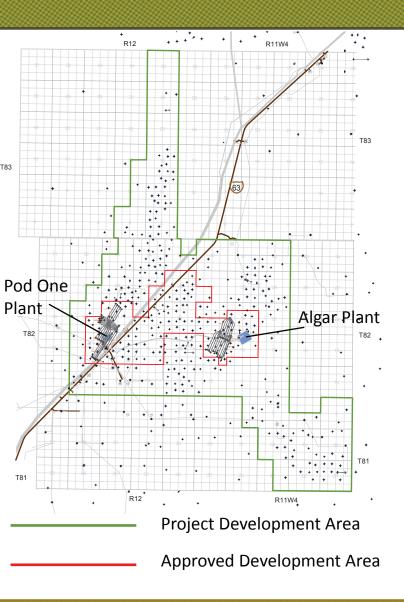
- 23 Well Pairs and 16 Infills
 - Pad 101N 5 Well Pairs
 - Pad 101S 6 Well Pairs, 6 Infills
 - Pad 102W 5 Well Pairs, 5 Infills
 - Pad 102S 3 Well Pairs, 2 Infills
 - Pad 104 4 Well Pairs 80m interwell spacing, 3 Infills

Pod One Development History

- Original 15 Well Pairs Drilled in 2007
- All well pair interwell spacing 100m except Pad 104
- 2 Well Pairs Drilled in 2009 (101S and 102S)
- 2 Well Pairs Drilled in 2010 (102S)
- 4 Infills Drilled in 2013 (102W)
- 4 Well Pairs Drilled in 2013 (104)
- 9 Infills Drilled in 2014 (102W(1), 102S(2), 101S(6))
- 3 Infills Drilled in 2019 (104)

Great Divide (Approval 10587) Development





Algar Current Development

- 18 Well Pairs Producing, 5 Infills
 - Pad 201S 5 Well Pairs 100m interwell spacing
 - Pad 202S 6 Well Pairs (1 re-drill) 100m interwell spacing
 - Pad 203S 7 Well Pairs 100m interwell spacing,
 5 Infills

Algar Development History

- Original 17 Well Pairs Drilled in 2009
- Replacement Well Pair (202-01) drilled in 2013
- 5 Infills Drilled in 2019 (203S)

Great Divide Summary



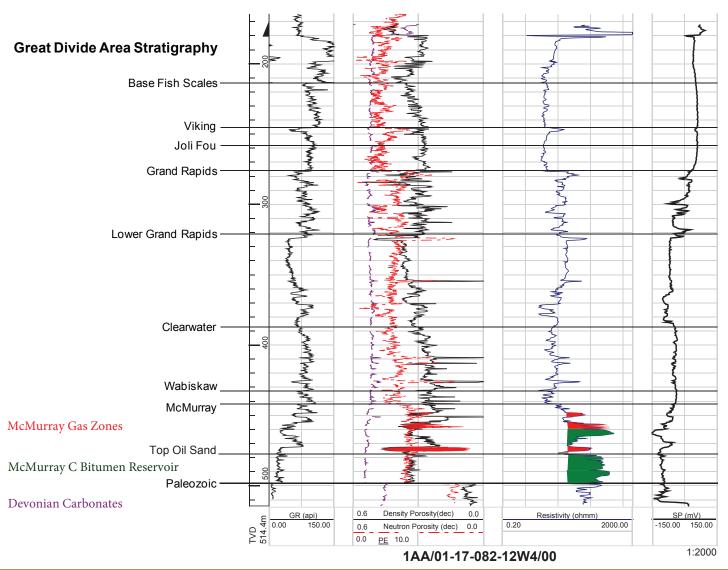
	Pod One @ Sept 30, 2019	Algar @ Sept 30, 2019
First Steam	September 2007	May 2010
First Sales Oil	October 2007	June 2010
Cumulative Bitumen Produced e ³ m ³	4,372	2,969
Cumulative Steam Injected e ³ m ³	16,522	14,196
Cumulative SOR	3.78	4.77
Number of Producing Well Pairs	19	18
Number of Circulating Well Pairs	0	0
Infill Wells Producing	12	5
Wells Using Gas Lift	0	18
Wells Using Downhole Pumps	31	5
Operating Pressure Gas Lift	N/A	3850 - 4000 kPa
Operating Pressure Pump	1300 - 3000 kPa	N/A
Directive 51 Operating MOP	6205 kPa Maximum Operating Pressure	6205 kPa Maximum Operating Pressure



Subsurface - Geology

Great Divide Area Type Well

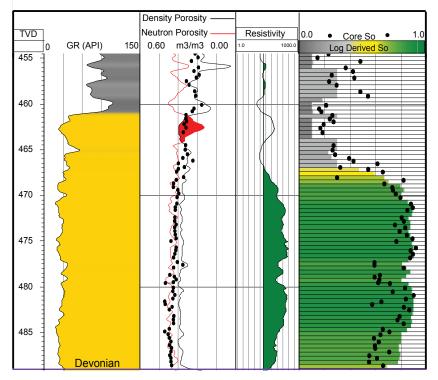




Great Divide Area Core & Log Data



Typical Composite Log with Interpretation and core data comparison.



1AA/13-16-082-12W4/00

- •Log vs Core Comparison
- •Analytical interpretation of geophysical logs to determine bitumen saturations (wt%) gives good correlation with core derived bitumen saturations (wt%). Examples shown below.

			Log	Core
	Log	Core Net	Bitumen	Bitumen
Well	NetPay	Pay	Wt %	Wt %
100/08-17-082-12W400	21.3	23.3	13.6%	14.0%
1AA/03-17-082-12W400	13.2	12.0	11.6%	12.7%
1AA/03-21-082-12W400	14.9	13.3	10.2%	10.4%
1AA/07-16-082-12W400	25.9	27.7	11.5%	12.7%
1AA/10-21-082-12W400	20.8	17.2	13.2%	14.8%



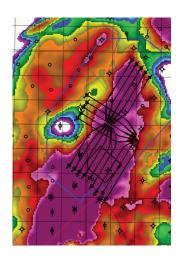
Great Divide Reservoir Parameters



	Pod One		Algar	
	Range	Average	Range	Average
Reservoir Thickness (m)	10 - 30	22	10 - 30	25
Depth to Top of Reservoir (m)	450 - 490	475	465 - 500	485
Reservoir Net Pay (m)	10 - 25	21	10 - 30	22
Oil Saturation (%)	75 - 85	80	72-80	76
Bitumen Density (kg/m3)		1018		1018
Bitumen Viscosity (cPs)		> 1 million		> 1 million
Porosity (%)	32 - 34	33	32 - 34	33
Vertical Permeability (mD)	1500 - 4000	7	1500 - 4000	-
Horizontal Permeability (mD)	2000 - 5000	<u></u>	2000 - 5000	-
Initial Reservoir Temperature (°C)		13		13
Initial Reservoir Pressure (kPa)		3500		4500
Initial Bottom Water Pressure (kPa)				2500

Great Divide Area - 3D Seismic



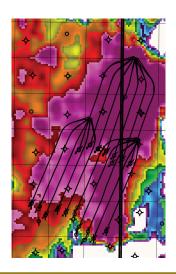


Pod One

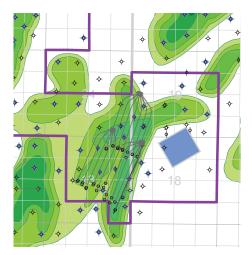


Net Pay (m)
10-15m
15-20m
20-25m
25-30m
>30m

3D Seismic - Interpreted McMurray Sand Isochron



Algar



3D Seismic has been successfully used by Connacher to define edges, sand thickness and paleo structure, and ultimately reduces the drilling costs.

No new seismic was shot during the last twelve months.

Great Divide Area Oil Sands Facies and Pay



Zones

Defined by Vshale

Connacher Cut-Offs

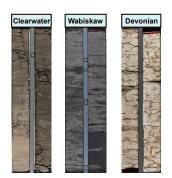
Z1 (Sand): 0-10% fines **Z2** (Sandy IHS): 10-20% fines

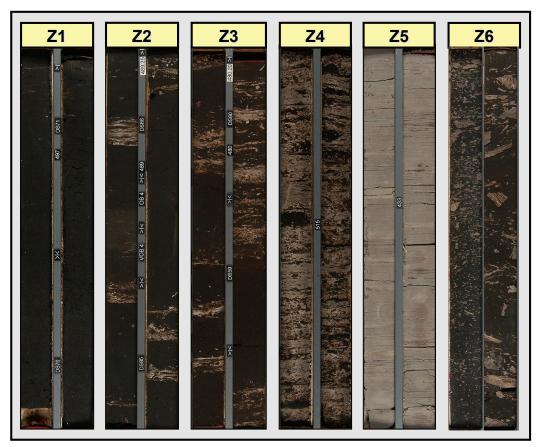
Z3 (IHS): 20-50% fines **Z4** (Muddy IHS): 50-80% fines

Z5 (Mud): 80-100% fines **Z6** (Breccia): >10% clasts

Pay Base Criteria

Minimum bitumen grade: 7wt% Minimum Net/Gross ratio: 80 % Maximum included shale interval: 2m Minimum zone thickness: 10 m



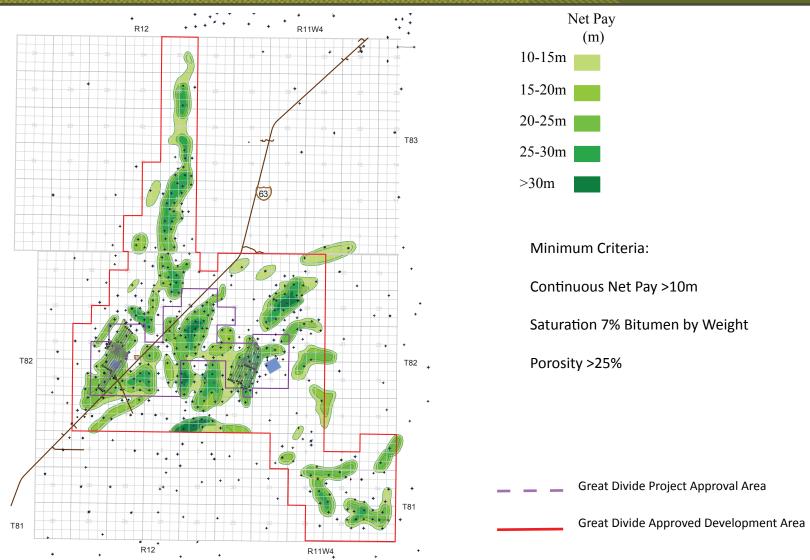


Core displayed is from a number of separate wells

Facies Z1,Z2, and Z3 are included in net pay

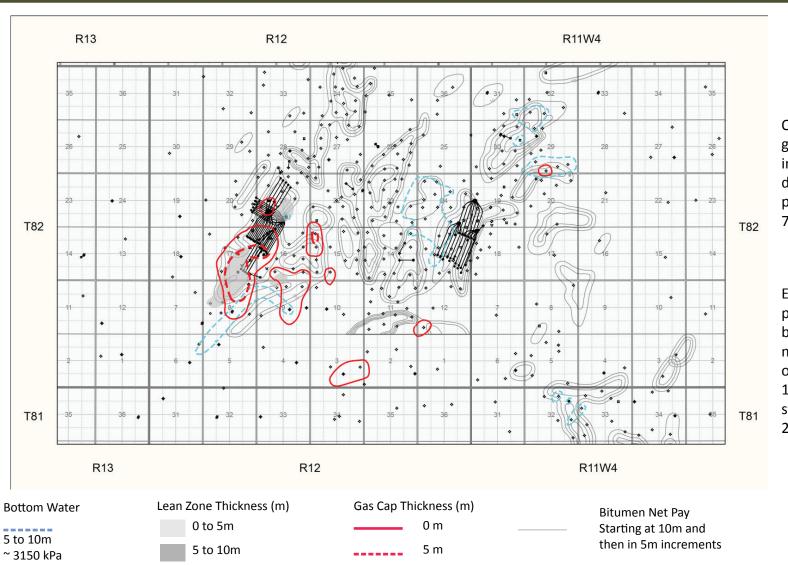
Net Pay Map Great Divide Area





Combined Gas Cap & Lean Zone & Bottom Water Map



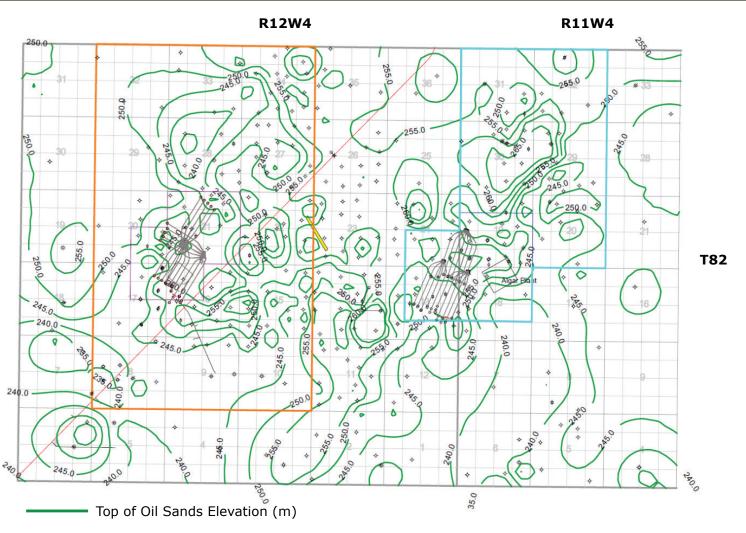


Original pressure of the gas cap was 2027 kPa in 1988. Subsequent to depletion, the lowest pressure recorded was 746 kPa in 2003.

Estimated original BW pressure of 2500 kpa based on lowest (520 mKB) gauge in Algar observation well 100/15-13-082-12W4 prior to steam injection May 2010.

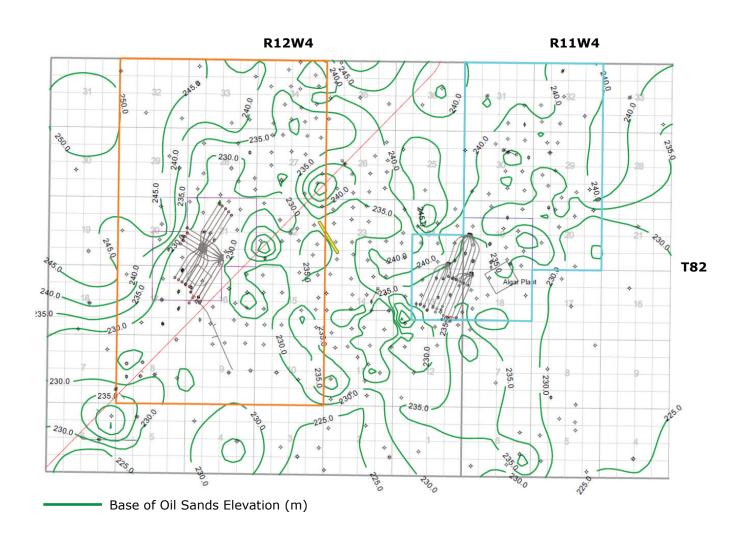
Top of Oil Sands Elevation





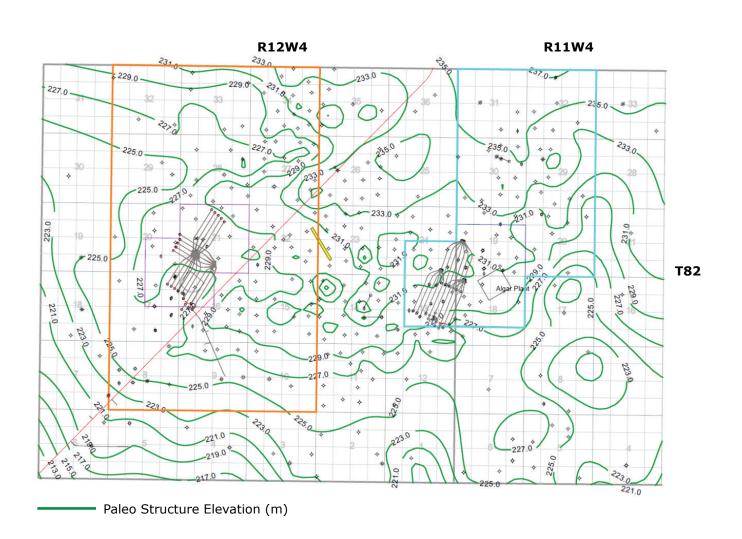
Base of Oil Sands





Paleo Structure Elevation







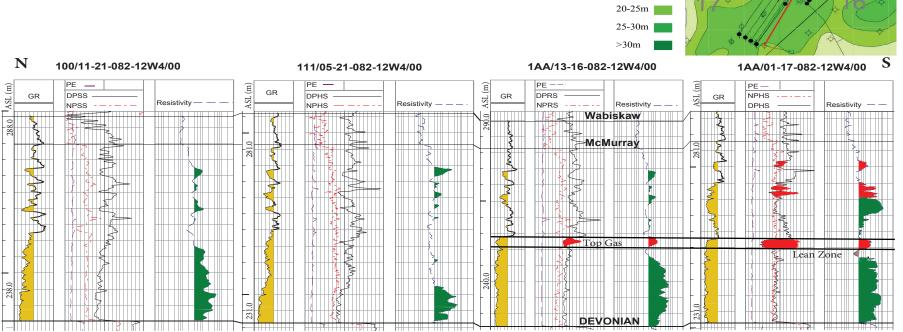
Net Pay (m)

10-15m

15-20m

Typical Section - Pod One

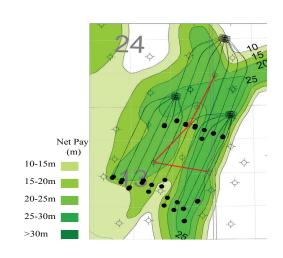
Pad 101N is characterized by a higher abundance of IHS in the upper part of the reservoir. As seen in well 05 - 21, the sand body gradually thins to the west. In contrast, the reservoir to the south is dominated by clean Z1 sand facies but develops a gas cap with a lean zone above the bitumen pay column.

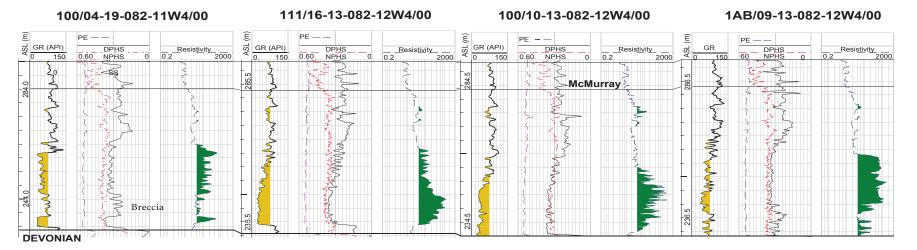




Typical Section - Algar

The Algar reservoir has a some IHS along with a breccia deposit to the north seen in well 100/04-19. Despite poor gamma ray, well 1AB/09-13 confirms high quality reservoir to the east which can be seen on the resistivity curve and veryfied by core. The poor gamma ray is caused by inaccurate log calibration.

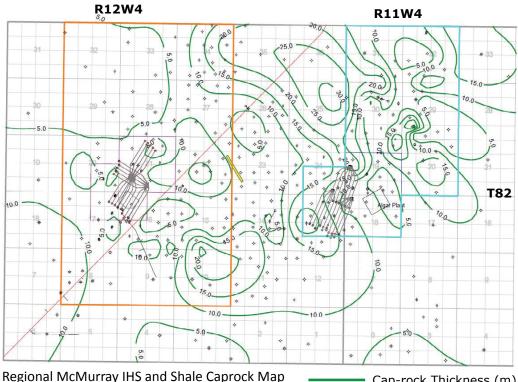




Cap Rock Integrity







Regional McMurray IHS and Shale Caprock Map ———— Cap-rock Thickness (m)

The cap-rock in the Great Divide Area consists of a mixture of muddy inclined heterolithic strata (IHS) and a mudstone that average over 10 meters in thickness. The muddy IHS consists of 80% volume of shale that is bio-turbated with mud-lined and sand-filled burrows. Muddy IHS is interpreted to be deposited in a muddy point bar. The light grey mudstone is thinly bedded with the top containing siderite nodules and rootlets. It is interpreted to be deposited in a mud flat to swamp environment. Above are core photos of the cap rock from well 1AA/06-21-82-12W4.

This regionally extensive McMurray caprock is considered the caprock for the project. The McMurray caprock is overlain by the Wabiskaw and Clearwater shales described on the following slide.

Cap Rock Integrity - Mini Frac Tests



Results of the 1st Mini Frac at 1AB/14-27-082-12W4

Zone Tested	Test Interval (mKb)	BH Fracture Pressure (kPa)	Gradient (kPA/m)	Closure Pressure (kPa)
Clearwater Shale	390 - 395	8,463	21.7	5,805
Wabiskaw Shale	417 - 425	10,991	26.3	9,500
McMurray Shale	449 - 452	8,583	19.1	6,106
Mcmurray Oilsand	461 - 466	8,463	17.7	5,805

Wabiskaw

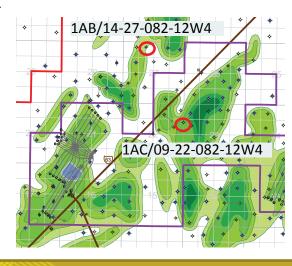
A Mini Frac test was conducted in well 1AB/14-27-082-12W4 in February 2010. Certain concerns were raised about one test being representative for the whole project area and also the closure pressure determined for the Wabiskaw which could have been influenced by local changes in rock mechanical properties.

Consequently a second test was conducted at 1AC/09-22-082-12W4 in April 2013, and this is reported in the table below.

Results for the second test are similar to the first. Although the Wabiskaw measured the highest stress gradient it was reduced from the first test.

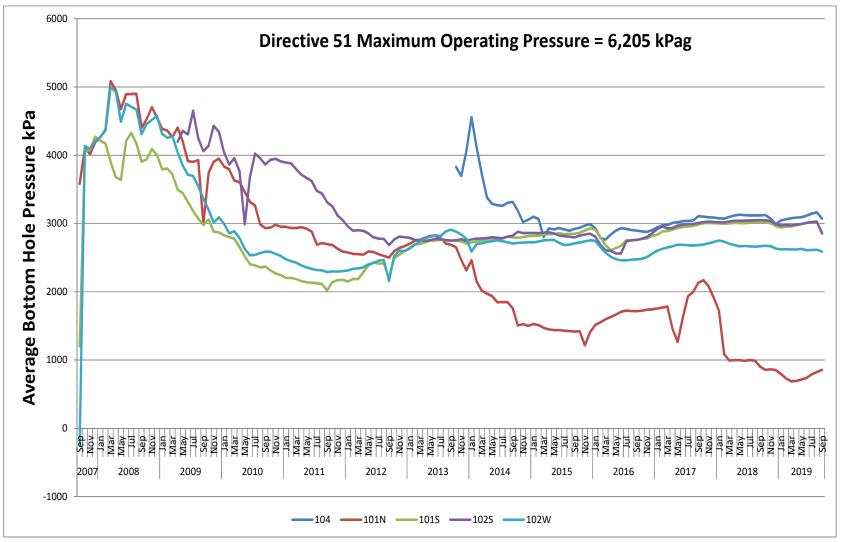
Results of the 2nd Mini Frac at 1AC/09-22-082-12W4

Zone Tested	Test Interval (mKb)	BH Fracture Pressure (kPa)	Gradient (kPA/m)	Closure Pressure (kPa)
Clearwater Shale	463 - 464	8,635	18.6	6,421
Wabiskaw Shale	474 - 475	10,534	22.2	7,917
McMurray Shale	481 - 482	8,057	16.7	6,155
Mcmurray Oilsand	517 - 518	6,503	12.6	5,397



Cap Rock Integrity - Pod One Monthly Average BH Injection Pressure

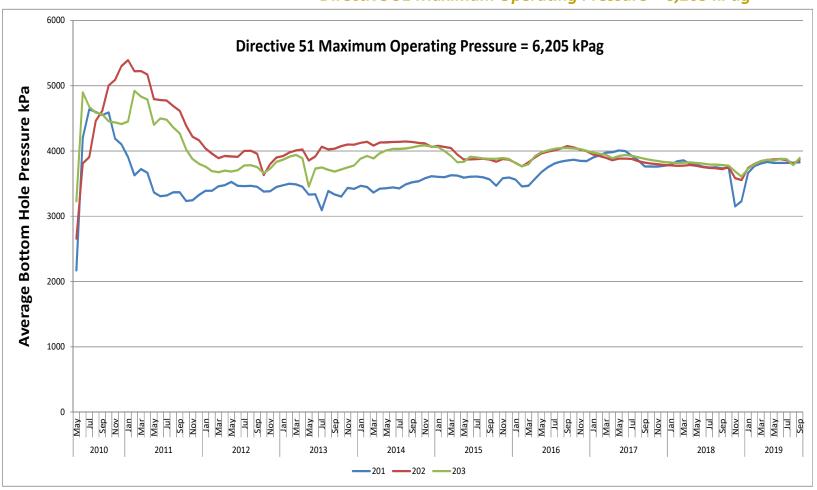




Cap Rock Integrity - Algar Monthly Average BH Injection Pressure



Directive 51 Maximum Operating Pressure = 6,205 kPag



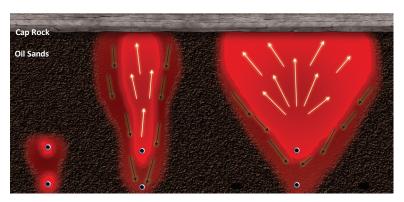




Great Divide SAGD Recovery Process



Basic Process



Circulation
High Pressure
~90 days
Steam Lift

Peak SAGD Production
High Pressure
~12 to 18 months
Gas Lift

Low Pressure SAGD Production
Low Pressure
~4 to 6 years
Pumps

Additional Process

Pod One

- Pressure Balancing under a gas cap and lean zone
- Infill Wells
- Gas Cap Repressurization
- Natural Gas Co-injection (intermittent pressure maintenance)

Algar

- Pressure Balancing over a water zone
- Infill Wells
- SAGD+® Commercial Project
- Natural Gas Co-injection (intermittent pressure maintenance)

Technologies Developed/Developing

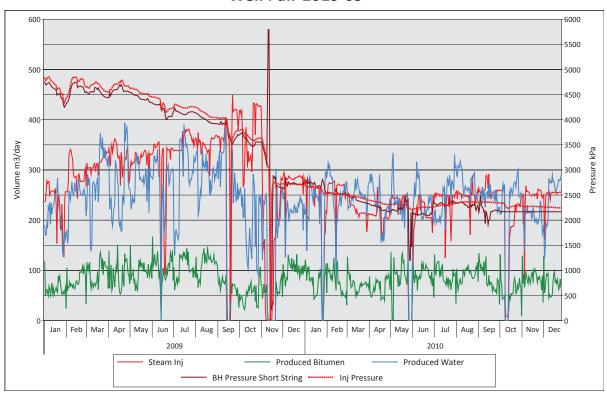


Description	Stage	Reason	Approvals
Pressure Balancing Under a Top Gas & Lean Zone & Bottom Water	Developed	 Eliminate steam losses into a gas and lean zone, lower SORs and improve productivity. Required the parallel development of reliability on high temperature downhole pumps. 	Operating within existing approvals
Gas Co-injection	Implemented	Natural gas can replace steam to maintain pressure	Approved for full field at Pod One Approved for full field at Algar
Gas Cap Repressurization	Implemented	Reduces steam losses into gas cap and lean zone	Approved
SAGD+® Process Trial / Commercial	Trial Completed	Reduces bitumen viscosity lower than steam alone to improve production rates, SOR, and recovery.	Commercial SAGD+® Commercial Project approved at Algar
Infill Wells	Implemented	Additional production and reserves at low capital and SORs	Approved for Infill Wells at Algar and Pod One

Pressure Balancing (Top Gas & Lean Zone)



Well Pair 101S-09

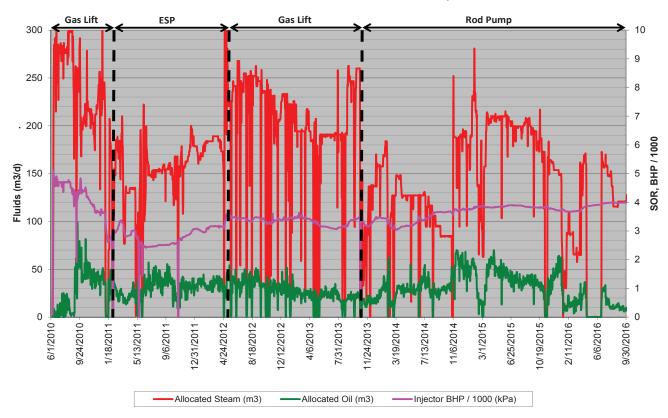


- Temporary production impact during pressure balance
- Improved SOR with low pressure operation
- Pad 104 is being operated in a similar manner except that the re-pressurization is expected to reduce the quantity of steam losses when the steam reaches the lean zone and pumps are being installed earlier

Pressure Balancing (Bottom Water)







- No update in strategy for pairs operating above bottom water
- Monitoring injection pressure, SOR, and produced water chlorides for signs of steam loss and bottom water production
- Continued operation with mechanical lift (pump) and injection via steam diverter in 201-I03

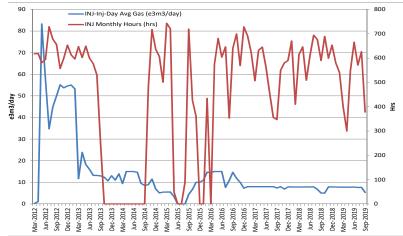
Re-Pressure Pod One Gas Cap

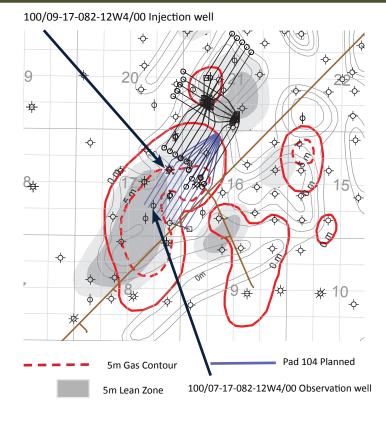


The purpose of gas cap repressurization is to increase the pressure in the gas cap and bitumen lean zone immediately above Pad 104 and institute a more effective pressure balancing process. Simulations have shown long term benefits to production and SOR by repressurizing to just below the SAGD operating pressures, 2000 - 3000 kPa with mechanical lift. Details are discussed in Connacher's Pressure Balancing paper, available upon request.

- The repressurizing process was underway prior to the start up of Pad 104 in 2013. Methane was injected into the 9-17 well at the injection rates shown in the graph below.
- The gas cap pressure at the 7-17 observation well was approximately 1600 kPa prior to gas injection, and the average pressure for 2019 was 2758 kPa in the gas cap and 4108 kPa in the lean zone.
- Currently the well is injecting methane to maintain the pressure.

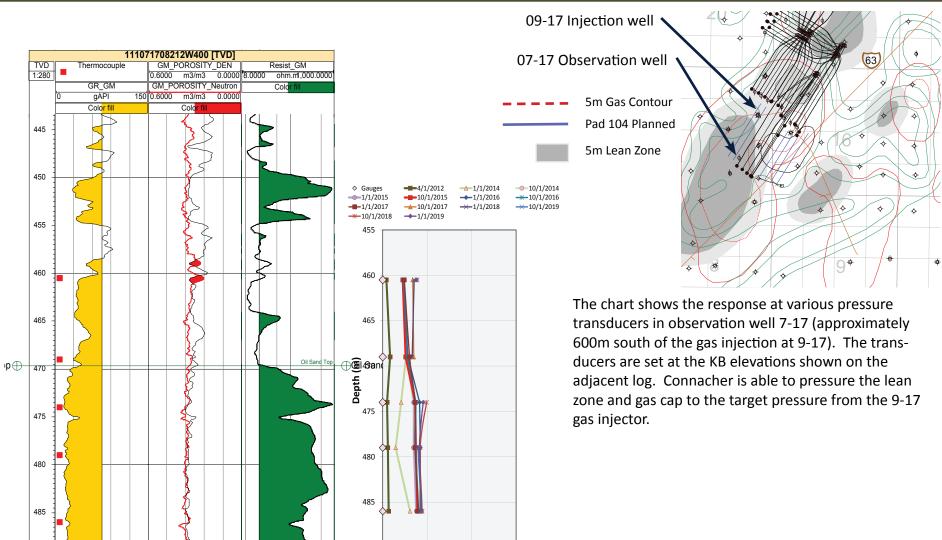
• The response to gas injection at the 7-17 observation well is shown in the following slide.





Re-Pressure Pod One Gas Cap





1500

3500

5500

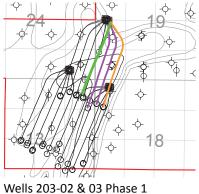
7500

SAGD+® Commercial Project



Phase 1

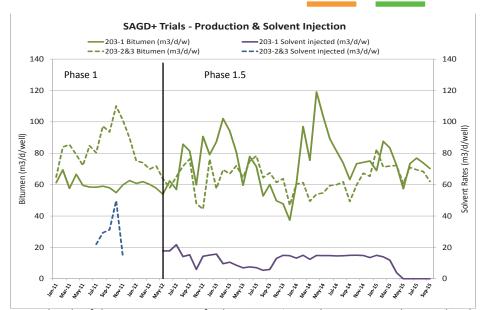
- In January 2011, ERCB granted approval for a trial of light hydrocarbon steam co-injection in the seven well pairs of Pad 203.
- Connacher selected two well pairs 203-2 and 203-3 for an initial test (Phase 1) of the process.
- In Phase 1, a commercially available solvent was co-injected with the steam starting in July 2011 at initial rates of approximately 10% by volume and increased to 15% by volume in October 2011. Compared to an April 2011 baseline, daily average per well bitumen production volumes during the months of August 2011 through October 2011 increased approximately 28% percent with a SOR decrease of 16%. The SOR decrease was limited by the necessity to increase steam injection rates to maintain normal operating pressure.
- Phase 1 injection ended November 2011. Solvent was recovered from the Phase 1 wells until April 2012 just prior to the start of Phase 1.5. 89% of the solvent had been recovered to surface.



Well 203-01 and 203-04 Phase 1.5

Phase 1.5

- Phase 1.5 commenced in May 2012 with solvent injection of approximately 10% until August when injection rates were reduced to approximately 6%, and further reduced in March 2013 to approximately 4%. In 2014 solvent injection rates averaged 5.9%.
- In the 12 months May 2012 through April 2013 bitumen rates increased by approximately 30% compared to the four months prior to the test. The SOR decreased 32% over the same period.
- In July 2013 an ESP was installed in 203-01. Following operational issues the pump was removed in December 2013. The bank of solvent built up during the ESP issues resulted in impoved results following the return to gas-lift.
- The SOR for Well 203-01 during the life of the test is 3.0 significantly lower than other wells in the project.
- Solvent injection was stopped in Well 203-1 on April 21, 2015.



Note: details of the measurement of solvent injection and recovery are discussed in the attached Steam Solvent SAGD Paper and the Algar MARP

Pad 101N



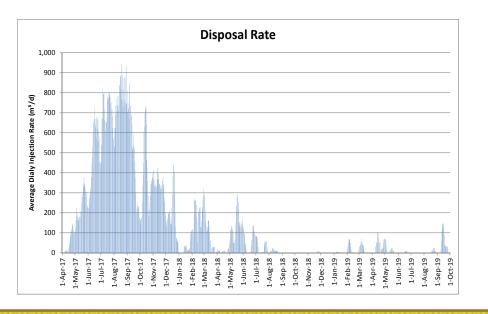
- Strategy for Pad 101N has not changed, going forward the plan is to continue to produce 101-P04 using rod pump
- No futher steam injection is planned
- Pad 101N was approved for produced water disposal on February 8th, 2016. Approval No. 10587S
- Produced water disposal into 101-I01 and -I02 began on April 15, 2017 and is ongoing
- Charts show the production history from 101N

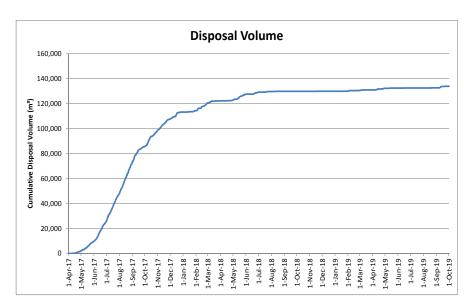


Pad 101N Produced Water Disposal



- Produced water disposal into 101-I01 and -I02 has declined from the peak in August 2017 as oil cut on SAGD production has recovered following the 2016 production curtailment
- Prior to August 2017, Connacher required a disposal strategy for produced water that was in excess of steam generation capacity
- Disposal of approximately 750 m³/d of produced water into 101N allowed Connacher to maximize production and accelerate time required for BS&W of SAGD pairs to "recover" following the production curtailment period
- Charts show the disposal history as well as the cumulative produced water disposal into 101N since April 2017

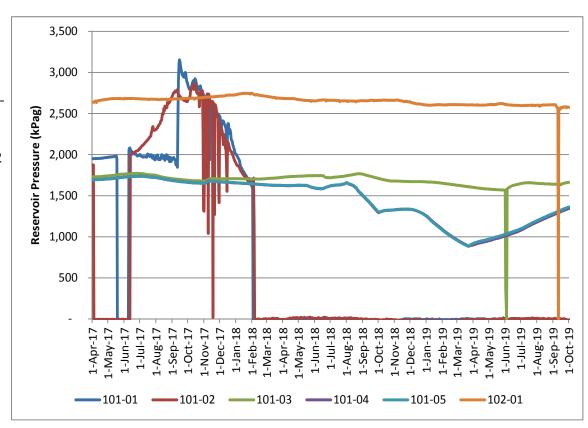




Pad 101N Produced Water Disposal



- Produced water disposal is conditional on not interfering with SAGD production operations
- Disposal into 101-I01 and 101-I02 only, 101-03 not operational, production from 101-04, 101-05, and 102-01
- Active monitoring of reservoir pressure in 102-I01 and 101-I04 for signs of communication with 101-I01 and -I02
- Bubble tubes on 101-I01 and I02 were mistakenly shut in until from April through mid-June 2017
- Bubble tube on 101-I01 (blue) was plugged and not reading accurate bottomhole pressure until mid-September 2017
- Downhole packers were installed on 101-I01 and-I02 in February 2018, making bottomhole pressure measurement, via annulus gas pressure inference, impossible
- There has been no indication of communication between 101-I01 and -I02, and 101-03 nor 102-01
- There has been no indication of loss of injectivity in either well; Connacher has no preventative maintenance planned for either well



NCG Co-injection



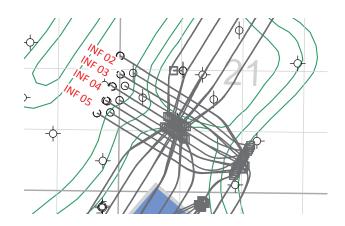
Non-condensible gas (NCG) co-injection is intended for use in pressure maintenance and ability to replace steam with NCG during times of steam shortage.

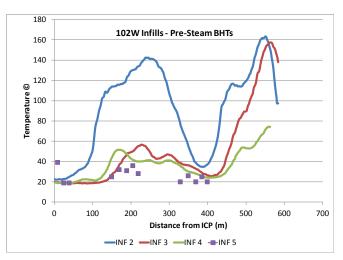
Commercial Scheme Approval issued for Full Field NCG Co-injection at all wells at Pod One and Algar:

- maximum of 10 e³ m³ per day
- limited to a maximum of 4 mole per cent with steam (monthly basis)
- limited to a maximum 20 per cent NCG replacement with steam (6 month average basis)

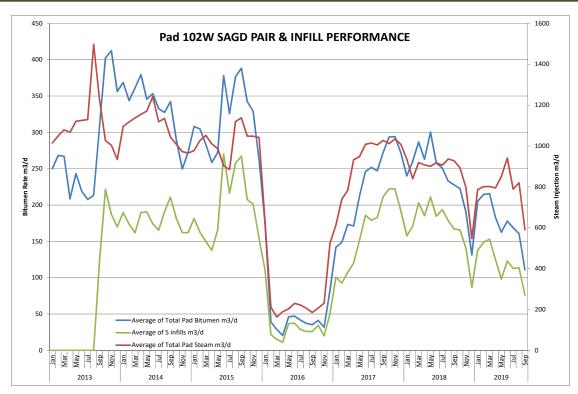
Infill Wells at Pod One - Pad 102W







Bottom Hole temperature surveys were carried out prior to steaming the infill wells.



- Infills were drilled shorter than the adjacent well pairs to avoid penetrating the thin channel edge
- Temperature logs prior to the steam injection indicated wide variations in temperatures along horizontal sections of the infill wells
- In order to increase temperature in the wells steam cycles were initiated as shown in the graph to the right
- Infill well 02 received the smallest volume of steam and responded the fastest and also had the highest temperature measured in the pre-steam survey.

Infill Wells at Pod One - Pad 101 & 102



Well Pad	Infill Well	UWI	Production Start Date	Cum Oil (m³)
1015	101-INF07	109/16-17-082-12W4/00	18-Sep-15	40,000
1015	101-INF08	108/16-17-082-12W4/00	13-Sep-14	80,406
1015	101-INF09	105/09-17-082-12W4/00	17-Jul-14	68,173
1015	101-INF10	112/12-16-082-12W4/00	24-Jul-14	54,619
1015	101-INF11	114/12-16-082-12W4/00	18-Aug-14	57,663
1015	101-INF12	113/12-16-082-12W4/00	4-Oct-14	96,878
102W	102-INF06	112/08-20-082-12W4/00	3-May-15	61,439
102W	102-INF13	115/12-16-082-12W4/00	19-Oct-15	51,585
102W	102-INF14	116/12-16-082-12W4/00	17-Jan-17	71,623

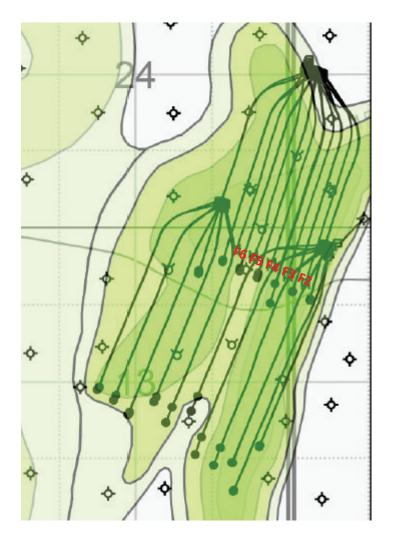


Infill Wells at Algar - Pad 203



Well Pad	Infill Well	UWI	Production Start Date	Cum Oil (m³)
203	203-INF02	05/13-18-082-11W4/0	1-Sep-19	3,143
203	203-INF03	20/16-13-082-12W4/0	4-Sep-19	1,084
203	203-INF04	21/16-13-082-12W4/0	8-Sep-19	1,199
203	203-INF05	22/16-13-082-12W4/0	9-Sep-19	1,085
203	203-INF06	23/16-13-082-12W4/0	6-Sep-19	1,650

 New Infill wells at Pad 203 drilled, completed, and producing as of September 2019.







Typical bottom hole pressure and temperature measurement



Injector well BHP measurement:

 Blanket gas on annular side of the wellhead which is isolated from steam injection points for short and long strings

Producer well BHP measurement:

- Algar (gas lift), read by the short string lift gas pressure at surface. This is landed at the heel of the well. The annulus of the well, function as a bubble tube.
- Pod One, read by instrumentation coils which function as a bubble tube. This is landed at the toe of the well. The coil has a check valve at the end to prevent fluid from backing up inside.

Injector well BHT measurement

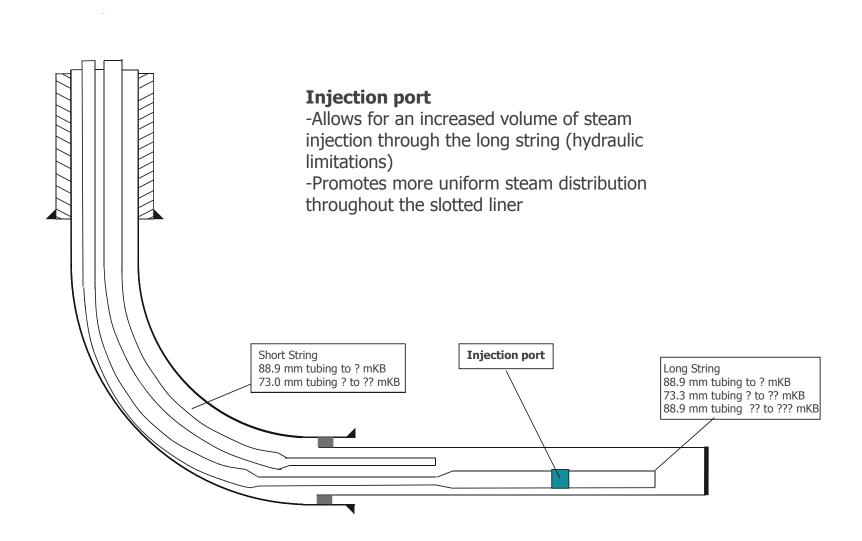
 Connacher does not measure injector well BHT. This is intrepeted from injector reservoir pressure using saturated steam temperature tables.

Producer well BHT Measurement

 Connacher uses instrumentation coil strings with fiber or thermocouples to measure producer well BHT at both Algar and Pod One.

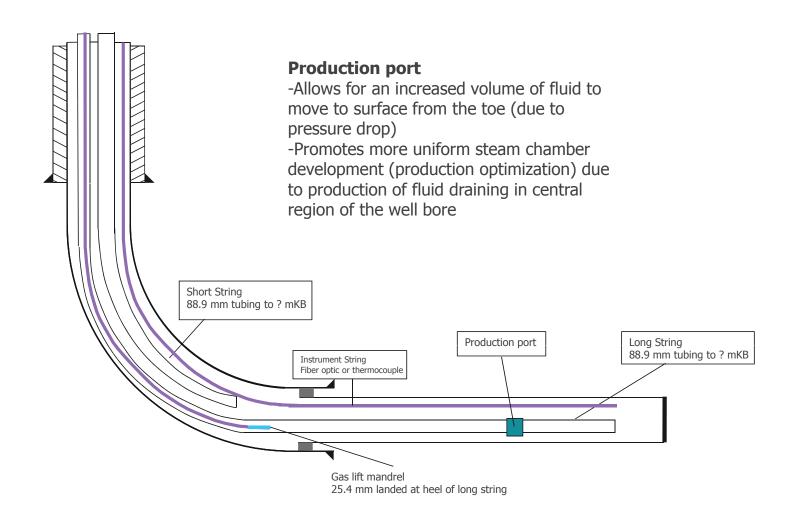
Typical Injector Completion





Typical Producer Gas Lift Completion



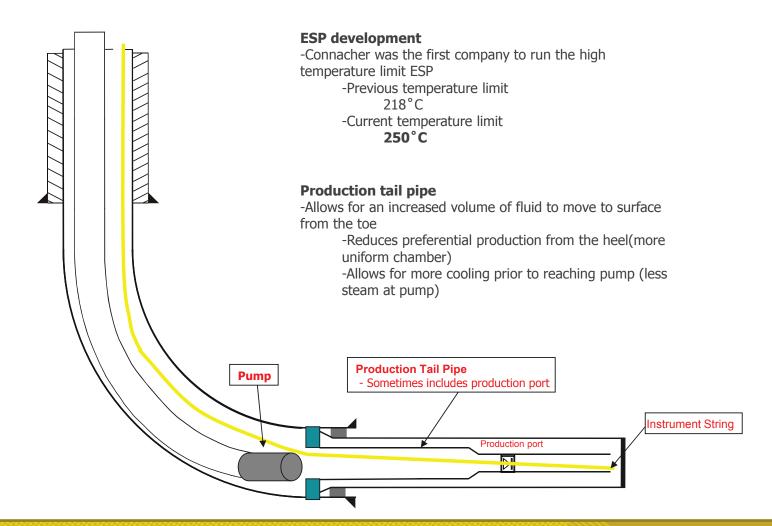


Typical Producer Mechanical Lift



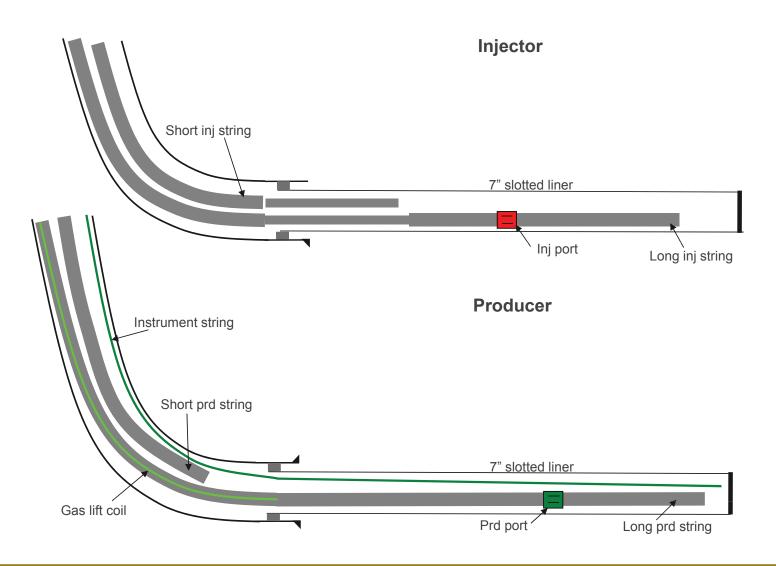
Electronic Submersible Pump

Metal on metal Progressive cavity pump Tubing pump (hydraulic pump jack)



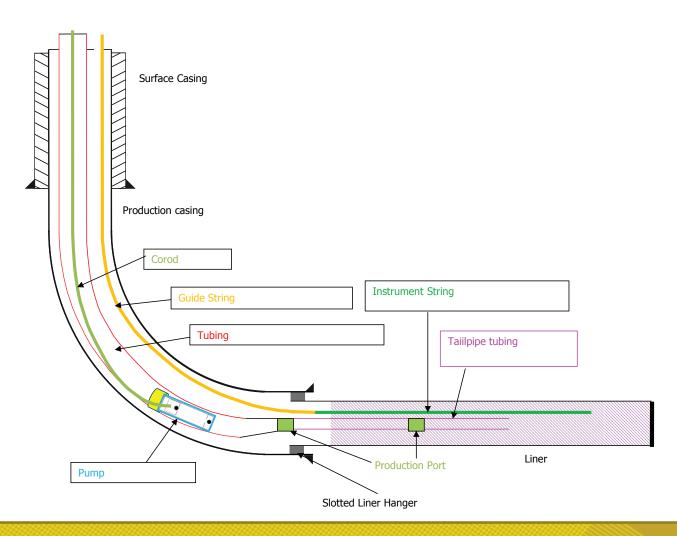
Improved Well Bore Design (Algar)





Typical Infill Well Completion









Artificial Lift Performance - Pod One



92898								8
Pad	Well	Pump Type	Pump	Install date	failure date	Run Time (days)	Current	
101N	101-01	PCP	1	5/5/2010	12/25/2010	234		
101N	101-01	Rod Pump	2	4/24/2013	5/29/2013	35		
101N	101-01	Rod Pump	3	10/26/2013	1/22/2016	818	Shut In	
101N	101-02	PCP	1	05/05/10	05/07/10	2		
101N	101-02	PCP	2	5/10/2010	11/5/2010	179		
101N	101-02	Rod Pump	3	4/14/2013	9/9/2013	148		
101N	101-02	Rod Pump	4	9/11/2013	2/12/2014	154		
101N	101-02	Rod Pump	5	2/17/2014	1/22/2016	704	Shut In	
101N	101-03	PCP	1	08/19/10	09/13/10	25		
101N	101-03	PCP	2	9/18/2010	10/16/2010	28		
101N	101-03	Rod Pump	3	9/26/2011	6/2/2012	250		
101N	101-03	Rod Pump	4	6/7/2012	1/9/2013	216		
101N	101-03	Rod Pump	5	1/15/2013	7/19/2013	185		
101N	101-03	Rod Pump	6	7/25/2013	1/22/2016	911	Shut In	
101N	101-04	PCP	1	08/11/10	11/05/10	86		
101N	101-04	Rod Pump	2	4/16/2013	5/31/2013	45		
101N	101-04	Rod Pump	3	10/27/2013	2/17/2014	113		
101N	101-04	Rod Pump	4	2/20/2014	7/28/2018	1619		
101N	101-04	Rod Pump	5	8/1/2018	10/1/2019	426	Running on Rod Pump	
101N	101-05	PCP	1	08/06/10	09/08/12	764		
101N	101-05	PCP	2	9/16/2012	7/25/2014	677		
101N	101-05	PCP	3	7/27/2014	8/28/2014	32		
101N	101-05	PCP	4	9/9/2014	10/14/2015	400		
101N	101-05	PCP	5	10/27/2015	10/13/2016	352		
101N	101-05	PCP	6	8/10/2018	3/23/2019	225	Shut In	

Pad	Well	Pump Type	Pump	Install date	Failure Date	Run Time (days)	Current
104	104-03	ESP	1	11/22/2014	4/24/2017	884	
104	104-03	ESP	2	4/30/2017	10/1/2019	884	Running on ESP
104	104-04	ESP	1	5/11/2014	10/25/2016	898	
104	104-04	ESP	2	11/4/2016	9/15/2017	315	
104	104-04	ESP	3	9/23/2017	8/16/2018	327	
104	104-04	ESP	4	8/26/2018	10/1/2019	401	Running on ESP
104	104-05	ESP	1	3/12/2015	3/8/2017	727	
104	104-05	ESP	2	3/27/2017	7/16/2018	476	
104	104-05	ESP	3	7/23/2018	7/25/2019	367	

Pads 101S, 102W, 102S & 104

These Pads produce from good quality oil sands reservoir and are a good application of ESP's. The pump history for 101N and 104 pads is shown here as an example.

The higher rate wells can accommodate ESP's whereas lower rate wells and infills operate more efficiently with rod pumps.

Pads 101S, 102W and 102S are similar and a detailed history of all the pumps at Great Divide is provide in the additional files accompanying this

Artificial Lift Performance - Algar



Pad	Well	Pump Type	Pump	Install date	Failure date	Run Time (days)	Current
201	201-03	ESP	1	1/19/2011	5/19/2011	120	
201	201-03	ESP	2	5/23/2011	10/22/2011	152	
201	201-03	ESP	3	10/28/2011	4/26/2012	181	
201	201-03	Rod pump	4	11/3/2013	6/19/2014	228	
201	201-03	Rod pump	5	6/22/2014	8/14/2014	53	
201	201-03	Rod pump	6	8/17/2014	3/1/2015	196	
201	201-03	Rod pump	7	3/7/2015	11/8/2015	246	
201	201-03	Rod pump	8	11/12/2015	4/24/2016	164	
201	201-03	Rod pump	9	6/23/2016	12/30/2016	190	
201	201-03	Rod pump	10	1/11/2017	2/19/2017	39	
201	201-03	Rod pump	11	2/27/2017	6/28/2017	121	
201	201-03	Rod pump	12	7/12/2017	9/30/2017	80	
201	201-03	Rod pump	13	10/22/2017	3/24/2018	153	Converted to Gas Lift
201	201-04	ESP	1	2/14/2011	6/14/2012	486	
201	201-04	ESP	2	6/21/2012	9/25/2013	461	
201	201-04	Rod pump	3	10/8/2013	10/21/2014	378	
201	201-04	Rod pump	4	10/24/2014	5/15/2015	203	
201	201-04	Rod pump	5	5/16/2015	10/15/2015	152	
201	201-04	Rod pump	6	10/22/2015	11/25/2016	400	
201	201-04	Rod pump	7	12/14/2016	6/29/2017	197	
201	201-04	Rod pump	8	7/13/2017	9/23/2017	72	
201	201-04	Rod pump	9	9/28/2017	12/14/2017	77	Converted to Gas Lift
201	201-05	FSP	1	1/27/2011	5/8/2011	101	
201	201-05	ESP	2	5/18/2011	5/2/2012	350	
201	201-05	ESP	3	5/5/2012	6/29/2013	420	
201	201-05	Rod pump	4	7/30/2013	5/19/2014	293	
201	201-05	Rod pump	5	5/22/2014	9/27/2014	128	
201	201-05	Rod pump	6	9/30/2014	2/2/2015	125	
201	201-05	Rod pump	7	2/5/2015	12/4/2016	668	
201	201-05	Rod pump	8	12/18/2017	8/27/2017	252	
201	201-05	Rod pump	9	9/26/2017	10/15/2017	19	
201	201-05	Rod pump	10	10/20/2017	3/7/2018	138	Converted to Gas Lift
203	203-01	ESP	1	5/3/2013	12/24/2013	235	Converted to Gas Lift
203	203-02	ESP	1	5/8/2013	9/5/2014	485	Converted to Gas Lift
203	203-02	ESP	1	5/14/2013	9/28/2013	137	Converted to Gas Lift
203	203-64 203-F02	Rod pump	1	9/1/2019	9/12/2019	11	CO.IVETECA TO GAS EITE
203	203-F02 203-F02	Rod pump	2	9/14/2019	10/1/2019	17	Running on Rod Pump
203	203-F03	Rod pump	1	9/4/2019	9/10/2019	6	iiiig oir nou'r uirip
203	203-F03	Rod pump	2	9/12/2019	9/15/2019	3	
203	203-F03	Rod pump	3	9/24/2019	10/1/2019	7	Running on Rod Pump
203	203-F04	Rod pump	1	9/8/2019	9/27/2019	19	naming on nou rump
203	203-F04 203-F04	Rod pump	2	9/30/2019	10/1/2019	1	Running on Rod Pump
203	203-F05	Rod pump	1	9/2/2019	9/2/2019	0	naming on nou rump
203	203-F05 203-F05	Rod pump	2	9/9/2019	10/1/2019	22	Running on Rod Pump
203	203-F05 203-F06	Rod pump	1	9/6/2019	10/1/2019	25	Running on Rod Pump
203	203-100	Nou pump	1	3/0/2013	10/1/2019	23	Running on Rou Pullip

Algar

In late-2017 and 2018 the remaining three rod pumping wells, 201-03, -04, and -05, were converted to gas lift.

Going forward, artificial lift on well pairs at Algar will solely gas lift until a conversion back to mechanical lift is warranted by reservoir pressure and operating strategy.

The new infill wells at Pad 203 have been equipped with Rod pump.

Historically, both ESPs and rod pumps have been on Pad 201 due to the proximity of the wells to a limited bottom water zone.

As part of the SAGD+™ pilot, ESPs were installed in three wells in Pad 203. Due to reservoir characteristics and economics, these wells were converted back to gas lift.

Gas Migration & Surface Casing Vent Flows



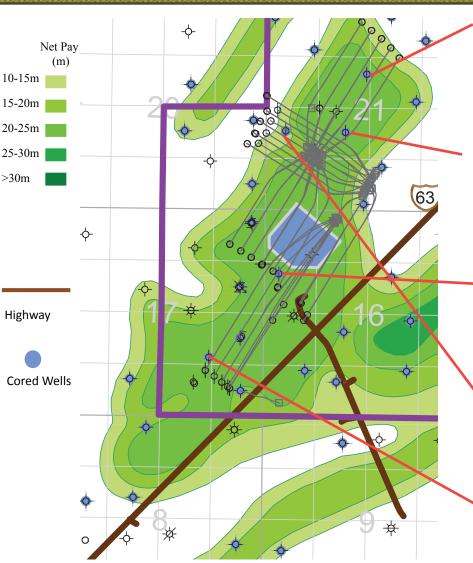
- SCVF tests were conducted on all injectors and producers at Pod One and Algar in September, 2018. No issues were identified and the results have been reported to the AER through DDS.
- SCVF tests will be completed in late-2019, the results of which will be reported to the AER through DDS.





Pod One Observation Wells





100/11-21-82-12W4, Operational Apr 2011

- Monitor North Pad Performance (47 m from Well Pair 101-04)
- Five temperature and five pressure measurements all operational
- Temperature readings suspect all at original reservoir temperature ~14 °C
- Pressure gauges operational
- Continue collecting data

100/06-21-082-12W4, Operational Dec 2007

- Purpose was to measure rise of steam and to determine if steam moved into any overlying gas caps (39 m from Well Pair 101-05)
- Operational but readings suspect
- Maximum temperature 20 °C
- Pressure gauges not operational
- Continue collecting data

111/12-16-82-12W4, Operational Mar 2010

- Provided observations on effects of low pressure operations (40 m from Well Pair 101-10)
- Five temperature measurements all operational. 3 of 5 Pressure gauges not operational
- Continue collecting data

111/05-21-82-12W4,Operational Mar 2012

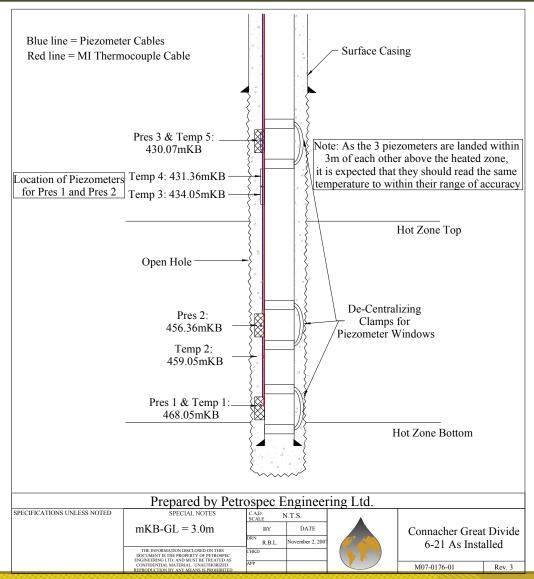
- Drilled to acquire information on temperature between well pairs for future infill wells (40m from Well Pair 102-03)
- Five temperature measurements operational. Lower pressure gauge not operational
- Continue collecting data

100/07-17-82-12W4, Operational Mar 2012

- Drilled to acquire information on gas cap repressurizing (33m from Well Pair 104-P03)
- Five temperature and five pressure measurements operational
- Continue collecting data

Pod One - Typical Observations Well

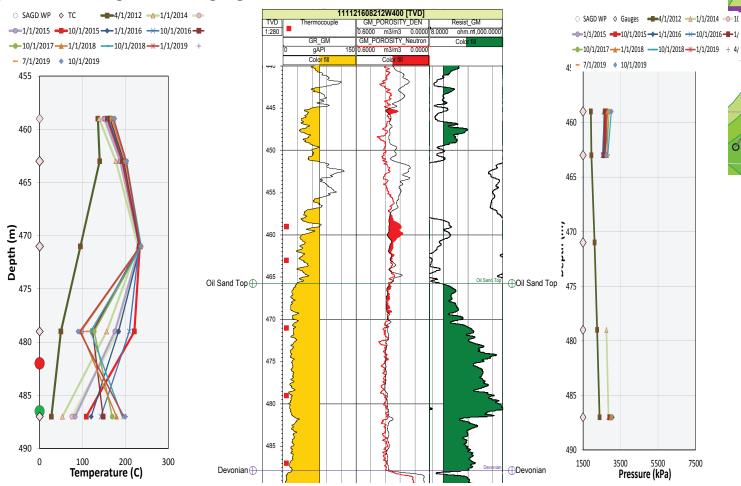


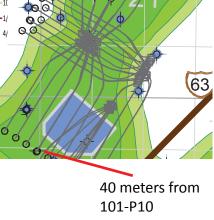


Pod One Obs Well - 111/12-16-82-12 W4



Chamber appears to be fully developed. Steam is suspected to be leaking to gas cap and lean zone. Temperature readings provide support for gas cap repressurization. No valid pressure readings for 3 of 5 gauges.

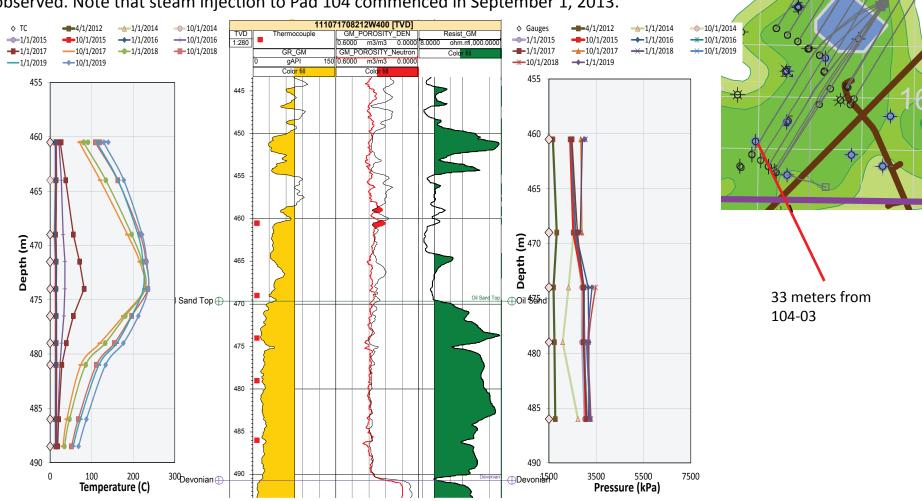




Pod One Obs Well - 111/07-17-82-12 W4



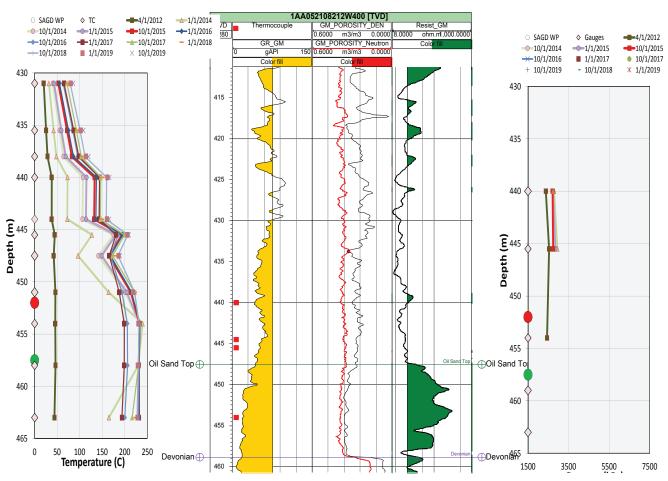
Temperature response observed by April 2016. Pressure response to steam injection observed. Note that steam injection to Pad 104 commenced in September 1, 2013.

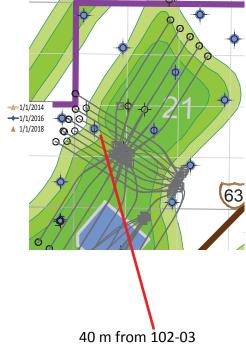


Pod One Obs Well - 111/05-21-82-12 W4



No valid pressure readings at the lowest gauge after January 1, 2013. The piezometer at 445.5 m has failed and is no longer reporting accurate reservoir pressure.

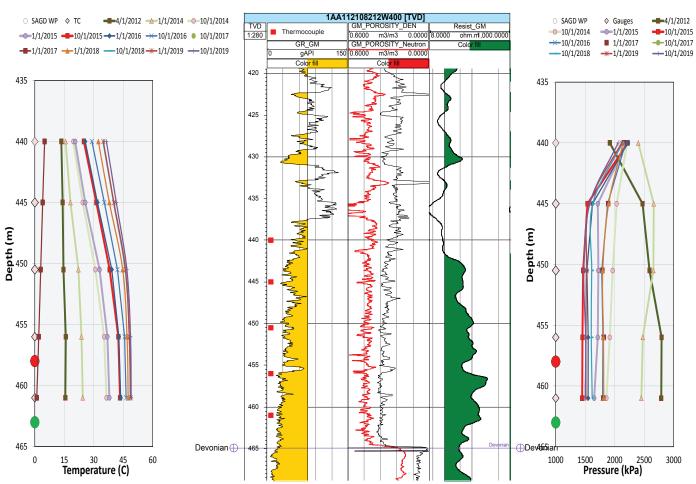


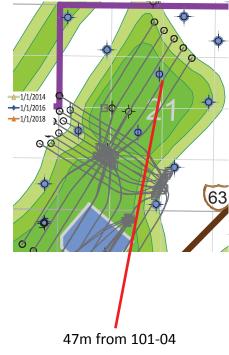


Pod One Obs Well - 100/11-21-82-12 W4



Temperature readings confirm that steam distribution in Pad 101N was a challenge. Note that Pad 101N is on blowdown. Temperature and pressure readings portray a relatively fast response to blowdown.

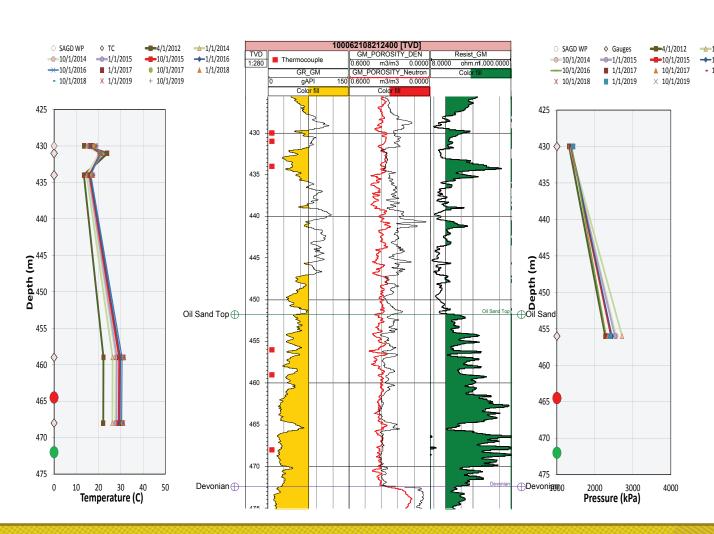


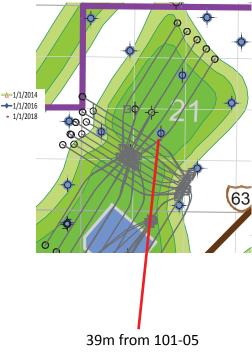


Pod One Obs Well - 100/06-21-82-12 W4



Pressure and Temperature readings are suspect.





Algar Observations Wells







100/04-19-082-11W4M Operational February 2011

- 6m from Well Pair 203-04
- Monitors Pad 202 performance
- Five temperature measurements operational
- Pressure measurement at 503.5 mKB failed Aug 2013

100/01-24-082-12W4M Operational February 2011

- 20m from Well Pair 203-06
- Five thermocouples operational
- Four pressure gauges operational

100/15-13-082-12W4M Operational February 2011

- 8m from Well Pair 201-04
- Five thermocouples operational
- One pressure gauge operational

100/09-13-082-12W4M Operational February 2011

- 37m from Well Pair 202-04
- Five thermocouples operational

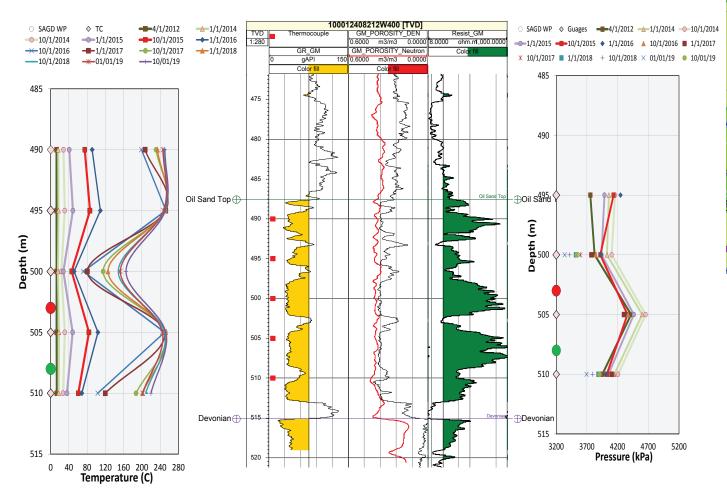
111/16-13-82-12W4W4 Operational March 2012

- 48m from Well Pair 203-05
- Five thermocouples operational
- Five pressure gauges operational

Algar Obs Well - 100/01-24-82-12 W4



Temperature readings at 490 m depth suggest that steam is moving to higher IHS zones. This suggests that the IHS zone are discontinuous at this location.

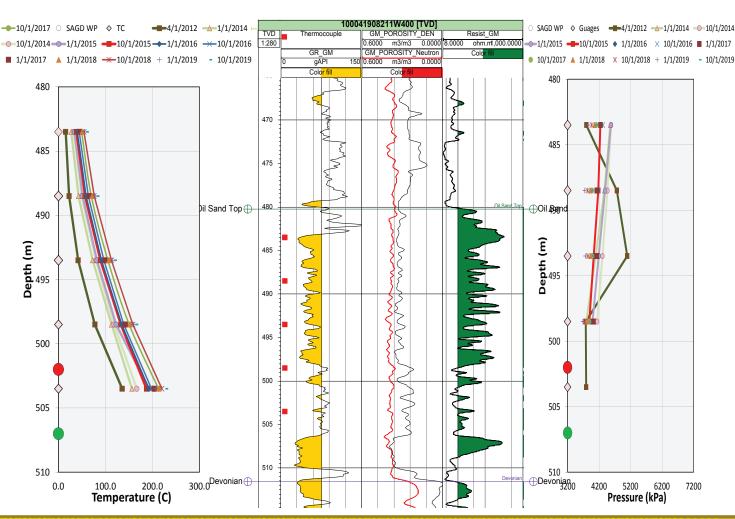




Algar Obs Well - 100/04-19-82-11 W4



Temperature readings show temperature development in intense IHS zones. Pressure readings at this location are suspect.

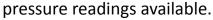


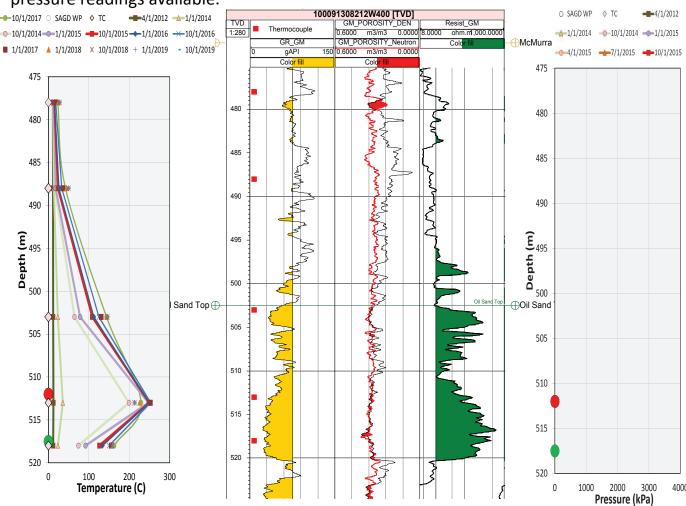


Algar Obs Well - 100/09-13-82-12 W4



Temperature readings supports the development of infill wells at this location. No



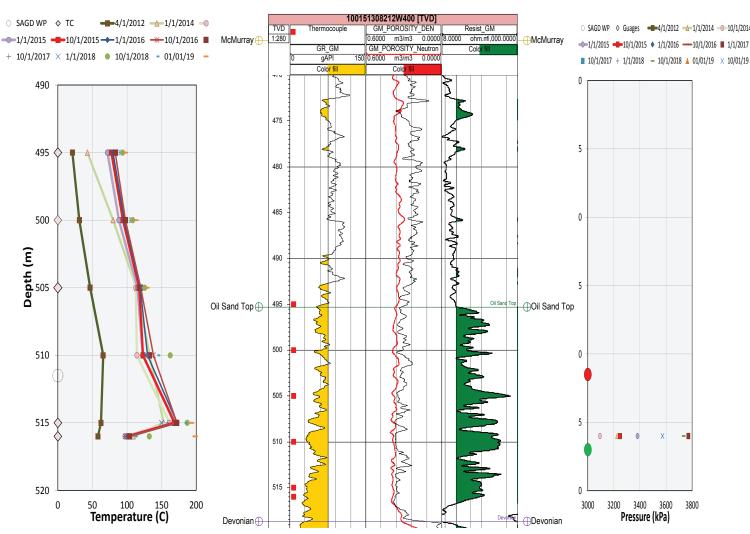




Algar Obs Well - 100/15-13-82-12 W4



Temperature readings show temperature response in IHS zone.

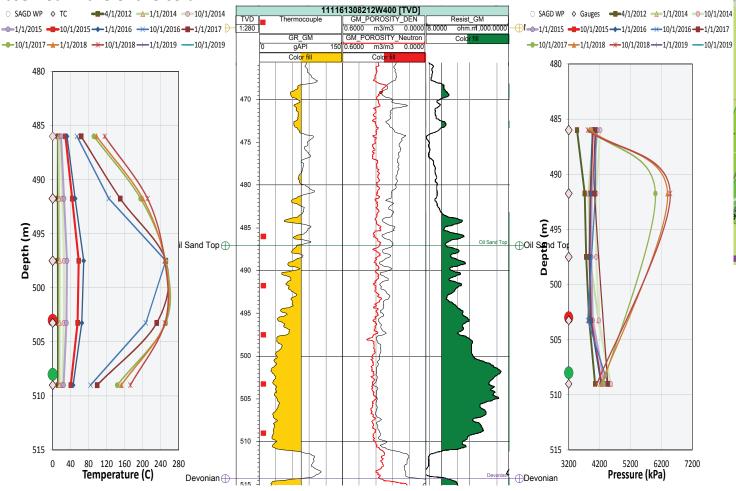




Algar Obs Well - 111/16-13-82-12 W4



Temperature readings shows temperature development in the IHS zone. It is expected that there will be more temperature response at lower depths in the future. Pressure response is observed in the entire column.





Notes on Obs Well equipment failure



Pod One

12-16-082-12W4 - Thermocouples at all measurement depths are operating properly. Piezometers at depths of 471, 478, and 487 m are not operating due to gauge failure. There are no plans to replace the equipment.

5-21-082-12W4 - Thermocouples at all depths are operating properly. Piezometer located at 445.5 m and 454 m are not operating due to gauge failure. There are no plans to replace the equipment.

6-21-082-12W4 - Thermocouples at all depths are operating properly. All piezometers in this well are not operational. There are no plans to replace the equipment.

7-17-82-12W4 - Thermocouples at all depths are operating properly. Piezometer located at 474 m and 469 m are not operating due to gauge failure. There are no plans to replace the equipment.

Algar

04-19-082-12W4 - Thermocouples at all depths are operating properly. Piezometer at 503.5 mKB is not operational. There are no plans to replace the equipment.

09-13-082-12W4 - Thermocouples at all depths are operating properly. All piezometers in this well are not operational. There are no plans to replace the equipment.

15-13-082-12W4 - Thermocouples at all depths are operating properly. Piezometer at 516 m is the only pressure gauge operating properly. There are no plans to replace the equipment.

16-13-082-12W4 - Thermocouples at all depths are operating properly. Piezometers at 503.3 and 497.5 mKB are not operational. There are no plans to replace the equipment.

Pod One & Algar Ground Movement





Highway 63 Profile Survey

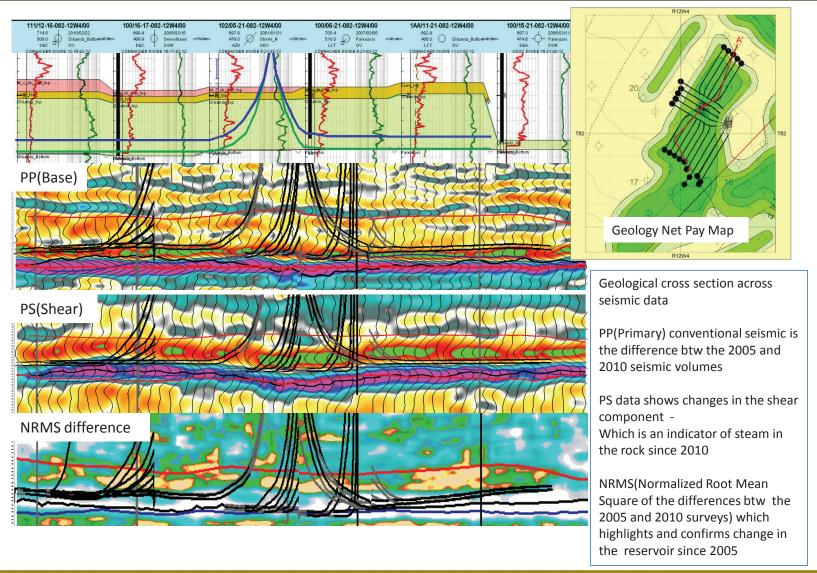
16 km of Highway 63's road profile adjacent to the Great Divide Project Area was resurveyed in 2019. Southbound lanes (original highway) continue to have agreement between the 2017 - 2019 data with no deviations of concern. Northbound lanes also match very closely between the 2017 and 2019 observation campaigns.

Static Monument Survey

40 monuments resurveyed in 2019 (17 at Algar, 18 at Pod One, & 5 controls). At Algar, slight subsidence in the area north of the Algar CPF was observed. At Pod One, localized uplift in the area southwest of the Pod One CPF was observed. Highway 63 road profiles and all static monuments will be resurveyed in summer of 2020 to investigate any long term trends.

Pod One 4D Seismic



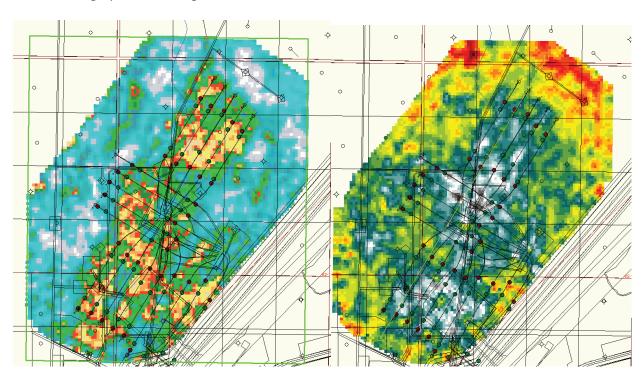


Pod One 4D Seismic (2)



NRMS - normalized root mean square represents the % change in the seismic signal since steaming operations began

Shear Data - should represent the extent of the steam chamber



The NRMS represents the percent change in the reservoir since steaming operations commenced in 2007. This roughly corresponds to produced bitumen and should represent the various steam chambers. The shear data is not affected by steam, gas or bitumen heated above 80 C, as this acts like a liquid. The resulting map should show the current extend of the steam chambers. The two maps should be similar and are not, therefore the results of the 4D seismic are inconclusive. Possible reasons for this include plant and highway noise, and errors resulting from using different geophones at different locations in the two surveys.





Great Divide Well Layout





Pod One

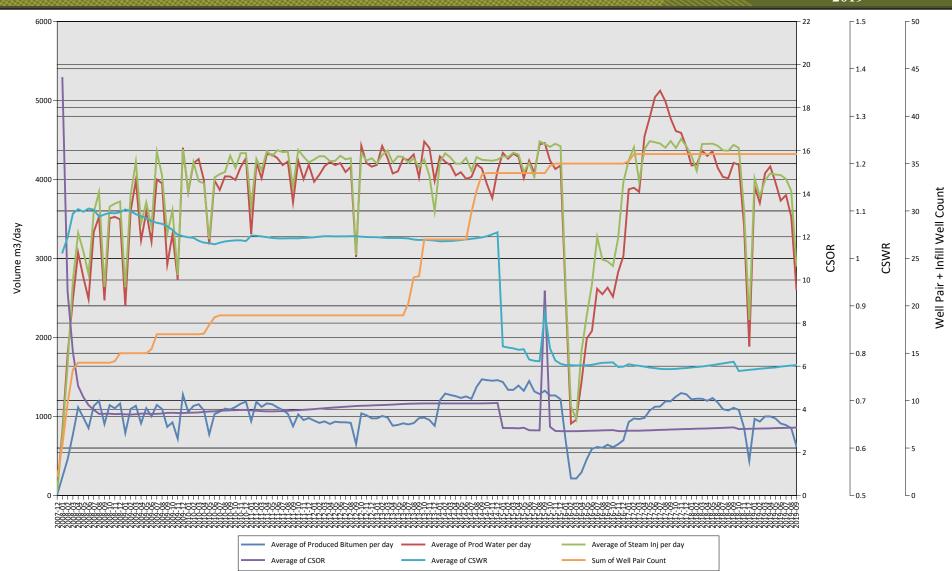
- 23 Well Pairs (101N, 101S, 102S, 102W and 104)
- 16 Infills
- SAGD well pairs in 101N, 101S, 102S and 102W were drilled at 100m spacing
- SAGD well pairs in 104 were drilled at 80m spacing
- All infills (except 102 INF06 @35m) were drilled at 50m spacing between the SAGD producers

Algar

- 18 Well Pairs (201, 202 and 203)
- 5 Infills
- All SAGD well pairs except 202 R01 were drilled at 100m spacing
- 202 R01 was drilled 35m from 201-01 and 65m from 202-02 well pair
- All infills drilled at 50m spacing between SAGD producers.

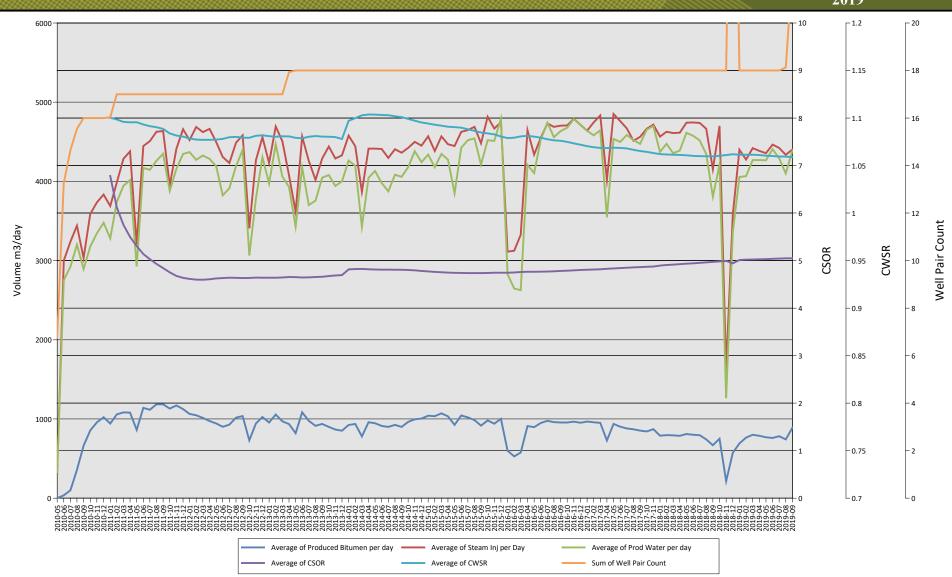
Pod One Performance





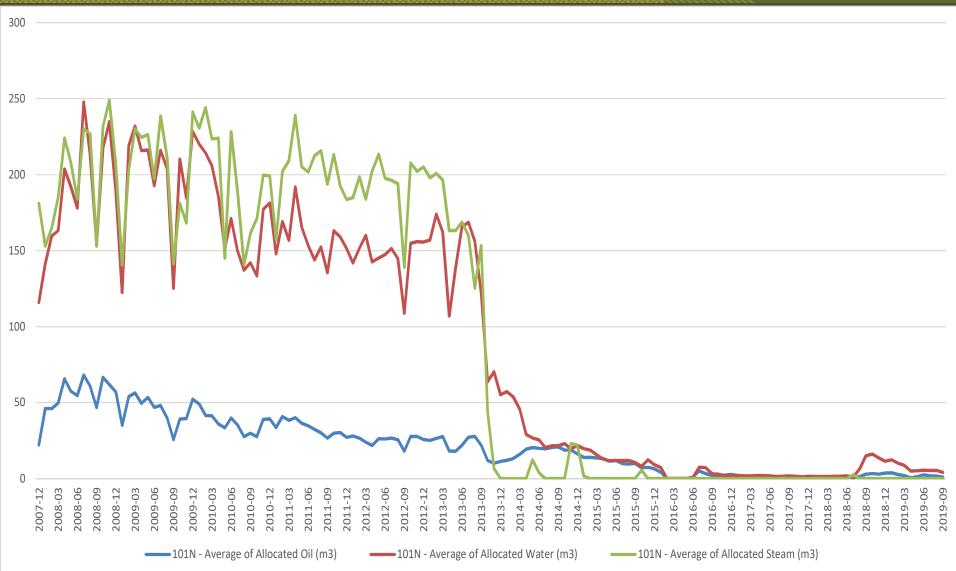
Algar Performance





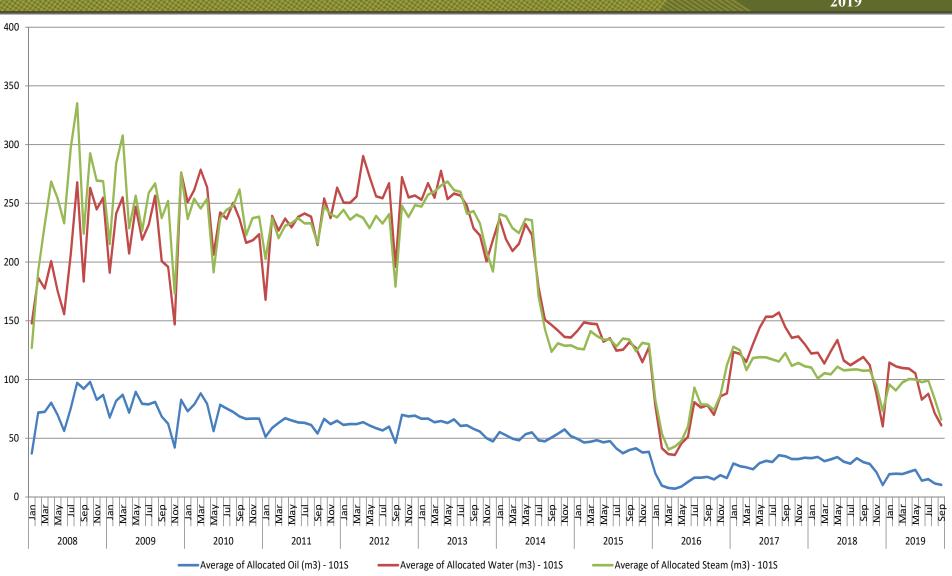
Pod One - Pad 101N Production





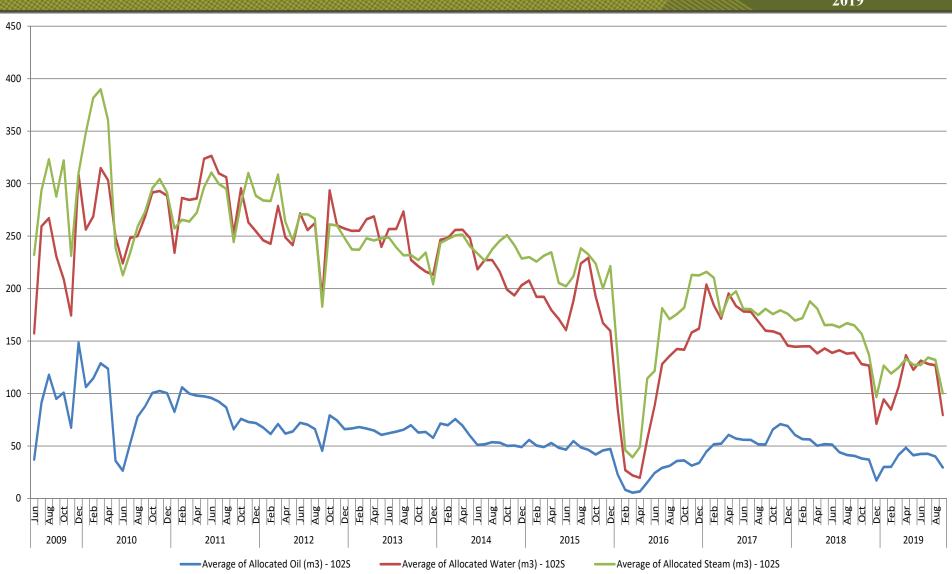
Pod One Pad 101S Production





Pod One Pad 102S Production





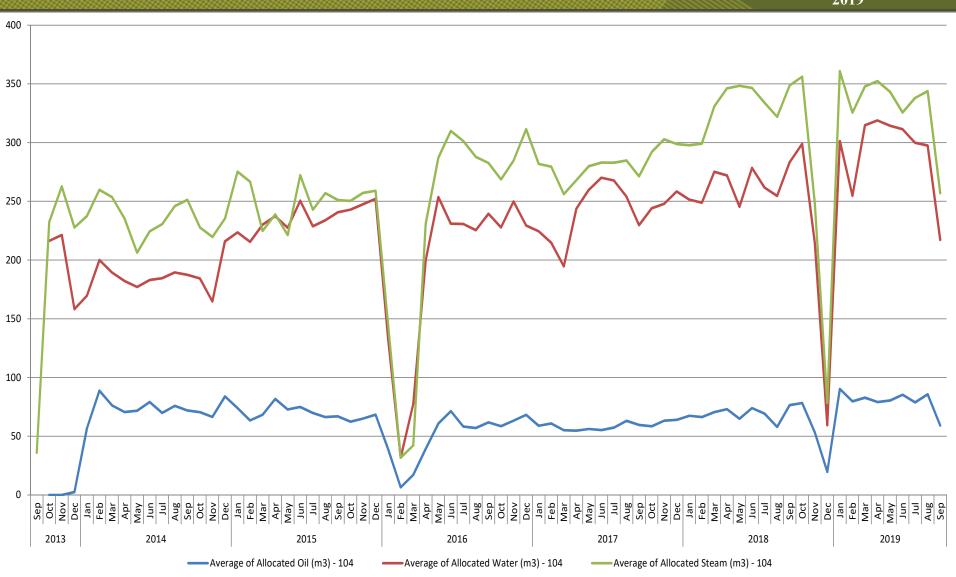
Pod One Pad 102W Production





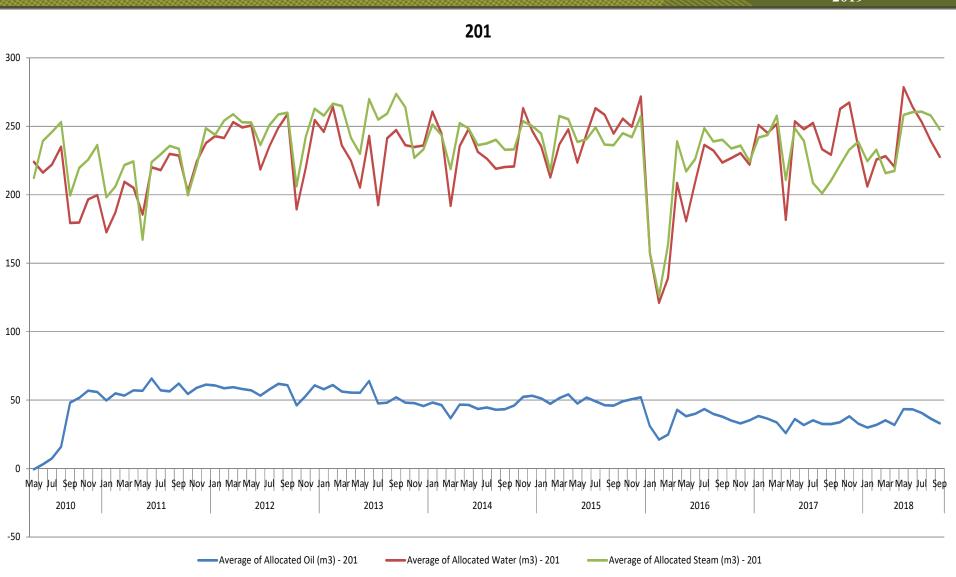
Pod One Pad 104 Production





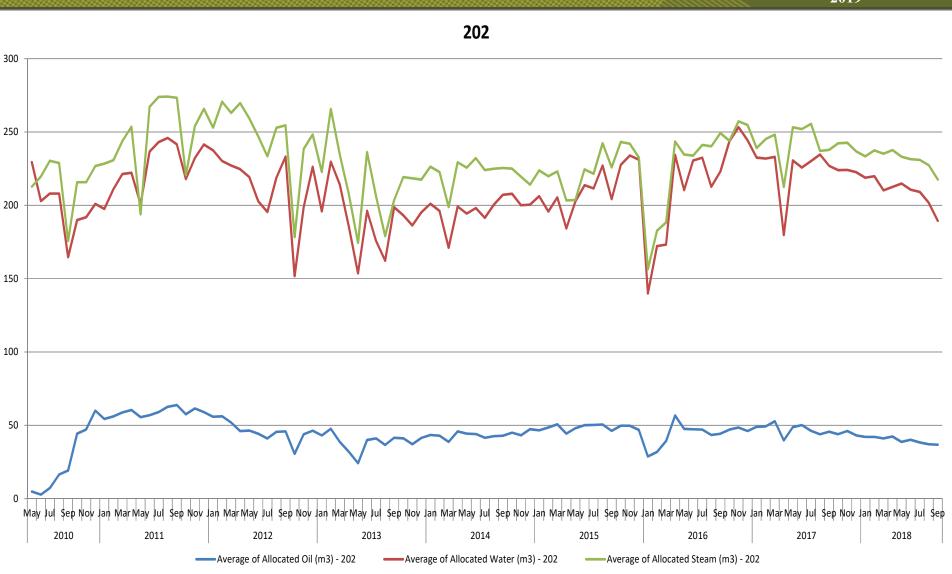
Algar - Pad 201 Production





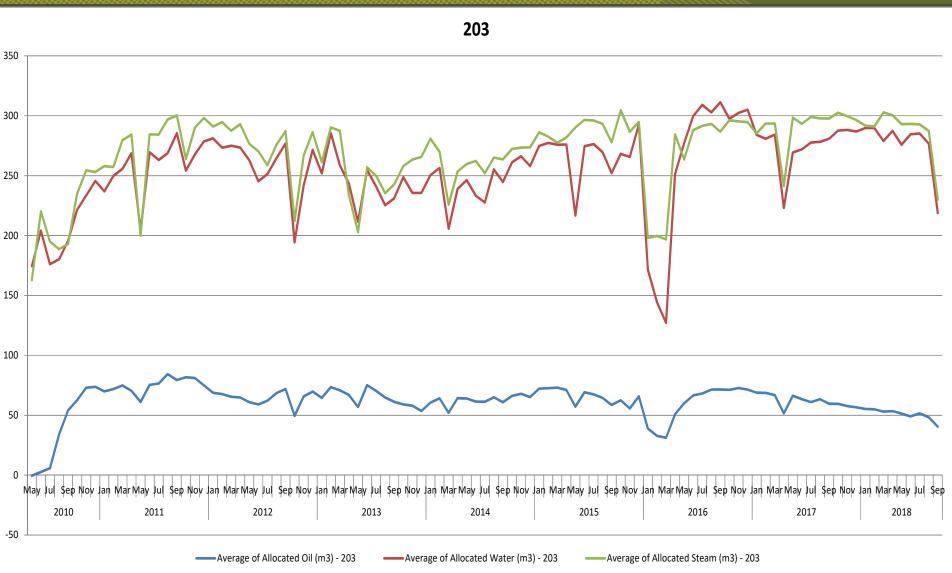
Algar Pad 202 Production





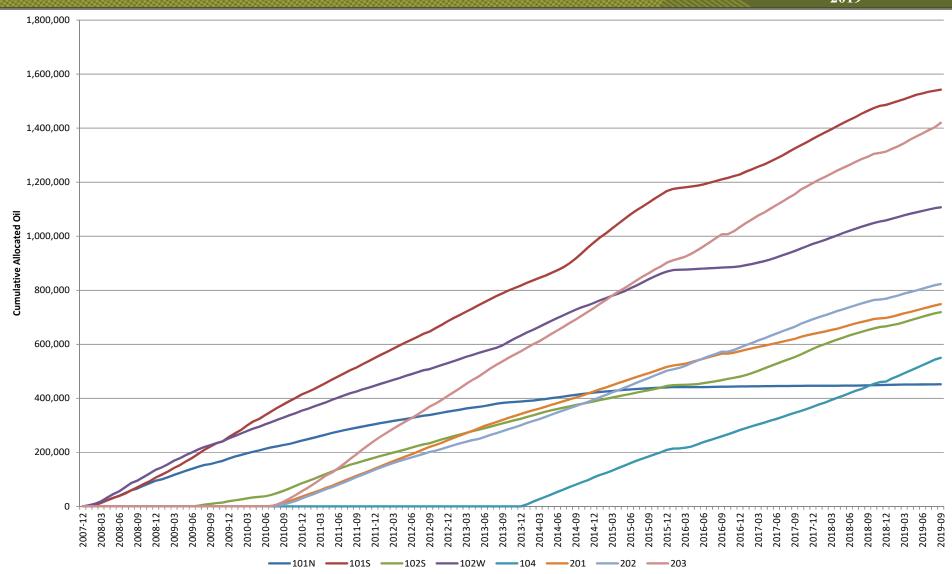
Algar Pad 203 Production





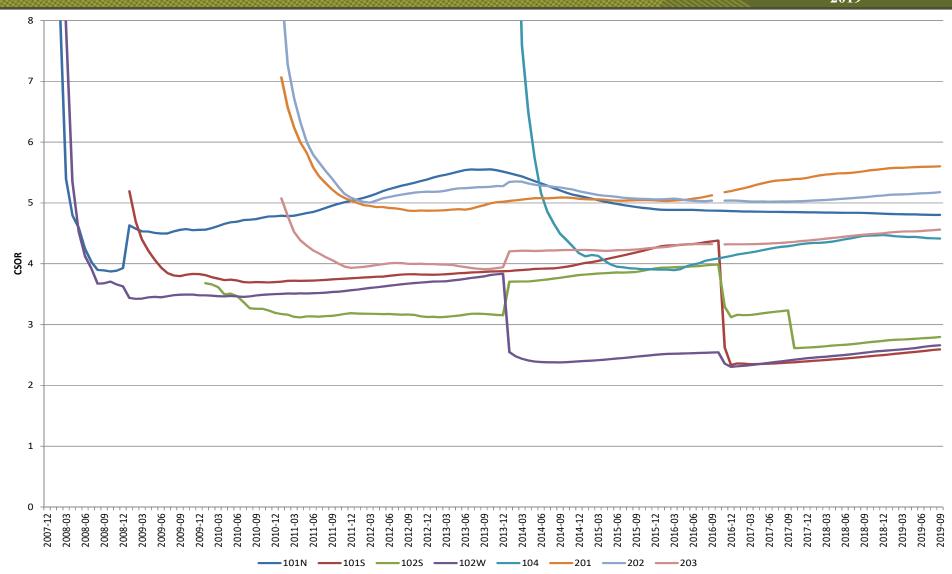
Great Divide Performance - Cumulative Production by Pad





Great Divide Performance -Cumulative Steam to Oil Ratio by Pad





Pod One Performance - Well Summary



Well Pad	Well Pair	Date	Months On	Cum Oil m3	Cum Steam m3	Oil Rate (m3/day)	CSOR	Lift	Comments	
101N	101-01	Sep-2019	101	90,674	436,980	0.00	4.82	Rod Pump	North Pad, Channel Edge, Shut-in Jan 2016	
101N	101-02	Sep-2019	101	78,888	429,657	0.00	5.45	Rod Pump	North Pad, Channel Edge, Shut-in Jan 2016	
101N	101-03	Sep-2019	100	65,631	331,677	0.00	5.05	Rod Pump	North Pad, Channel Edge, Shut-in Jan 2016	
101N	101-04	Sep-2019	145	116,611	465,679	8.14	3.99	Rod Pump	North Pad, Channel Edge, Blowdown	
101N	101-05	Sep-2019	111	105,458	417,136	0.00	3.96	PC Pump	North Pad, Channel Edge, Shut-in Oct 2016	
1015	101-06	Sep-2019	145	139,602	711,946	9.17	5.10	Rod Pump	Average Well, Channel Edge	
1015	101-07	Sep-2019	145	131,722	807,802	9.76	6.13	Rod Pump	Average Well, Channel Edge	
1015	101-08	Sep-2019	145	260,668	1,082,664	8.58	4.15	Rod Pump	Good Well in Good Pay	
1015	101-09	Sep-2019	145	173,394	874,398	4.34	5.04	Rod Pump	Good Well in Good Pay	
1015	101-10	Sep-2019	145	213,711	998,958	0.00	4.67	Rod Pump	Good Well in Good Pay	
1015	101-11	Sep-2019	126	224,891	1,118,116	11.80	4.97	ESP	Good Well in Good Pay	
1015	101-INF07	Sep-2019	49	40,000	6,268	11.12	0.16	Rod Pump	Good Well in Good Pay	
1015	101-INF08	Sep-2019	61	80,406	917	25.56	0.01	Rod Pump	Good Well in Good Pay	
1015	101-INF09	Sep-2019	63	68,173	3,369	22.70	0.05	Rod Pump	Good Well in Good Pay	
1015	101-INF10	Sep-2019	63	54,619	9,985	12.66	0.18	Rod Pump	Good Well in Good Pay	
1015	101-INF11	Sep-2019	61	57,663	2,433	0.00	0.04	Rod Pump	Good Well in Good Pay, Shut-in Sept 2019	
1015	101-INF12	Sep-2019	62	96,878	1,184	23.11	0.01	Rod Pump	Good Well in Good Pay	

Pod One Performance Well Summary (2)



Well	Well Pair	Date	Months On	Cum Oil m3	Cum Steam m3	Oil Rate	CSOR	Lift	Comments
Pad			1.4=	4.5= 00.4	- 40.400	(m3/day)			
102W	102-01	Sep-2019	145	167,804	748,420	11.66	4.46	Rod Pump	Average Well, Crosses Channel
102W	102-02	Sep-2019	145	142,625	745,019	8.06	5.22	Rod Pump	Average Well, Crosses Channel
102W	102-03	Sep-2019	145	145,648	770,212	10.36	5.29	Rod Pump	Average Well, Crosses Channel
102W	102-04	Sep-2019	145	165,839	793,237	8.30	4.78	Rod Pump	Average Well, Crosses Channel
102W	102-05	Sep-2019	145	165,949	938,569	8.39	5.66	Rod Pump	Average Well, Crosses Channel
102S	102-12	Sep-2019	126	299,796	1,198,645	46.17	4.00	ESP	Good Well in Good Pay
102S	102-13	Sep-2019	114	132,210	651,223	9.88	4.93	ESP	Average Well, Channel Edge
102S	102-14	Sep-2019	113	160,696	749,041	38.62	4.66	ESP	Average Well, Channel Edge
102W	102-INF02	Sep-2019	74	49,721	613	11.51	0.01	Rod Pump	Average Well, Crosses Channel
102W	102-INF03	Sep-2019	75	78,652	434	25.29	0.01	Rod Pump	Average Well, Crosses Channel
102W	102-INF04	Sep-2019	75	75,062	975	20.22	0.01	Rod Pump	Average Well, Crosses Channel
102W	102-INF05	Sep-2019	75	61,716	1,083	20.86	0.02	Rod Pump	Average Well, Crosses Channel
102W	102-INF06	Sep-2019	53	61,439	1,560	35.25	0.03	Rod Pump	Good Well in Good Pay
102W	102-INF13	Sep-2019	48	51,585	2,438	25.64	0.05	Rod Pump	Good Well in Good Pay
102W	102-INF14	Sep-2019	33	71,623	2,145	79.64	0.03	Rod Pump	Good Well in Average Pay
104S	104-03	Sep-2019	73	185,501	723,060	111.44	3.90	ESP	Good Well, Thief Zone Impacts
104S	104-04	Sep-2019	73	153,697	586,441	108.12	3.82	ESP	Good Well, Thief Zone Impacts
104S	104-05	Sep-2019	73	124,118	544,180	69.14	4.38	ESP	Good Well, Thief Zone Impacts
104S	104-06	Sep-2019	73	78,921	365,555	54.74	4.63	ESP	Average Well, Thief Zone Impacts
104S	104-INF04	Sep-2019	0	0	0	0.00	N/A	N/A	New Infill Well
104S	104-INF05	Sep-2019	0	0	0	0.00	N/A	N/A	New Infill Well
104S	104-INF06	Sep-2019	0	0	0	0.00	N/A	N/A	New Infill Well

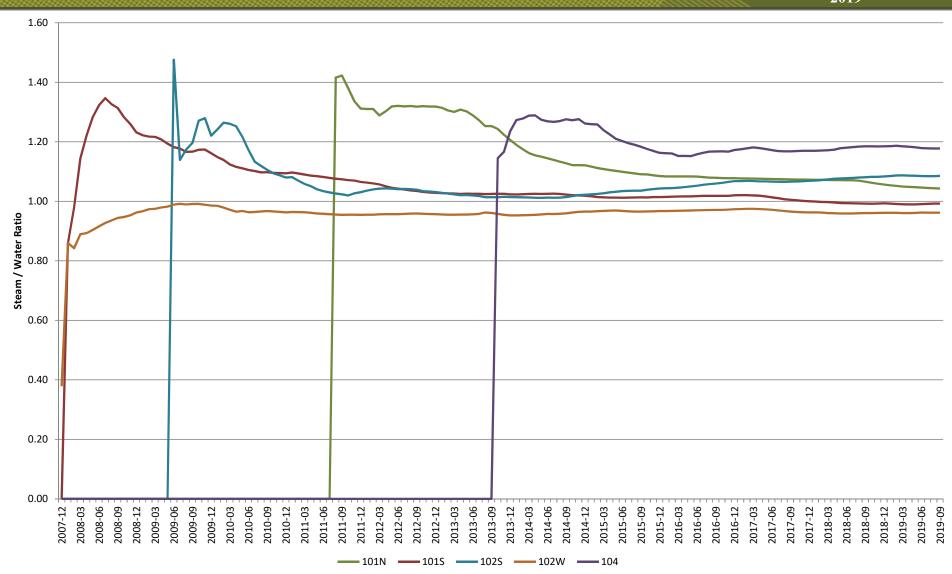
Algar Performance - Well Summary



Well	Well Pair	Date	Months	Cum Oil	Cum	Oil Rate	CSOR	Lift	Comments
Pad	201.01	0010	On	m3	Steam m3		4.00	0 1:0	
201	201-01	Sep-2019	113	238,230.1		41.39	4.93	Gas Lift	Good Well, Good Pay, BW
201	201-02	Sep-2019	113	236,240.9	1,067,115	40.15	4.52	Gas Lift	Good Well, Good Pay, BW
201	201-03	Sep-2019	113	84,883.1	506,858	27.76	5.97	Gas Lift	Intermittent, Sand Issues, BW
201	201-04	Sep-2019	113	95,433.8	575,375	29.40	6.03	Gas Lift	BW / Evaluating Pump Strategy
201	201-05	Sep-2019	113	85,623.5	541,367	23.10	6.32	Gas Lift	BW / Evaluating Pump Strategy
202	202-01	Sep-2019	113	106,506.2	207,702	30.53	1.95	Gas Lift	Edge Well
202	202-02	Sep-2019	113	187,327.8	896,522	30.54	4.79	Gas Lift	Good Well in Good Pay
202	202-03	Sep-2019	113	119,665.8	696,676	15.80	5.82	Gas Lift	Average Well, BW
202	202-04	Sep-2019	113	126,950.8	723,181	30.63	5.70	Gas Lift	Average well, BW
202	202-05	Sep-2019	113	156,929.8	881,723	27.32	5.62	Gas Lift	Good Well in Good Pay
202	202-01-1	Sep-2019	78	119,547.9	780,213	25.49	6.53	Gas Lift	Good Well in Good Pay
203	203-01	Sep-2019	113	208,184.0	836,141	35.47	4.02	Gas Lift	Average Well,Good Pay, Edge
203	203-02	Sep-2019	113	231,252.3	889,566	52.74	3.85	Gas Lift	Good Well in Good Pay
203	203-03	Sep-2019	113	204,193.7	902,365	49.97	4.42	Gas Lift	Good Well in Good Pay
203	203-04	Sep-2019	113	220,863.8	913,396	46.03	4.14	Gas Lift	Good Well in Good Pay
203	203-05	Sep-2019	113	236,981.0	1,015,922	41.44	4.29	Gas Lift	Good Well in Good Pay
203	203-06	Sep-2019	113	180,213.1	875,681	37.43	4.86	Gas Lift	Average Well, Near Edge
203	203-07	Sep-2019	113	121,944.8	683,745	31.95	5.61	Gas Lift	Edge Well, Delayed Start Up
203	203-INF02	Sep-2019	1	3,142.7	34	104.76	0.01	Rod Pump	New Infill Well
203	203-INF03	Sep-2019	1	1,084.3	285	36.14	0.26	Rod Pump	New Infill Well
203	203-INF04	Sep-2019	1	1,198.9	522	39.96	0.44	Rod Pump	New Infill Well
203	203-INF05	Sep-2019	1	1,084.9	9	36.16	0.01	Rod Pump	New Infill Well
203	203-INF06	Sep-2019	1	1,650.1	118	55.00	0.07	Rod Pump	New Infill Well

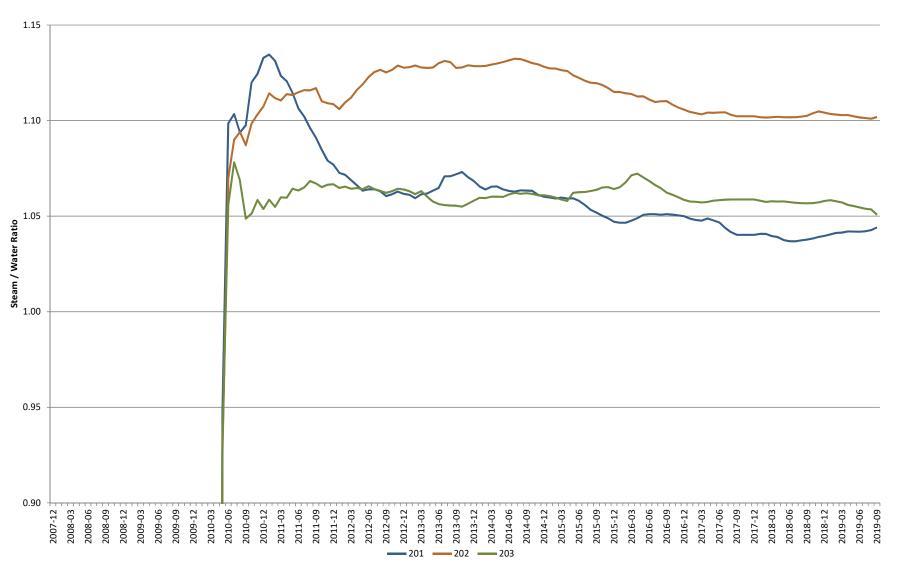
Pod One - Water Balance Cumulative Steam In / Water Produced





Algar - Water Balance <u>Cumulative Steam In / Water Produced</u>





Pod One -Recoverable Bitumen By Pad





	Pad	Area	Average Porosity (%)	Average So (%)	Average Net Pay (m)	Pad OBIP (e³m³)	To Date Recovery (e³m³)	To Date Recovery (%)	Estimated Ultimate Recovery (%)	Estimated Ultimate Recovery (e³m³)
	101N	29.6	33	74	18.0	1,300	457	35.2	34.9	454
	1015	32.6	33	80	20.0	1,720	1,542	89.6	87.0	1,496
-	102W	31.6	33	80	17.0	1,420	1,114	78.5	75.0	1,065
	102S	32.7	33	80	19.0	1,640	716	43.7	80.0	1,312
	104	70.3	33	80	21.5	4,030	542	13.5	80.0	3,224

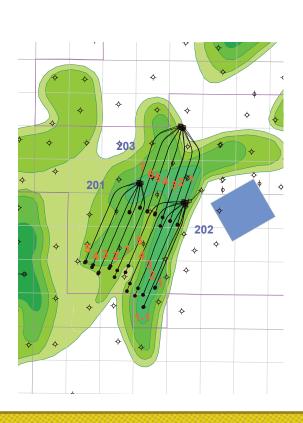
Notes:

- 1. Pad 101N only 101-04 and 101-05 are producing
- 2. Additional of estimated infill recoveries of approximately 8% for Pads 101S, 102W, 102S, and 104
- 3. Estimated Pad Recovery is based on the basic SAGD process
- 4. Pad 101N injectors were plugged back approximately 1/3 back from well toes
- 5. Initial Pad recoveries are proving to be on the conservative side

Algar -

Recoverable Bitumen by Pad





Pad	Area	Average Porosity (%)	Average So (%)	Average Net Pay (m)	Pad OBIP (e³m³)	To Date Recovery (e³m³)	To Date Recovery (%)	Estimated Ultimate Recovery (%)	Estimated Ultimate Recovery (e³m³)
201	47.1	33	75	19.0	1,930	740	38.4	75.0	1,448
202	45.6	33	75	18.0	1,890	866	45.8	80.0	1,512
203	56.7	33	75	22.0	3,040	1,412	46.4	80.0	2,432

Notes:

- Pad 203 has completed SAGD+ on a trial basis.
 Reserves will be adjusted when the commercial project begins. An additional recovery between 5 to 8% of the OBIP is estimated.
- 2. Estimated Pad Recovery is based on the basic SAGD process.





Pod One Plant





Algar Plant





Pod One Facilities



Key Points

Design Capacity ~ 1,600 m³/day bitumen

Steam Generation: Drum boilers

Operating pressure 6,300 kPa

Deliver 4,300 m³/day steam @ 98% + Quality

Treating: Diluent addition

Water Recycle: IGF, WS Filter, Two vertical tube falling film evaporator towers

Waste Water: Waste water shipped to Algar 2nd Stage Evaporators

Source water: 3 operating source water wells in the Lower Grand Rapids formation, 1 other source water well approved

Algar Facilities



Key Points

Design Capacity ~ 1,600 m³/day bitumen

Steam Generation: Drum boilers

Operating pressure 6,700 kPa

Deliver 4,800 m³/day steam @ 98% + Quality

Treating: Diluent addition

Water Recycle: IGF, WS Filter, Two vertical tube falling film evaporator towers

Waste Water: All water shipped from facility to approved disposal sites

Source water: 3 operating source water wells in the Lower Grand Rapids formation, 1

other source water well approved

Great Divide Plant Modifications



Pod One

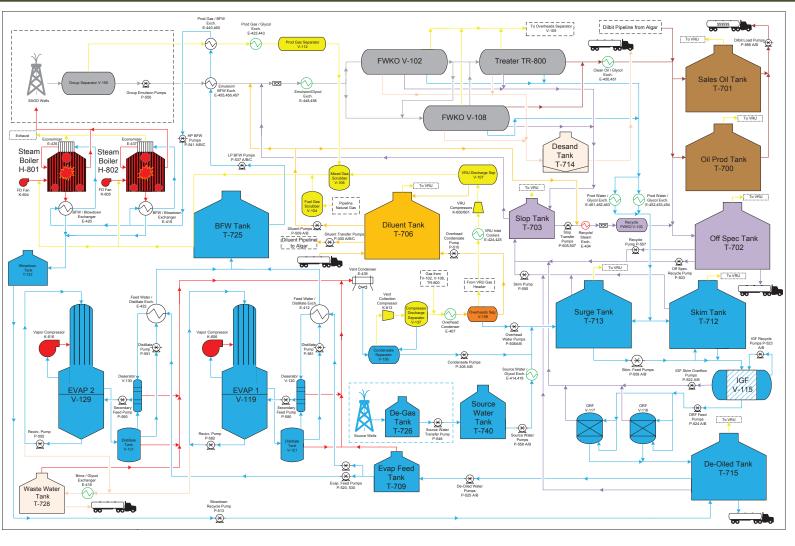
- Upgrade V-109 overhead separator
- Upsized two produced water exchangers
- Conversion of production well P10 from ESP to Rod Pump

Algar

- Addition of five infill wells at Pad 203
- Addition of one new produced water exchanger

Pod One Process Schematic

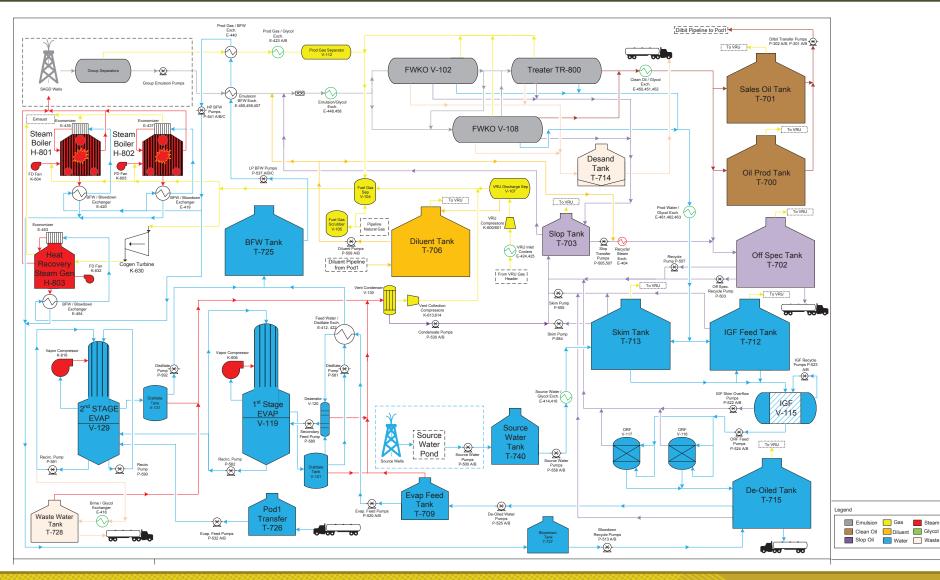






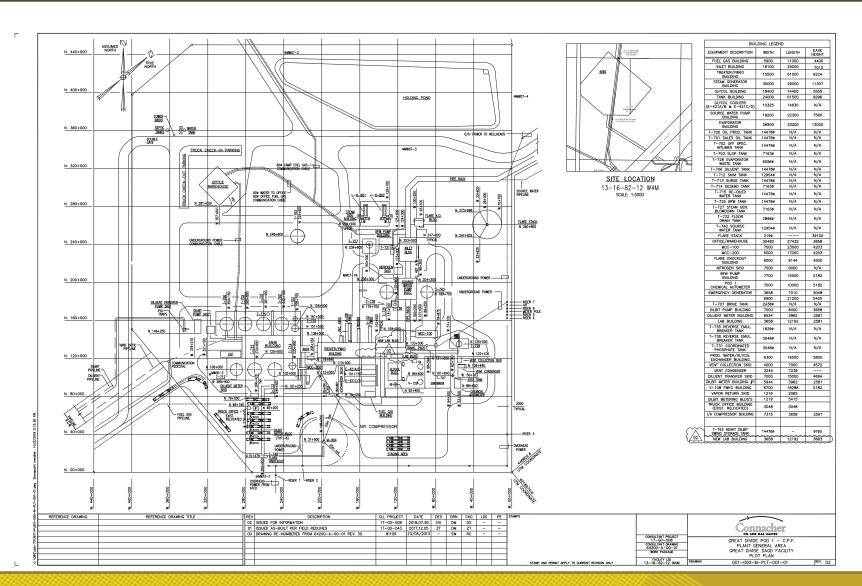
Algar Process Schematic





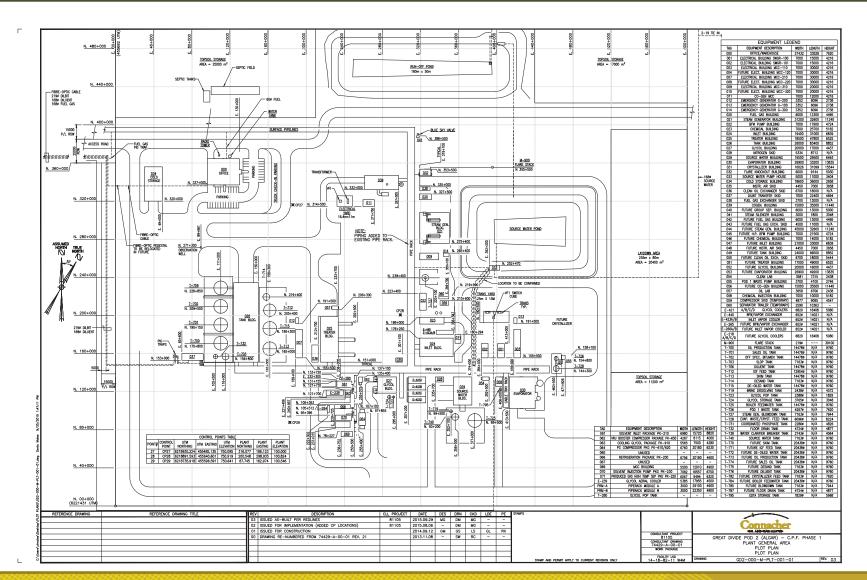
Pod One Plant Layout





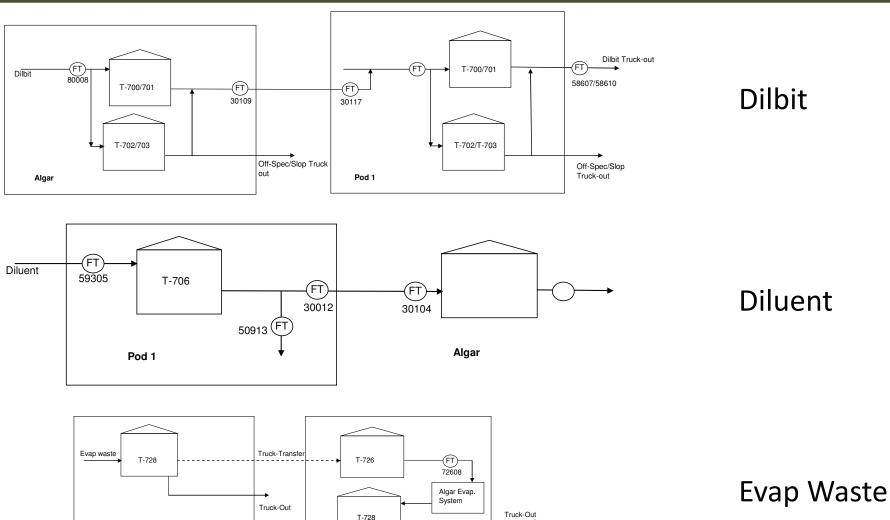
Algar Plant Layout





Pod One and Algar Integration





Algar

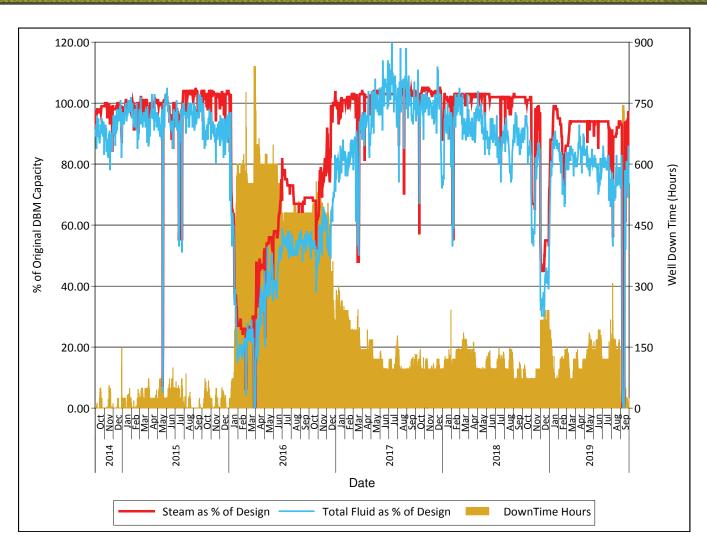
Pod 1





Pod One CPF Performance





The reliability considers the two steam Boilers at the plant.

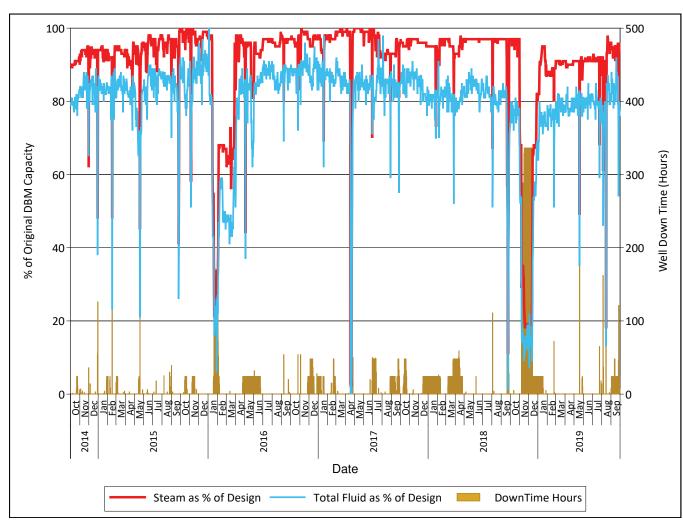
For the period October 1, 2018 to September 30, 2019 the steam plant has averaged 86.8% of the original design basis (4,320 m3 /day) and 74.6% of the designed total fluid capacity (5,920 m3/day).

This performance is lower compared to the previous 12 months. Which had a steam generation of 101.7% and a total fluid throughput of 92.6% of plant design capacity.

Downtime Hours is the reported downtime for the Well Pairs.

Algar CPF Performance





The reliability considers the two steam Boilers at the plant. The Cogen steam is not included.

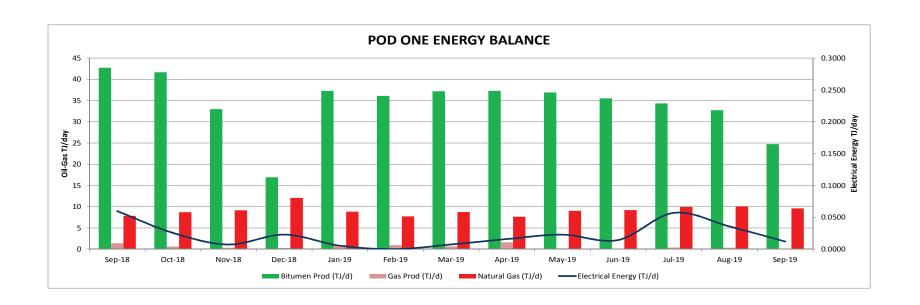
For the 12 months from October 1 2017, to the of September 30, 2018 the steam plant output has averaged 84.1% of the original design basis (4800 m3 /day) and 70.4% of the designed total fluid handling capacity (6400 m3/day).

This performance is lower compared to the previous 12 months which had a steam generation of 96.4% and total fluid throughput of 81.8% of plant design capacity.

Downtime Hours is the reported downtime for the Well Pairs.

Pod One Energy Balance

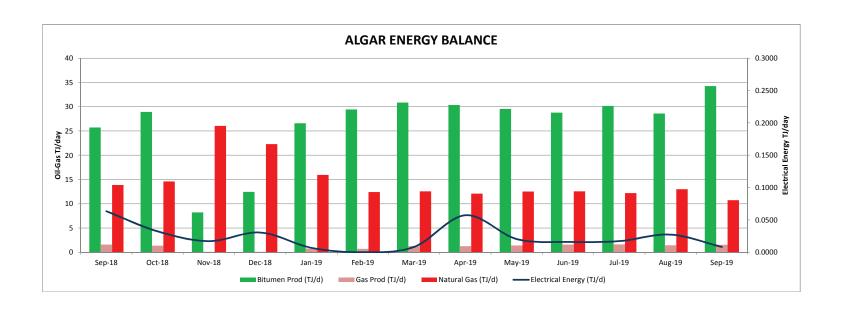




Greenhouse Gas Emissions Reported for December, 2017 = 237,333 t CO₂ equivalent

Algar Energy Balance





Greenhouse Gas Emissions Reported for December, 2017 = 288,064 t CO_2 equivalent

Algar Co-Generation Facility



- Designed to produce 13.1 MW electricity from GT and 588 m³/d of steam from the HRSG
- Horse River sub-station on line June 2011
- Running near capacity with power distributed to both Algar and Pod One
- Steam being used at Algar





Changes to MARP



Pod One

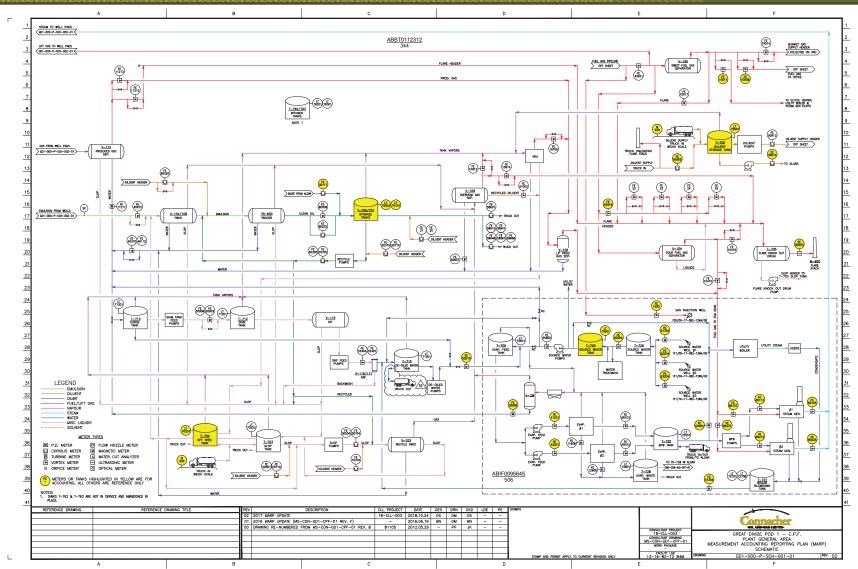
- 1. Removed MARP steam meters from Pad 101 infill wells (INF07, INF08, INF09, INF10, INF11, INF12). Steam phase on these wells is completed.
- 2. Changed 101-P8/P9/P10 from ESP to PD.
- 3. MARP steam meters at Pad 102 on wells INF-02/03/04/05/06/13/14 are not in service anymore. Changed 102-P4 and P5 from ESP to PD.

Algar

1. Added five infill wells at Pad 203 and associated MARP steam meters.

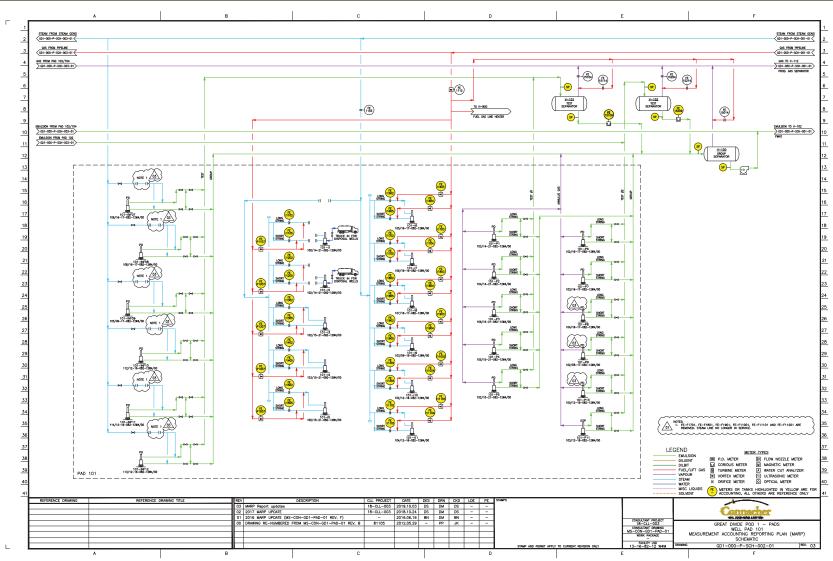
Pod One MARP - CPF





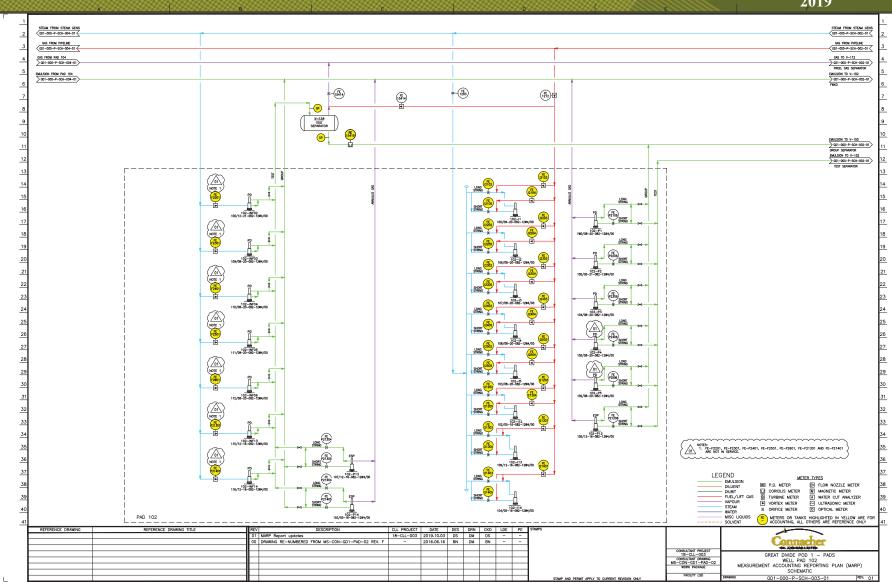
Pod One MARP - Pad 101





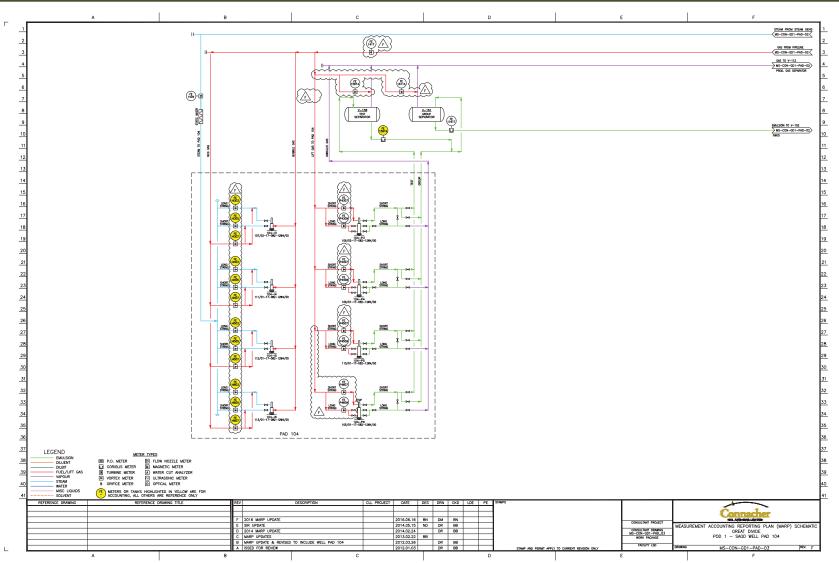
Pod One MARP - Pad 102





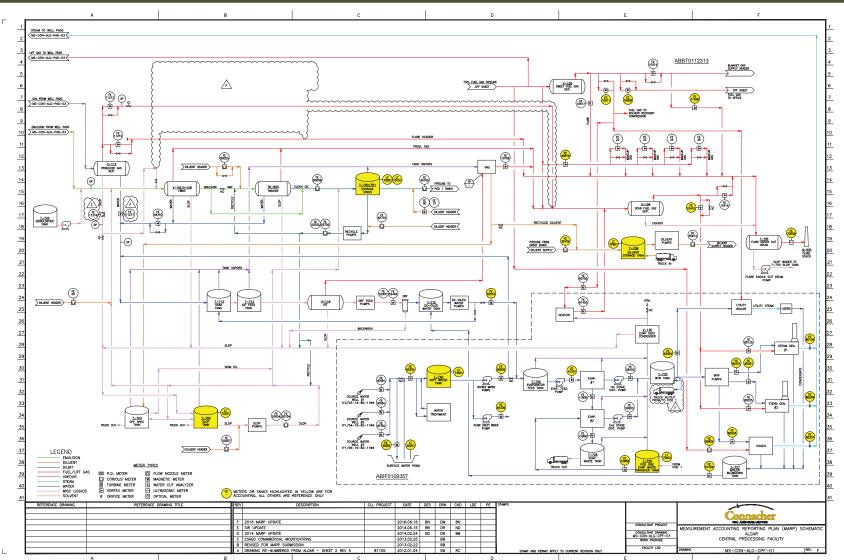
Pod One MARP - Pad 104





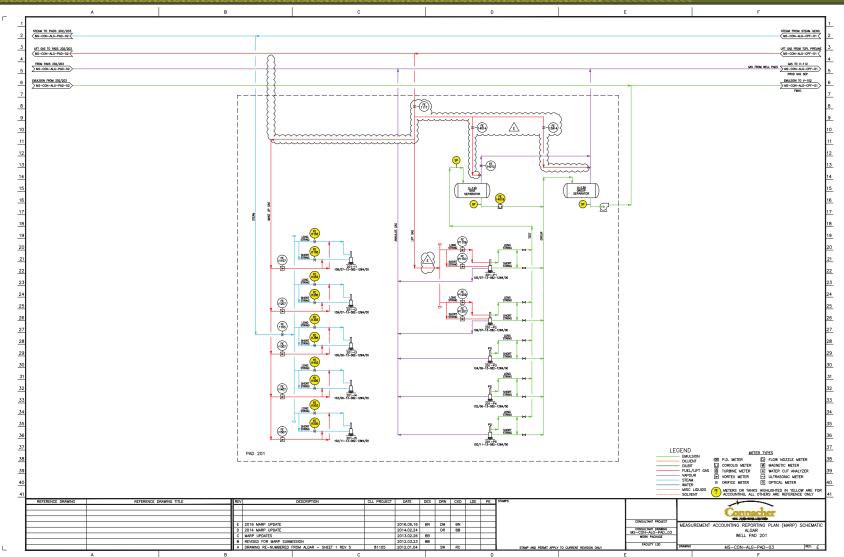
Algar MARP - CPF





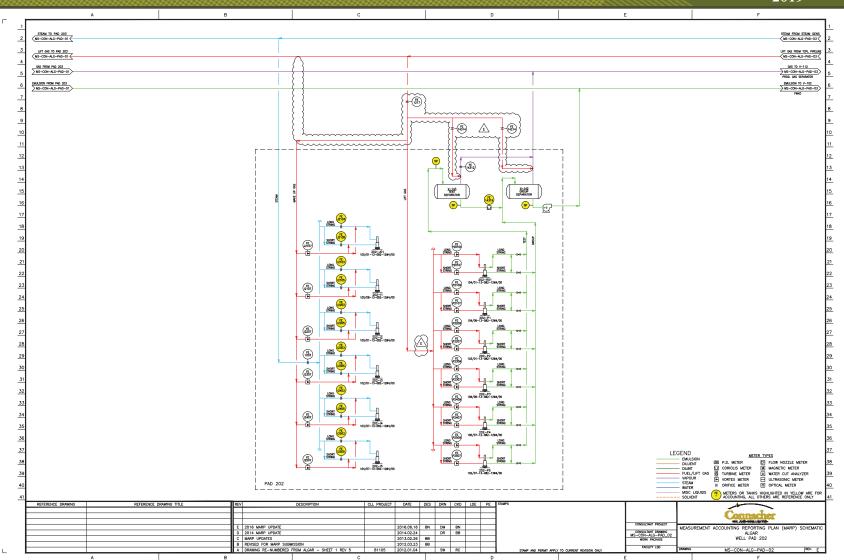
Algar MARP - Pad 201





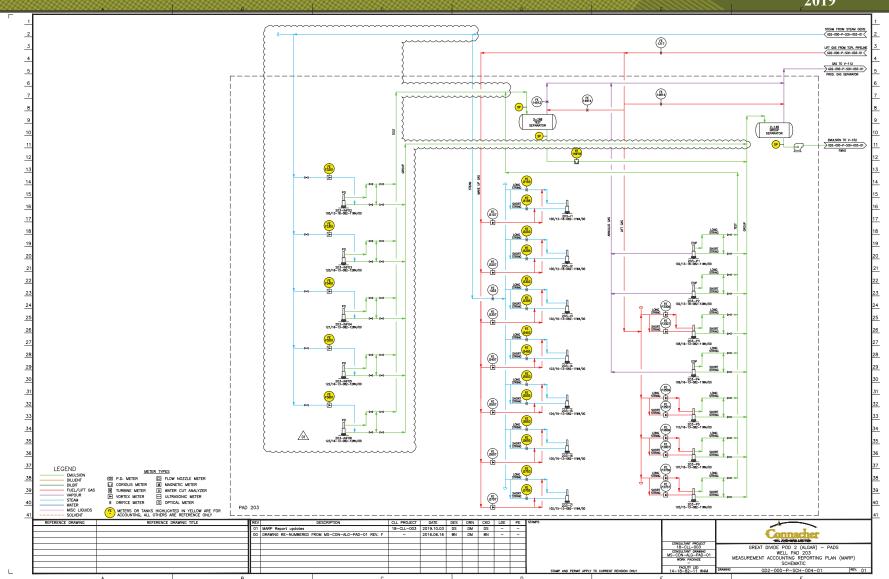
Algar MARP - Pad 202





Algar MARP - Pad 203

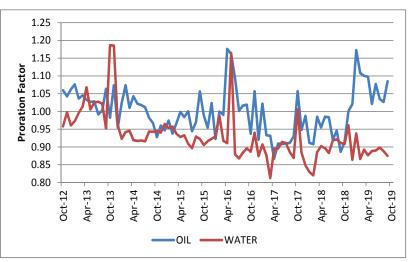




Pod One and Algar Proration Factors

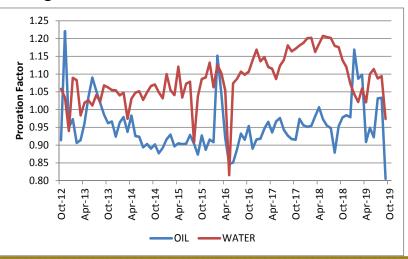


Pod One



Pod One uses manual oil cuts however procedures implemented 2012 are clearly showing improved results.

Algar



The proration factor at Algar is calculated from the interconnect pipeline volumes whereas the Pod One proration factor is calculated from truck receipts less the Algar pipeline volumes and is subject to typical truck measurement differences.



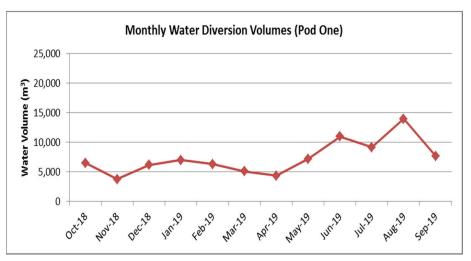


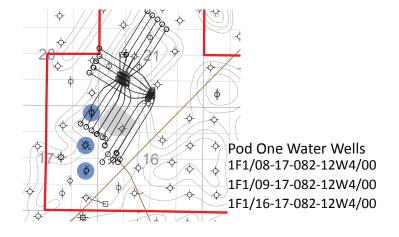
Source Water Wells - Pod One



Year	Pod One Water Withdrawals (m³/year)	Licenced Maximum Annual Diversion (m³/year)
2013	92,462	292,000
2014	134,309	292,000
2015	114,154	292,000
2016	156,313	292,000
2017	87,536	292,000
2018	123,428	292,000
2019	71,480	292,000

Water Act Licence 00240458-01-00				
Well Location	Production Interval (meters below grade)			
16-17-082-12 W4M	300 - 350			
09-17-082-12 W4M	300 - 350			
08-17-082-12 W4M	300 - 350			
02-17-082-12 W4M (standby)	324 - 330			



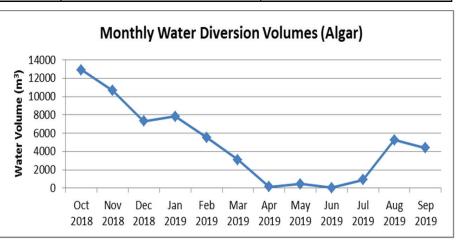


All wells use the Grand Rapids Formation for source water.

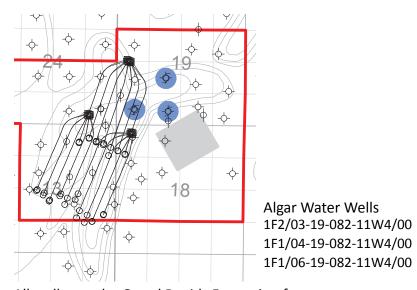
Source Water Wells - Algar



Year	Algar Water Withdrawals (m³/year)	Licenced Maximum Annual Diversion (m³/year)
2013	78,917	330,000
2014	52,916	330,000
2015	45,130	330,000
2016	68,956	330,000
2017	23,298	330,000
2018	52,710	330,000
2019	27,624	330,000



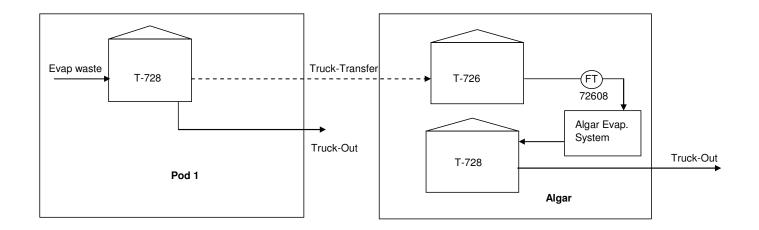
Water Act Licence 00240527-00-02				
Well Location	Production Interval (meters below grade)			
02-19-082-11 W4M standby	356 - 382			
03-19-082-11 W4M	349 - 382			
04-19-082-11 W4M	350 - 382			
06-19-082-11 W4M	347 - 382			



All wells use the Grand Rapids Formation for source water.

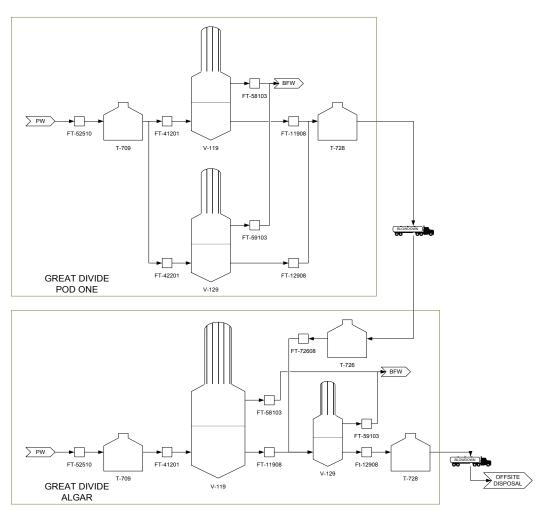
Evaporator Waste Integration





Integrated Water Recycle Scheme

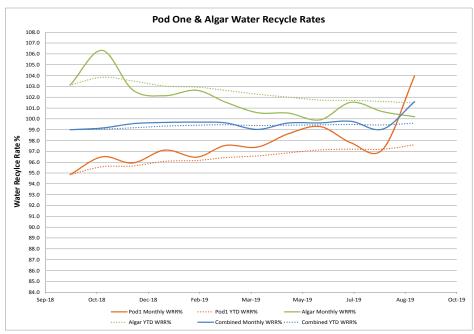




- Evaporators produce high quality boiler feed water efficiently while generating a highly concentrated brine for disposal.
- At Algar a second stage evaporator further concentrates both the Algar brine and a portion of the Pod One brine to improve water reuse and minimize disposal.
- Disposal concentrations are close to crystallizer performance.
- Chemical optimization has significantly improved evaporator reliability.

Water Recycle Ratio





Month	Pod1 Monthly WRR%	Pod1 YTD WRR%	Algar Monthly WRR%	Algar YTD WRR%	Combined Monthly WRR%	Combined YTD WRR%
Oct-18	94.9	94.9	103.1	103.1	99.0	99.0
Nov-18	96.5	95.6	106.3	103.8	99.2	99.1
Dec-18	95.9	95.7	102.7	103.5	99.6	99.2
Jan-19	97.1	96.1	102.1	103.0	99.7	99.3
Feb-19	96.5	96.2	102.6	102.9	99.7	99.4
Mar-19	97.5	96.4	101.6	102.6	99.6	99.5
Apr-19	97.4	96.6	100.6	102.3	99.0	99.4
May-19	98.6	96.9	100.5	102.0	99.6	99.4
Jun-19	99.3	97.1	99.9	101.7	99.6	99.4
Jul-19	97.8	97.2	101.5	101.7	99.8	99.5
Aug-19	97.2	97.2	100.7	101.6	99.1	99.4
Sep-19	104.0	97.6	100.2	101.5	101.6	99.6

- The series evaporator operation at Algar provides high recycle rates and improved reliability.
- The Algar operation accommodates waste from the parallel evaporators at Pod One and brine is shipped from Pod One to Algar.
- By treating part of the Pod One blow-down at Algar the average yearly water recycle ratio for both plants is approximately 99.6%.
- The increase in WRR% in September 2019 is attributed to the Pod One Plant turnaround.

Water Disposal and Directive 81 Compliance



Directive 81 Compliance						
Disposal Limit Actual Disposal						
Pod One	9.5%	3.2%				
Algar Great Divide	9.8%	0.0%				
Great Divide	9.6%	1.6%				

Pod One Water Volumes

Fresh Water Make-up: 104,621 m³ Produced Water: 1,294,745 m³ Disposal: 4,037 m³

Algar Water Volumes

Fresh Water Make-up: 46,232 m³ Produced Water: 1,393,012 m³ Disposal: 0 m³





Natural Gas Usage



Pod One Natural Gas Usage Summary

Production Month	Purchased Gas (e3m3)	Solution Gas (e3m3)	Consumed Gas (e3m3)	Flared and Vented (e3m3)
Oct-18	9,349	514	10,039	47
Nov-18	7,786	258	8,298	16
Dec-18	5,399	135	5,802	2
Jan-19	8,594	688	9,538	39
Feb-19	7,212	687	8,139	36
Mar-19	8,454	466	9,184	43
Apr-19	7,406	1,219	8,878	40
May-19	8,650	121	9,025	49
Jun-19	8,500	71	8,826	38
Jul-19	8,825	-181	8,890	52
Aug-19	8,580	-166	8,672	38
Sep-19	6,182	26	6,355	66

Algar Natural Gas Usage Summary

Production Month	Purchased Gas (e3m3)	Solution Gas (e3m3)	Consumed Gas (e3m3)	Flared and Vented (e3m3)
Oct-18	10,737	1,143	11,868	12
Nov-18	5,335	118	5,416	37
Dec-18	7,277	-128	7,139	10
Jan-19	10,864	592	11,443	13
Feb-19	9,354	522	9,859	16
Mar-19	9,912	1,005	10,915	3
Apr-19	9,394	965	10,354	5
May-19	9,463	1,103	10,554	12
Jun-19	9,264	1,216	10,477	3
Jul-19	9,412	1,252	10,639	25
Aug-19	9,509	1,122	10,611	20
Sep-19	9,435	1,170	10,600	4





Summary of Future Plans

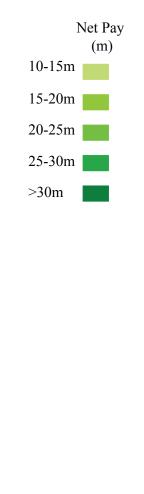


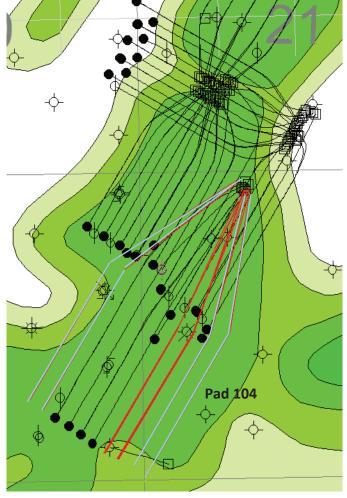
- Connacher has no major projects planned for the next 12 months that would require additional AER approvals
- Connacher has internal approval to drill nine infill wells on Pads 201, 202, and 203 currently scheduled for Q1 2020
- Connacher has internal approval to drill two well pairs on Pad 104 currently scheduled for Q2 2020
 - Connacher has approval for three major projects, summarized in the next slides:
 - Pod One Sustaining Production
 - Algar Expansion and Sustaining Production
 - Pod One Mini Steam Expansion
 - Algar SAGD+ Commercialization

Pod One Sustaining Production



- 10 Well Pair Approved for Pad 104 (Approval 10587H)
- Currently there are 4 existing Well Pairs at Pad 104



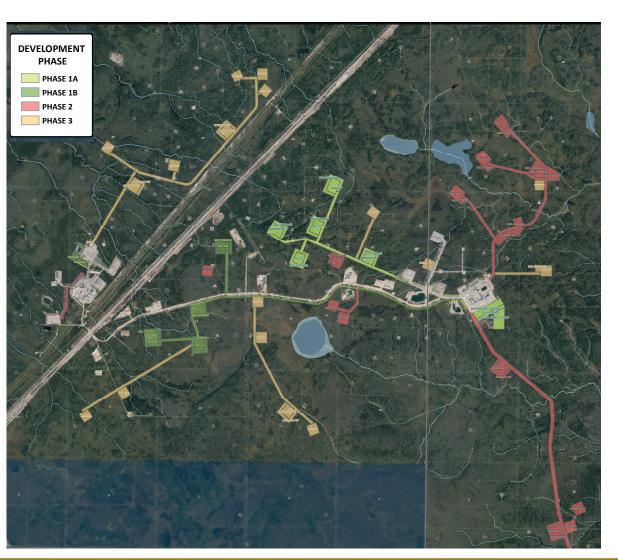


Approved

Approved

Great Divide SAGD Expansion Project





- EIA Deemed Complete
- Commercial Scheme Approval Received September, 2012
- EPEA Approval Amendment Received December, 2013
- Approved for expansion to 44,000 bbl/day

Algar Sustaining Production





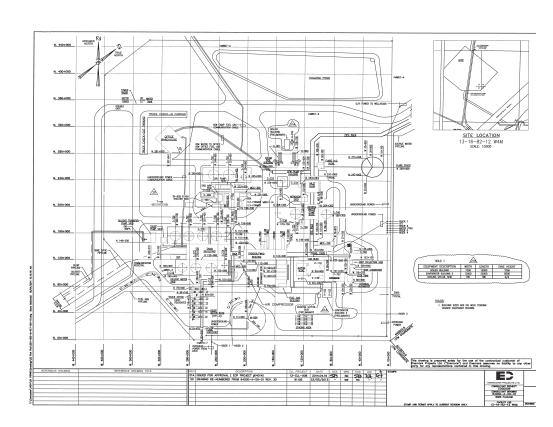
Near Future Development to include:

- Pad 232 (Phase 1A)
- Borrow Pit
- Utility Corridor

Pod One Mini Steam Expansion



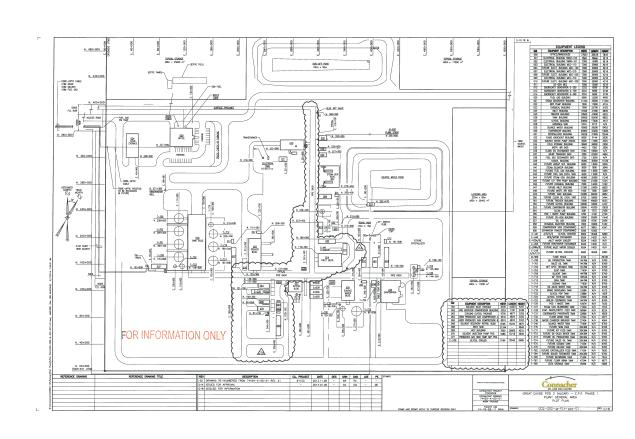
- Commercial Scheme Approval 10587P
- 500 t/d of steam
- Allows for 2 Well Pair at Pad 104
- Steam Generator (17.26 MW)
- 2 Evaporator Units
- No additional water allocation required



Algar SAGD+® Commercialization



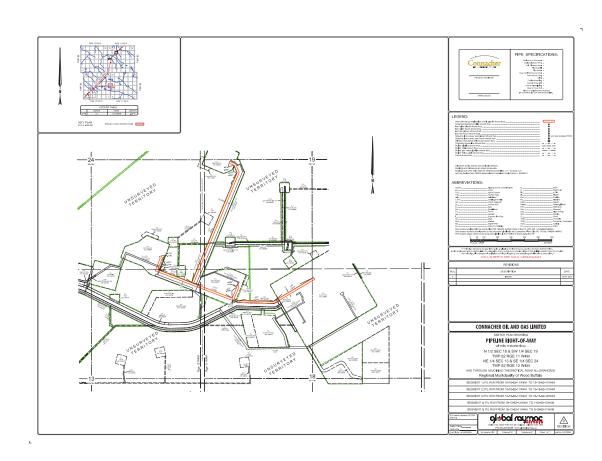
- Commercial Scheme Approval 10587K.
- Light hydrocarbon (solvent) and steam co-injection at all well pairs at Algar.
- Solvent to be recovered at facility for re-injection.
- EPEA 67(3) No objection received May, 2014.
- Construction began August,
 2014 but not yet completed.



Algar SAGD+® Commercialization



- Commercial Scheme Approval 10587K.
- 3 inch light hydrocarbon pipeline to all well pads.
- Installed on existing pipe rack.
- Construction completed but not yet commissioned.







Pod One Sulphur Emissions



Quarter	Average Sulphur Dioxide Emissions (t/day)
Q4-2018	0.21
Q1-2019	0.31
Q2-2019	0.19
Q3-2019	0.14

- Peak SO₂ emissions were 0.35 t/day: Jan 20, 2019
- Plant Total SO2 = Flared SO2 + Steam Generators' SO2 emissions
- No material changes in SO2 emissions from previous reporting period
- SO2 production is still well below emission limit (1.98 T/day)

Algar Sulphur Emissions

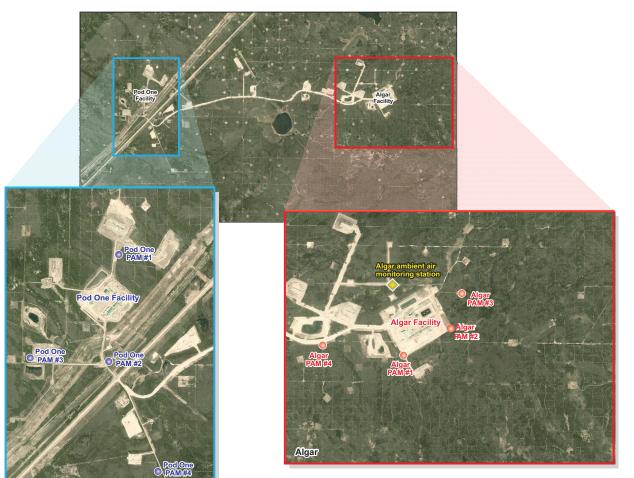


Quarter	Average Sulphur Dioxide Emissions (t/day)
Q4-2018	0.67
Q1-2019	1.10
Q2-2019	0.74
Q3-2019	0.76

- Peak SO₂ emissions were 1.35 t/day: Jan 23 and 31, 2019
- Plant Total SO2 = Flared SO2 + Steam Generators' SO2 emissions
- No material changes in SO2 emissions from previous reporting period
- SO2 production is still well below emission limit (1.98 T/day)

Ambient Air Quality Network





There are a total of 8 passive air monitoring stations at Pod One and Algar. These sites monitor for SO₂ and H₂S. For the reporting period there were no exceedances of the AAAQO

Connacher is required to complete continuous ambient air monitoring station for SO₂, H₂S and NO₂, as well as wind speed and wind direction. This monitoring is required 6 months per year. For the reporting period all measured concentrations were within the AAAQO's.

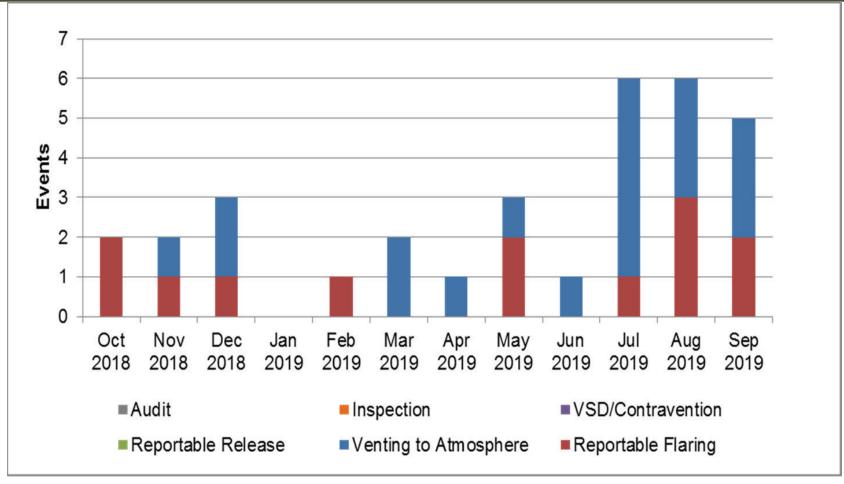
Pod One





Great Divide Compliance





Details of non-compliance events summarized above are available as an appendix to this presentation

Great Divide Applications / Authorizations



Approval Date	Authorization No.	Description
December 4, 2013	10587M	Pod One Full Field NCG Co-injection Scheme Approval
December 12, 2013	10587N	Pod One - Pad 101 and Pad 102 Infills (9) Scheme Approval
January 8, 2014	105870	SAGD+® Trail Pad 104 Scheme Approval
March 21, 2014	10587P	Mini-Expansion at Pod One Scheme Approval
Pending	Pending	EPEA Approval Amendment for Mini-Expansion at Pod One
June 10, 2014	F36853	Pod One Facility Licence Amendment
August 1, 2014	F40209	SAGD+® Commercial Project Facility Licence Amendment
August 13, 2014	56423	SAGD+® Commercial Project Solvent Pipeline Licence
September 10, 2014	10587Q	Algar - Pad 203 Infills (5) Scheme Approval
October 1, 2014	10587R	Algar Full Field NCG Co-injection Scheme Approval
Pending	Pending	Algar Water Act Licence 240527-00-00 Renewal
Pending	Pending	Pod One Water Act Licence 240458-01-00 Renewal
February 8, 2016	10587\$	Produced Water Disposal Operations at Pad 101N Approval
September 24, 2018	240008-01-00	EPEA Approval

Great Divide Inspections



Inspection Date	Agency	Location	Purpose	Inspection Result	Status
Oct 2018	AER	Algar CPF	Routine Inspection	Inspection ID 482419: Unsatisfactory. Deficiencies noted, corrective action s implemented and inspection closed.	Closed
June 2019	AER	12-19-082-11 W4M	Routine Inspection	Inspection ID 488690: Satisfactory	Closed
June 2019	AER	12-14-082-11 W4M	Inspection in response to spill	Inspection ID 488841: Satisfactory	Closed
August 2019	AER	Multiple Pipelines	Routine Inspection	Inspection ID: 492649 Satisfactory, with RFIs Inspection IDs: 492650, 492651, 492652: Satisfactory	Closed
September 2019	AER	Pod One SAGD Facility Algar SAGD Facility Multiple Wellsites	Routine Inspection	Inspection IDs: 493434, 493436, 493440, 493441, 493444: Satisfactory, with RFIs Inspection IDs: 493442, 493443, 493445, 493446, 493447, 493448, 493449 Satisfactory	Closed

Details of facilty inspections summarized above are available as an appendix to this presentation

Great Divide Audits



Period	Agency	Location	Purpose	Result	Status

No audits to report during reporting period.

Great Divide Voluntary Self Disclosures



Period	Approval #	Location	Description	Status

No voluntary self disclosures to report during reporting period.

Great Divide Monitoring Programs



Connacher currently implements the following monitoring programs at the Great Divide Project:

- Groundwater monitoring program;
- Ambient air monitoring program;
- Industrial wastewater & Industrial runoff monitoring program;
- Soil monitoring program; &
- Wildlife monitoring program.

No material developments or changes to EPEA compliance monitoring programs





Additional Material Attached to Submission



<u>Additional Material Attached to Submission:</u>

Energy Usage & Balance for Algar & Great Divide

Electrical Use at Pod One & Algar

Connacher Heave Monitoring Data

Pump Runlife Histories

Observation Well Pressure and Temperature Data

Production and Injection Well Pressure and Temperature Data

Great Divide Regulatory Compliance Table

Great Divide Summary of Non-compliance Events and VSDs





Bitumen Reserves and Resources

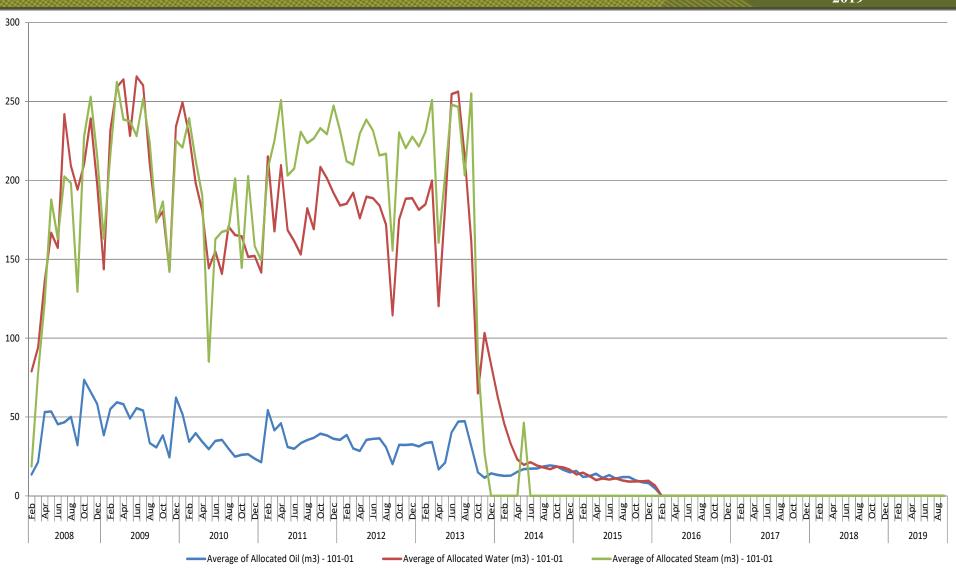


- 1)Proved reserves are those reserves that can be estimated with a high degree of certainty to be recoverable. It is likely that the actual remaining quantities recovered will exceed the estimated proved reserves.
- 2)Probable reserves are those additional reserves that are less certain to be recovered than proved reserves. It is equally likely that the actual remaining quantities recovered will be greater or less than the sum of the estimated proved plus probable reserves.

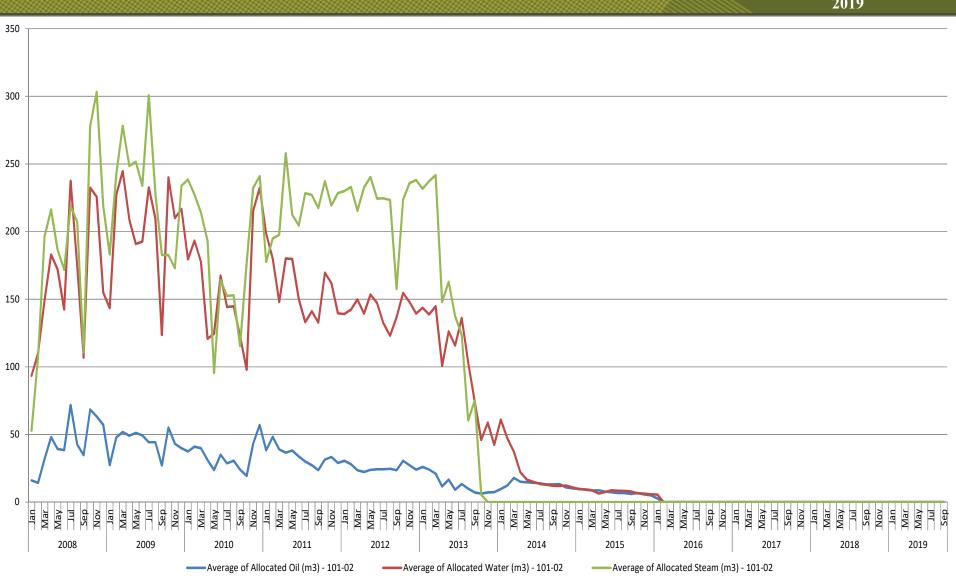




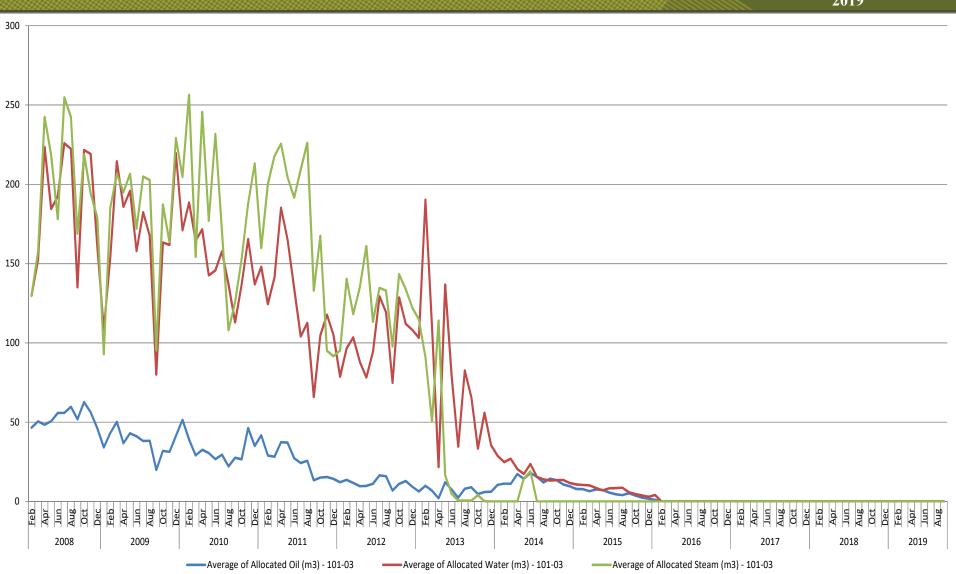




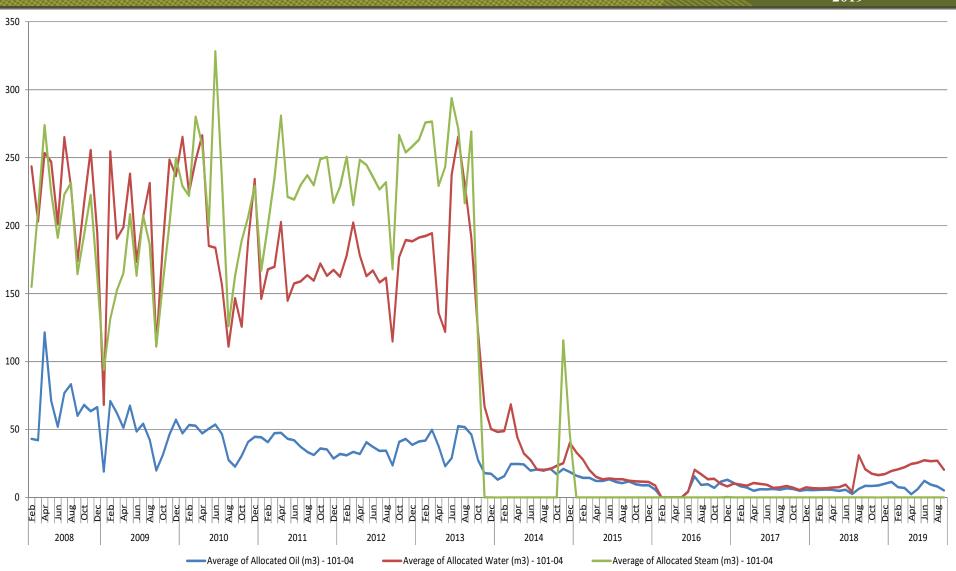




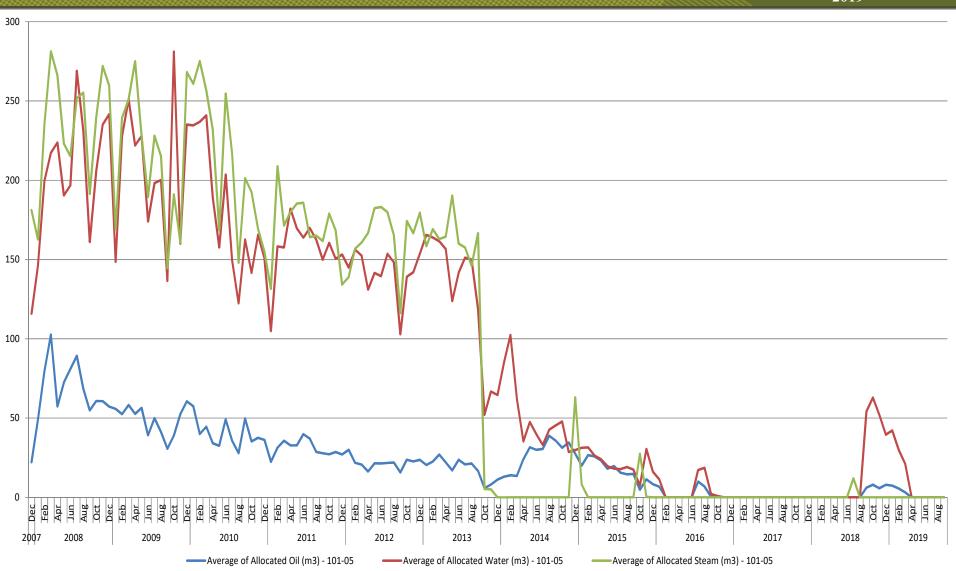




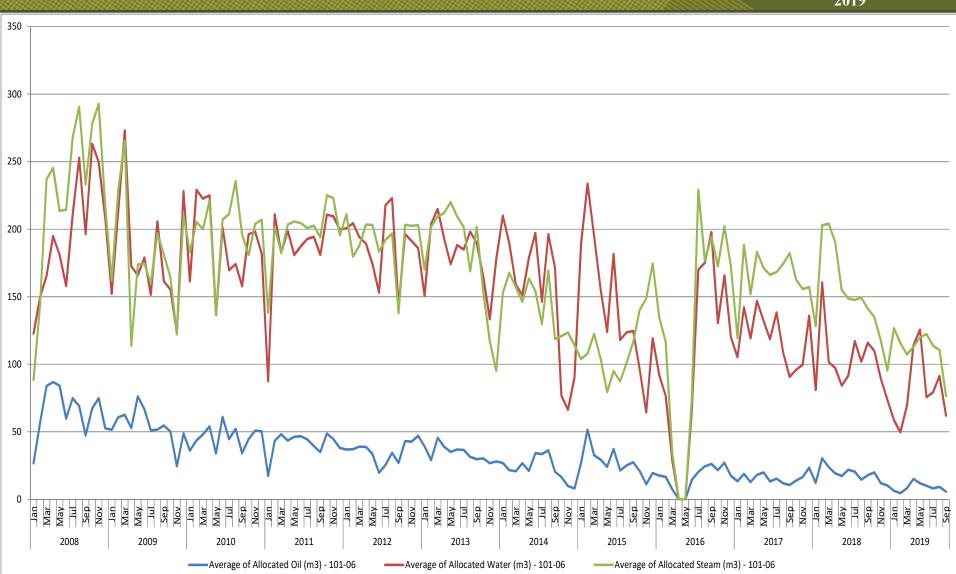




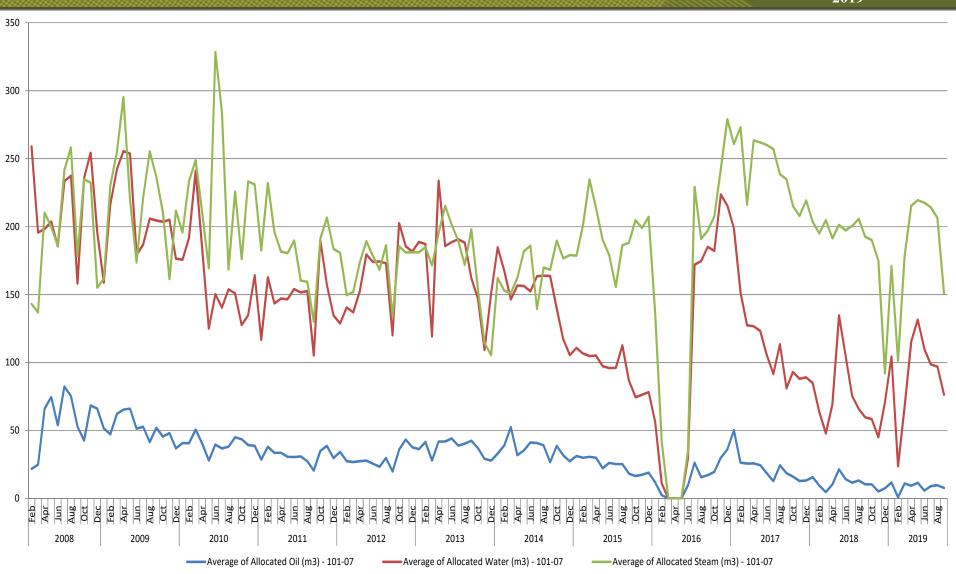




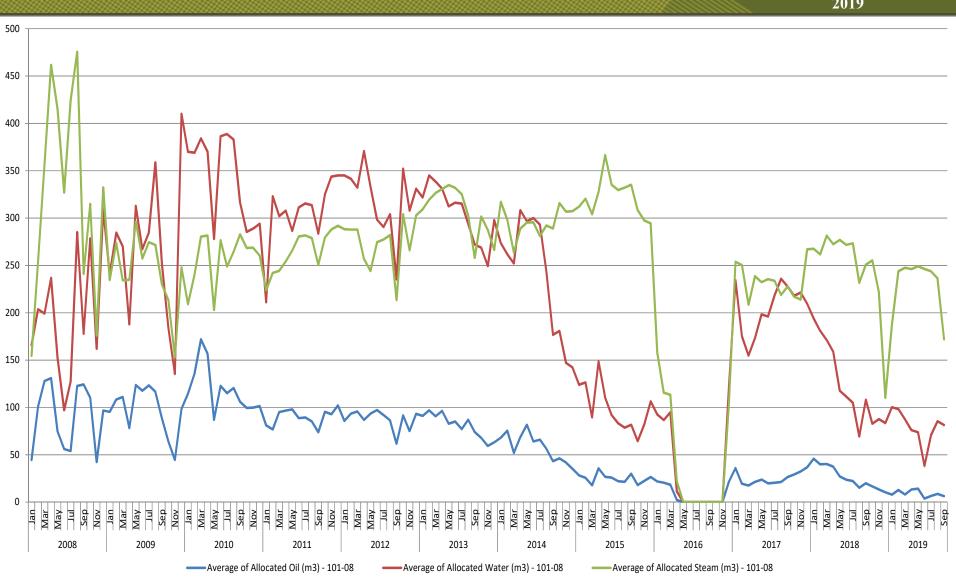




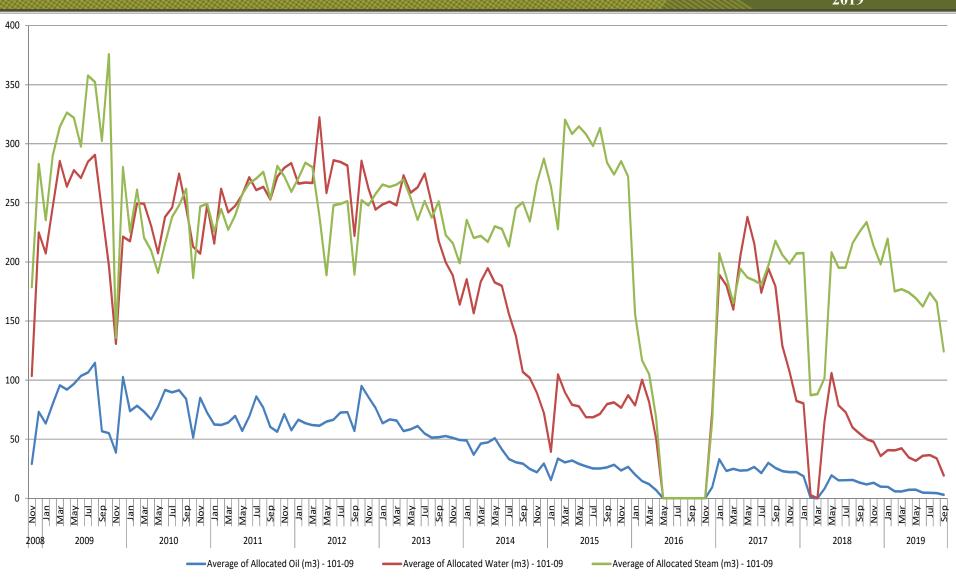




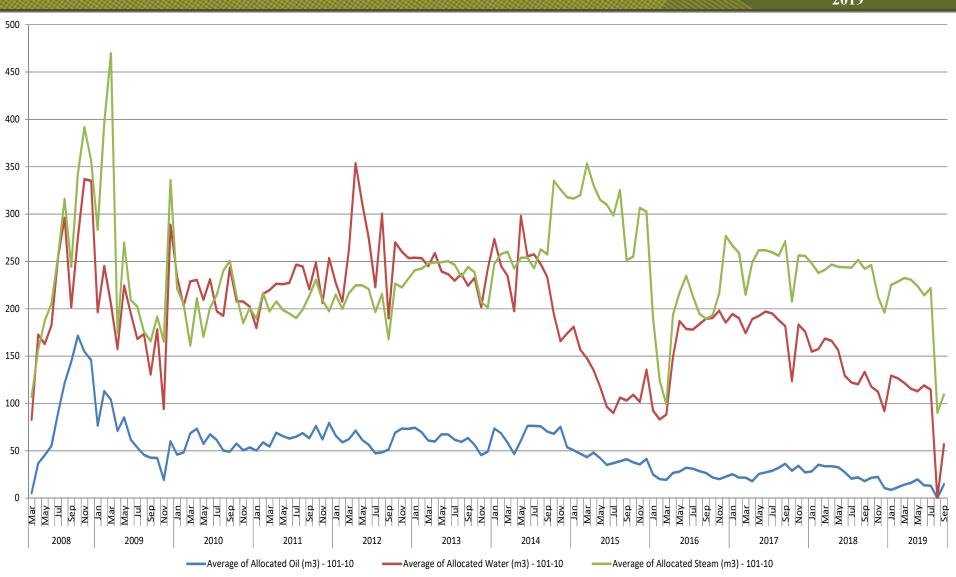




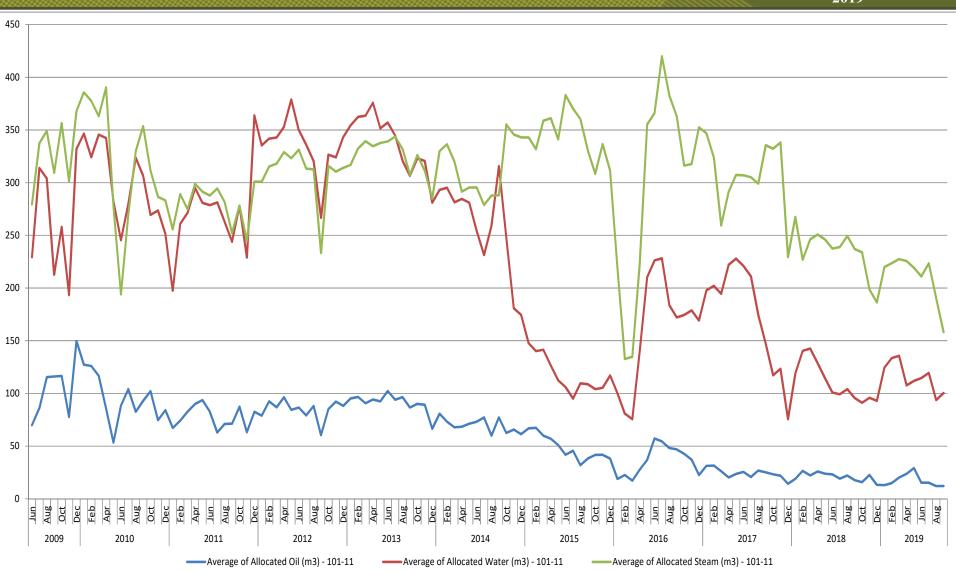




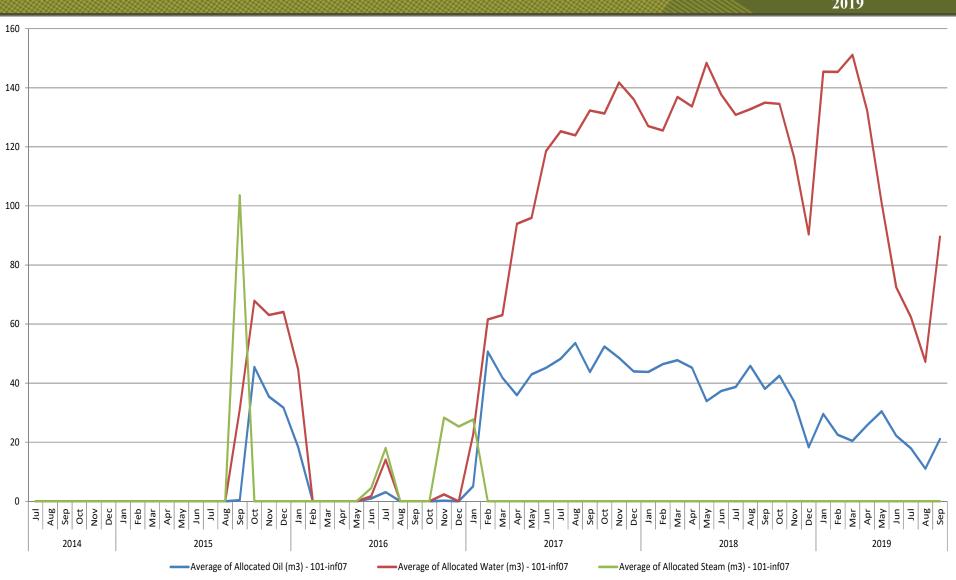




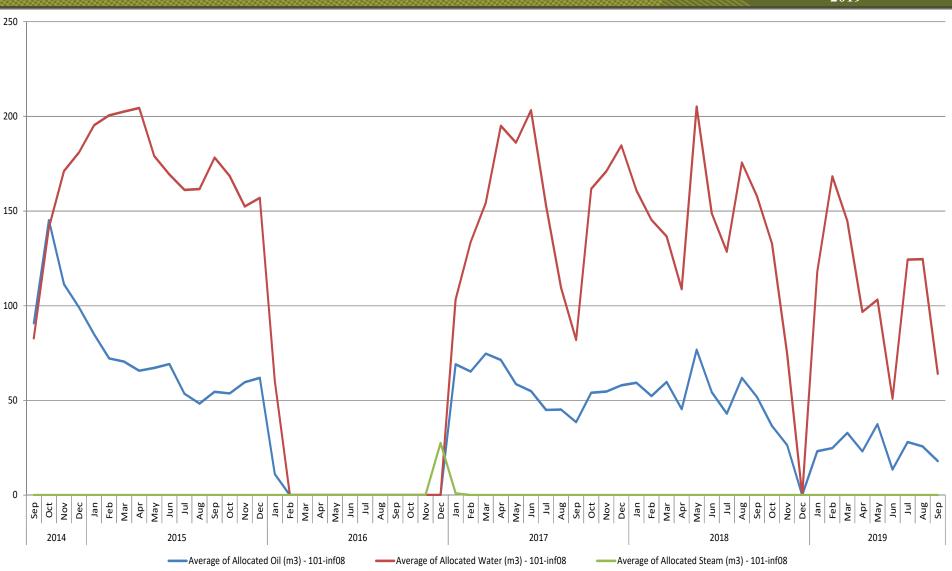




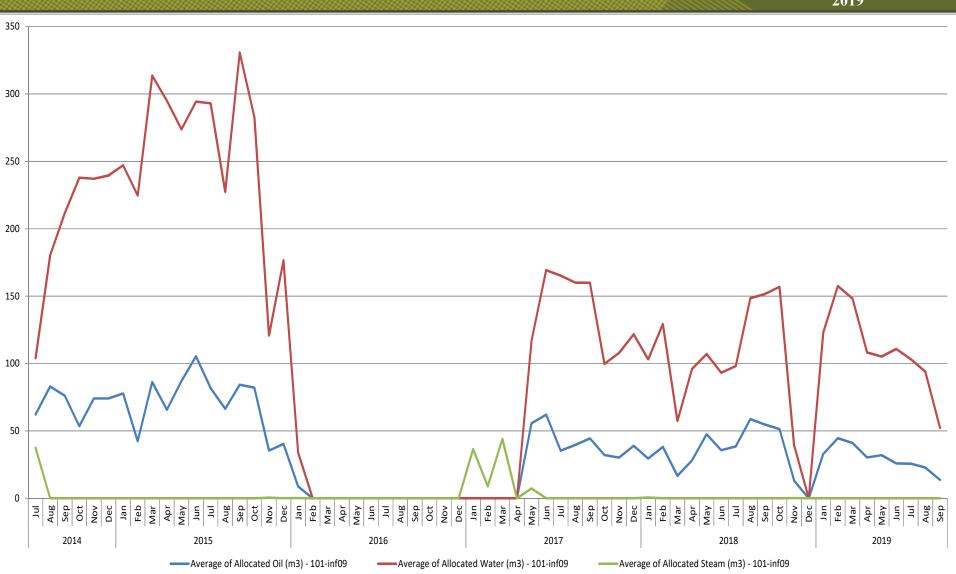




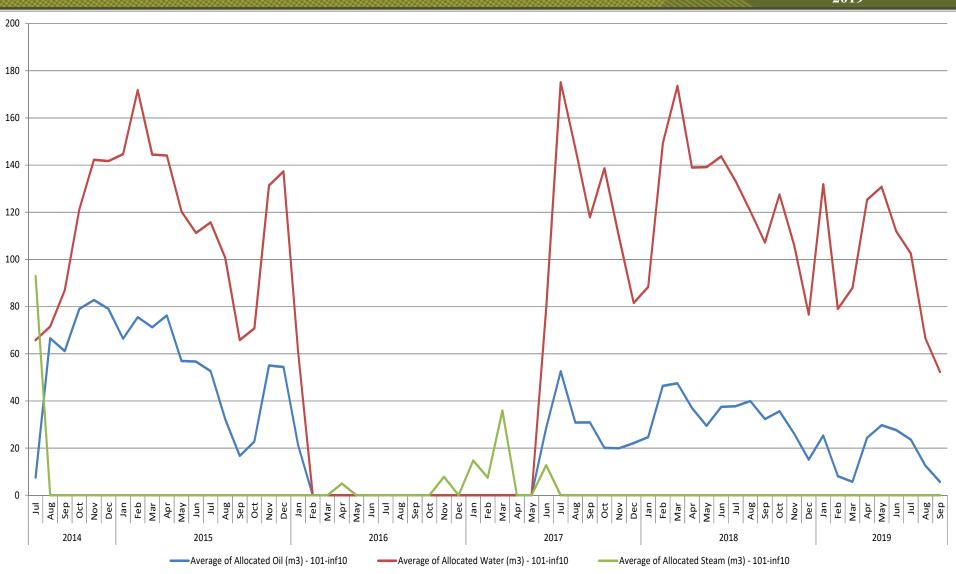




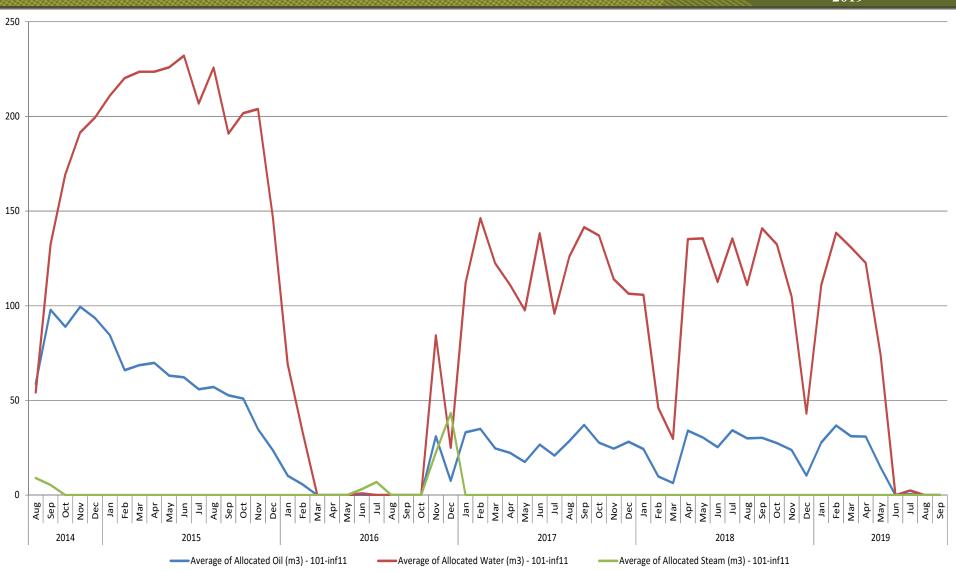




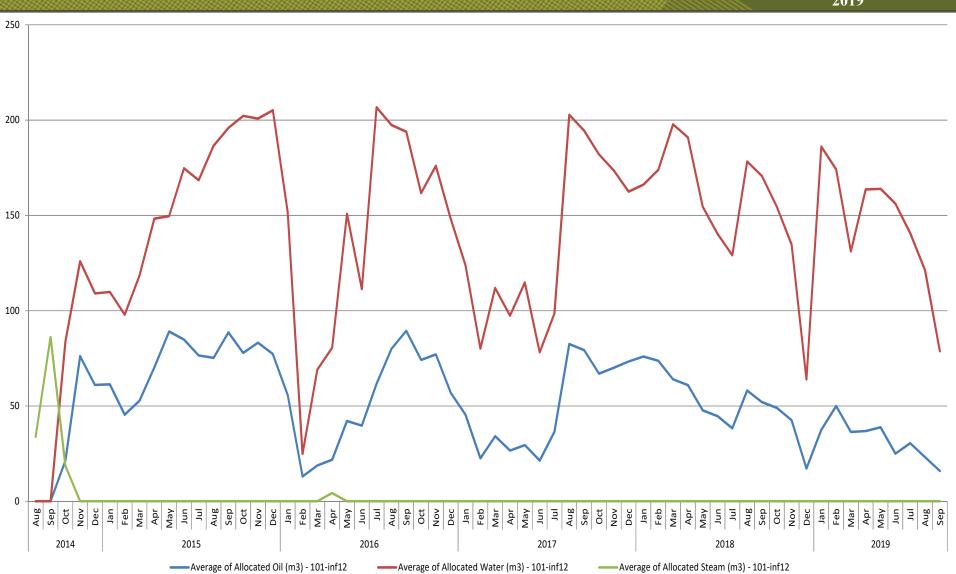




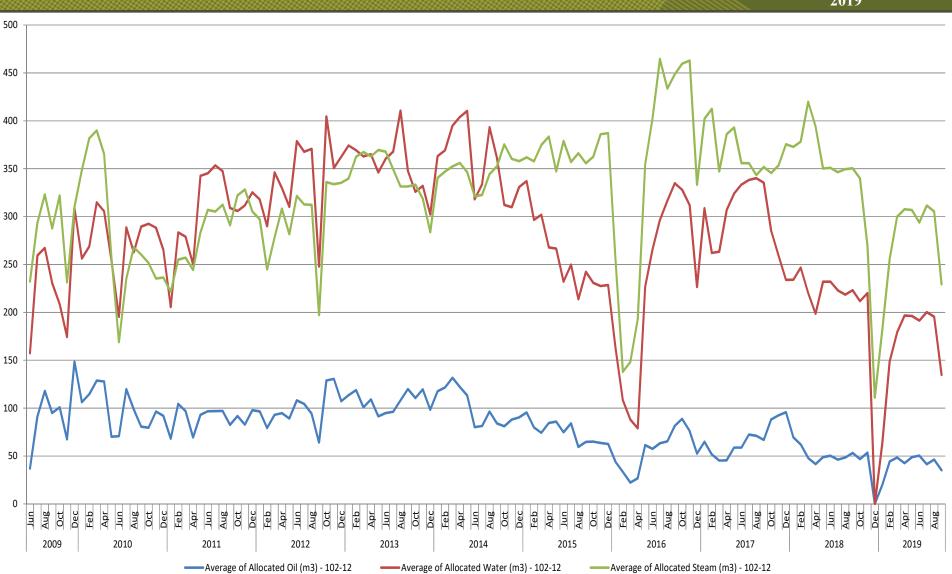




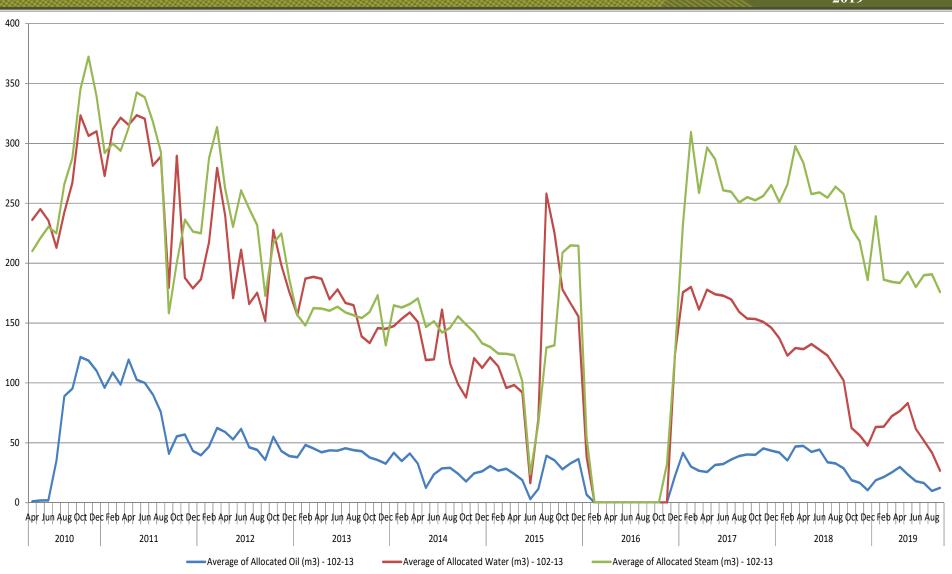




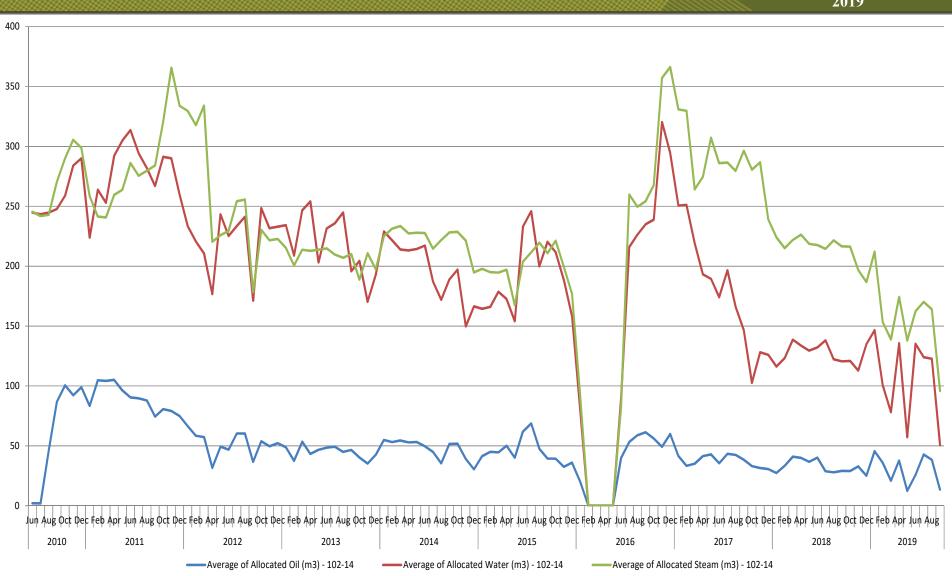




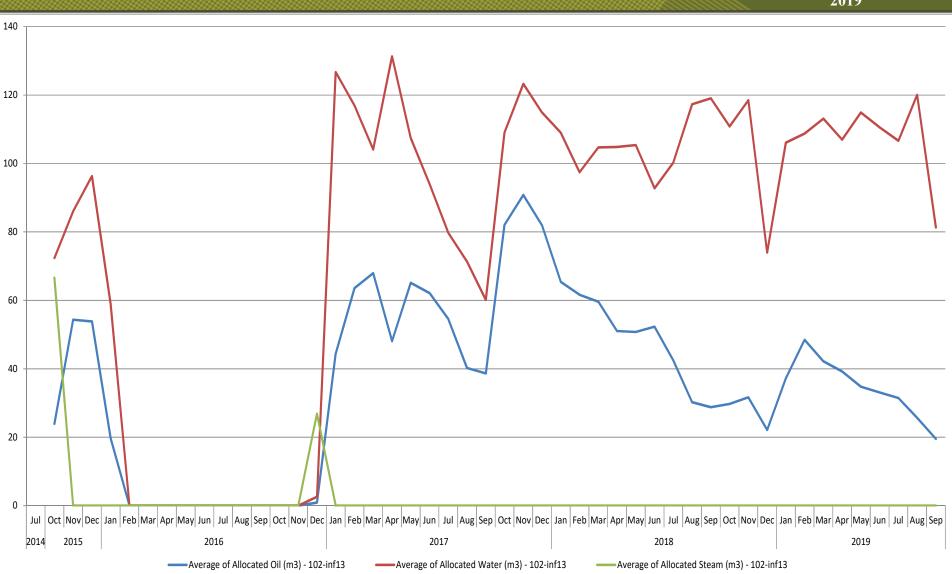








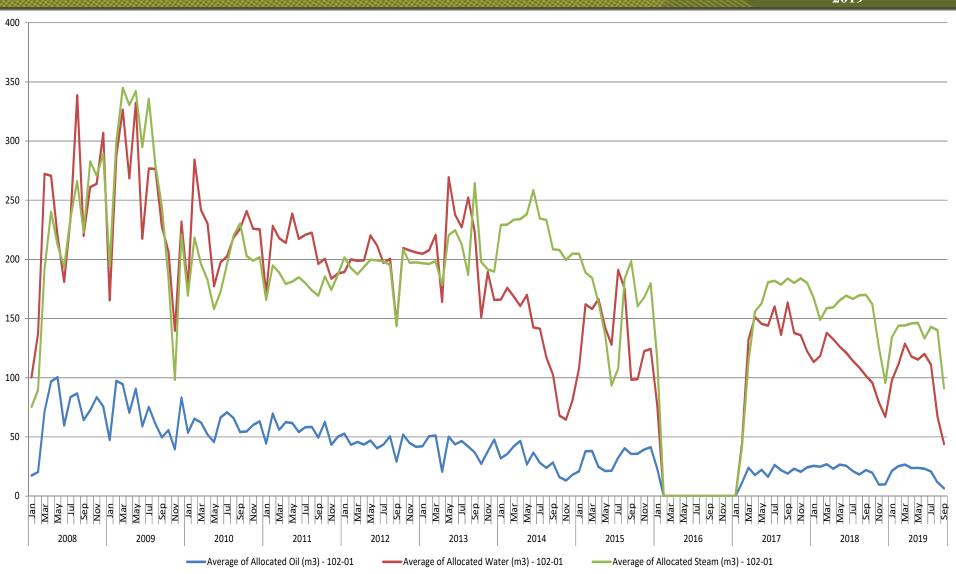




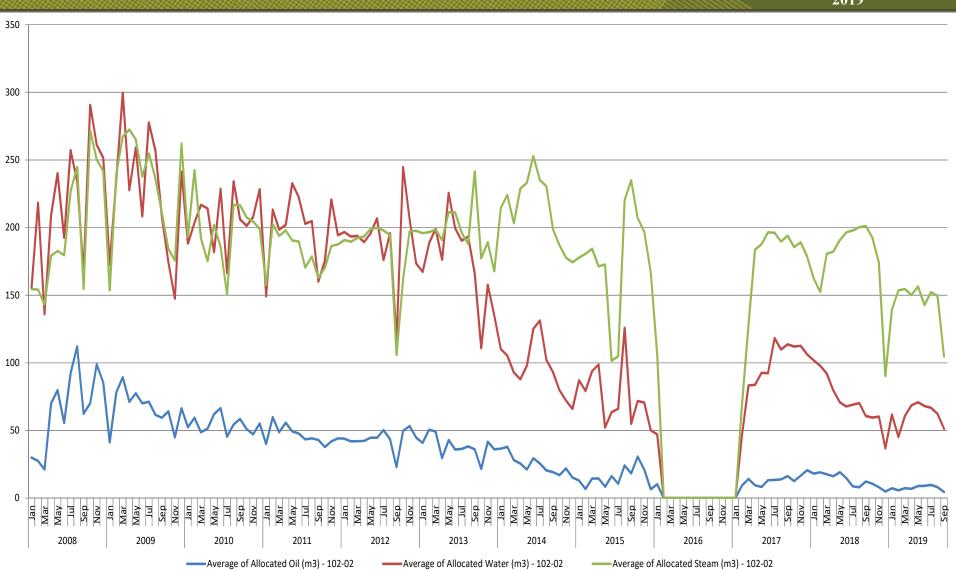




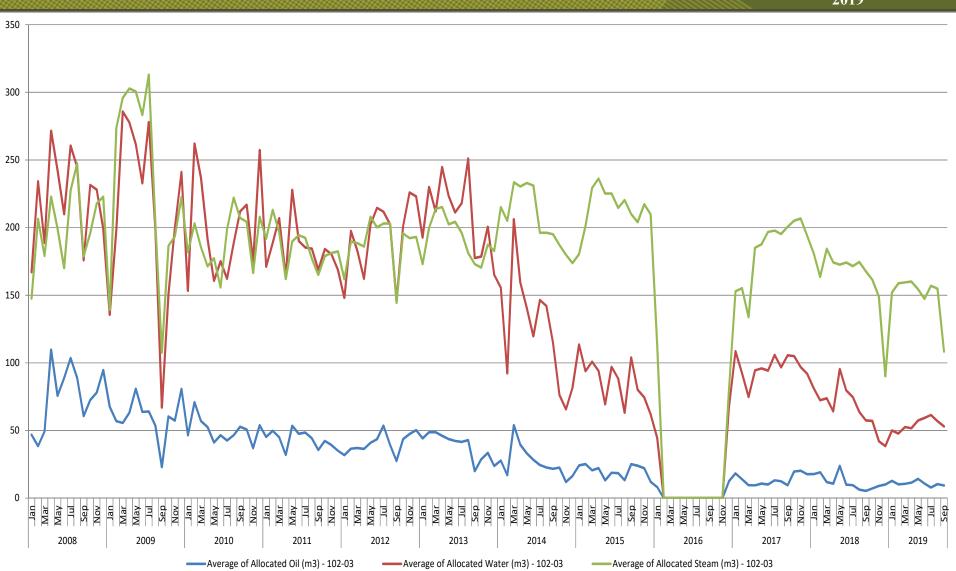




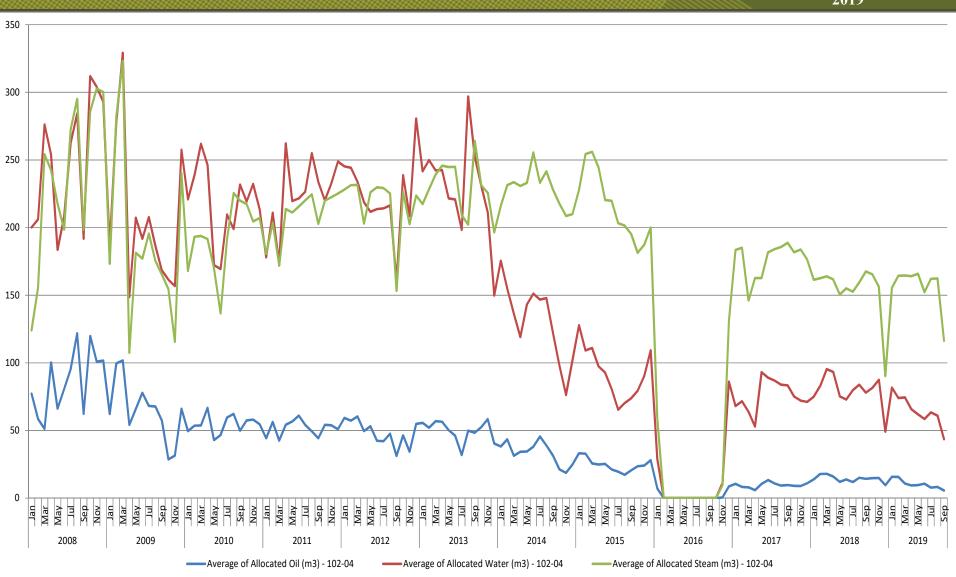




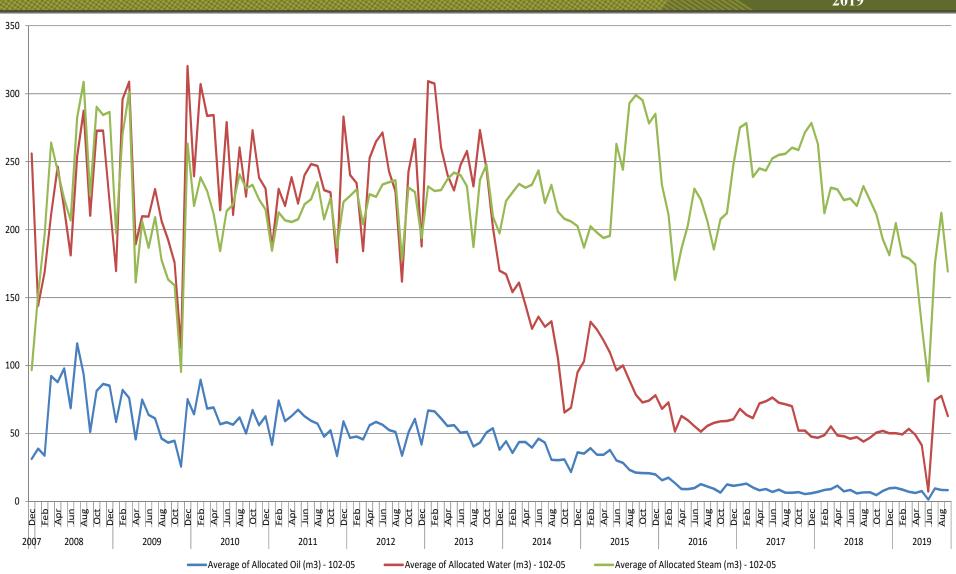




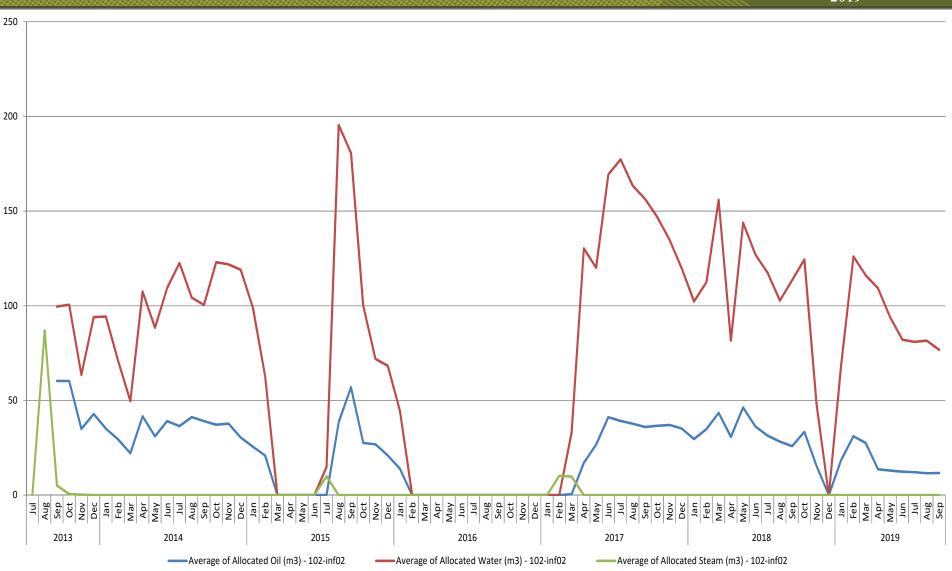




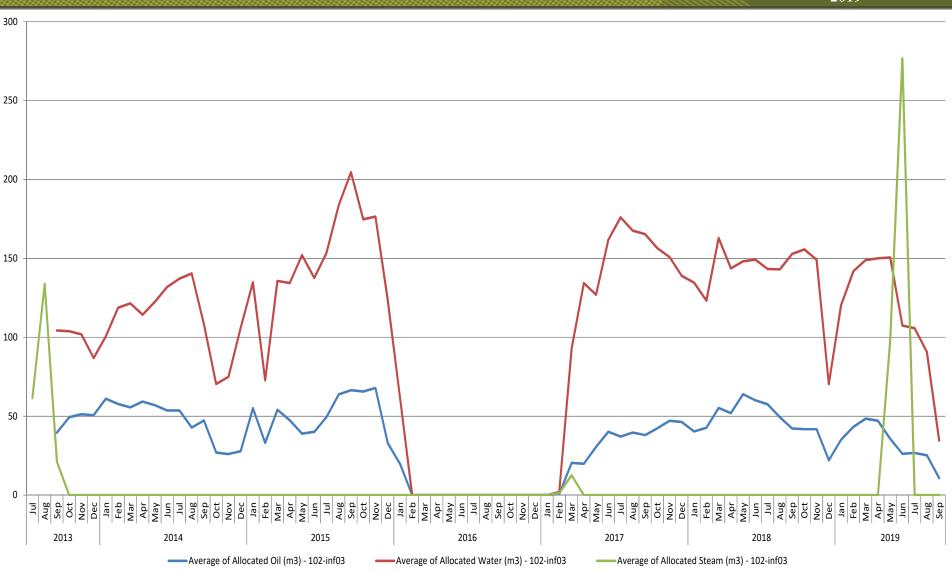




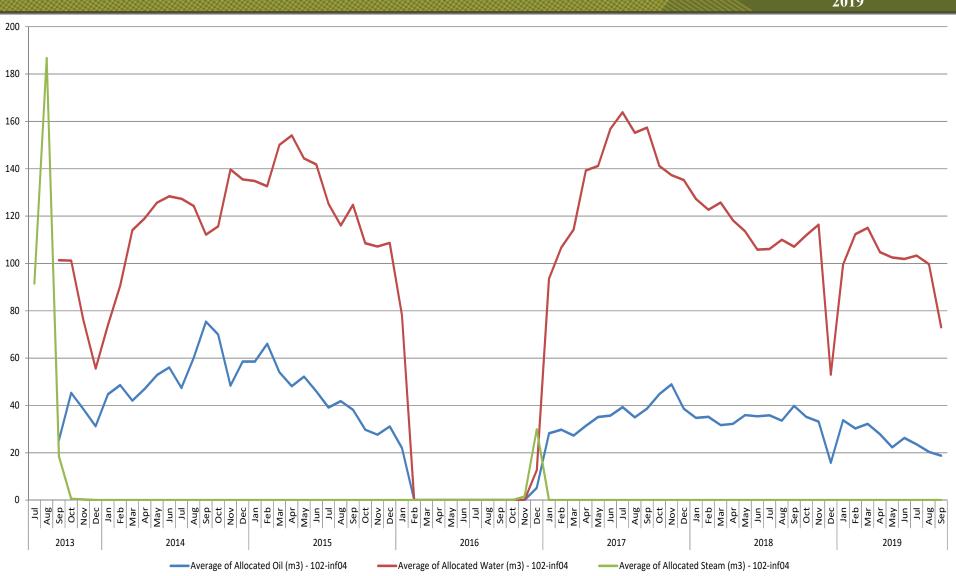




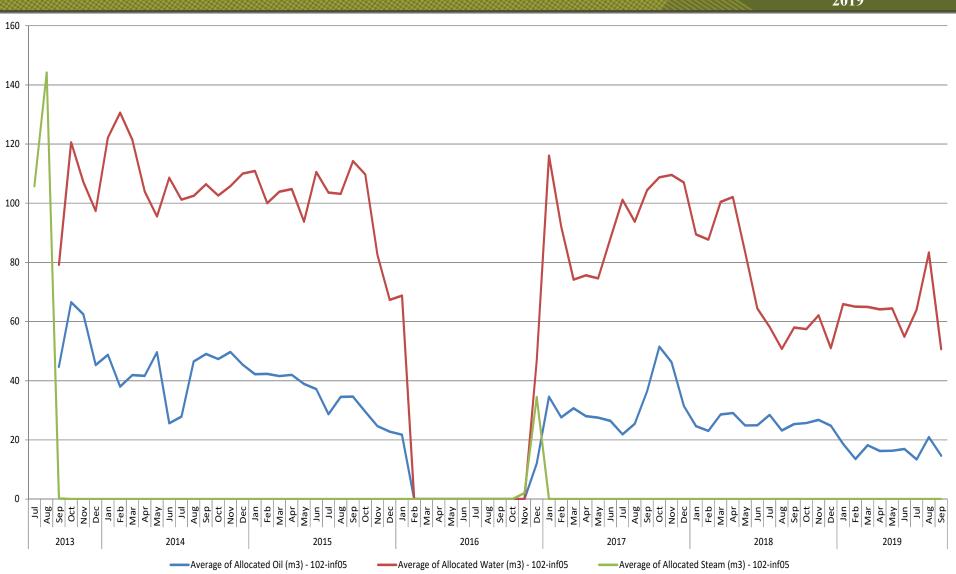




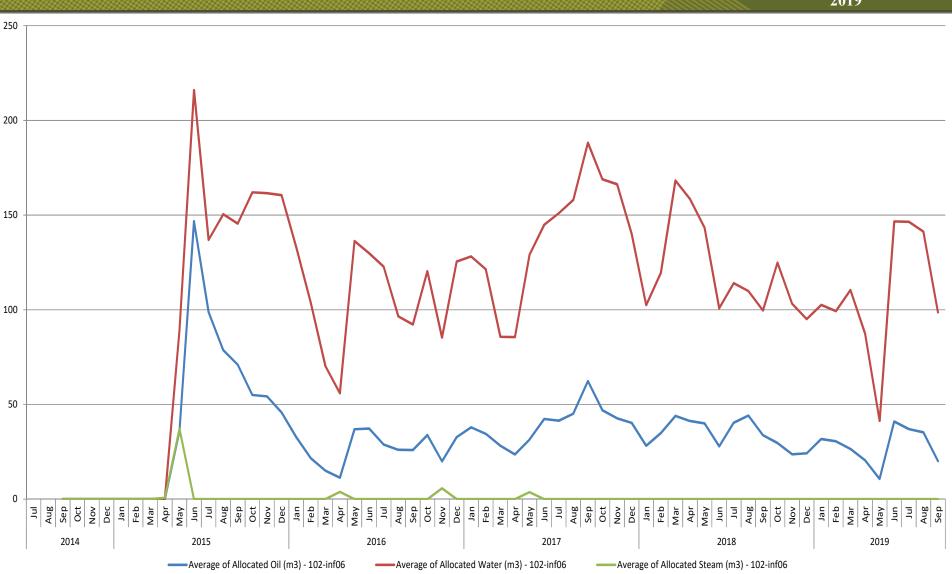




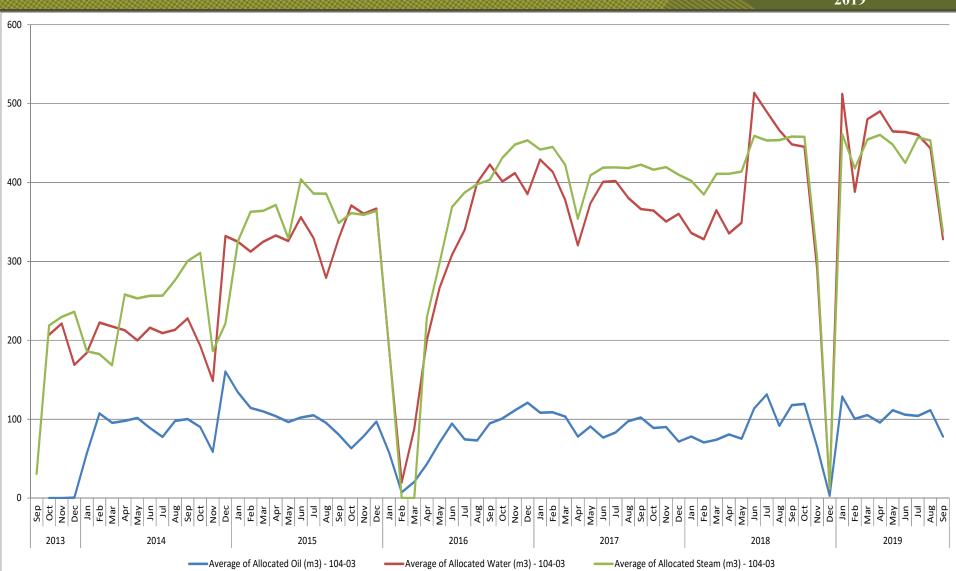




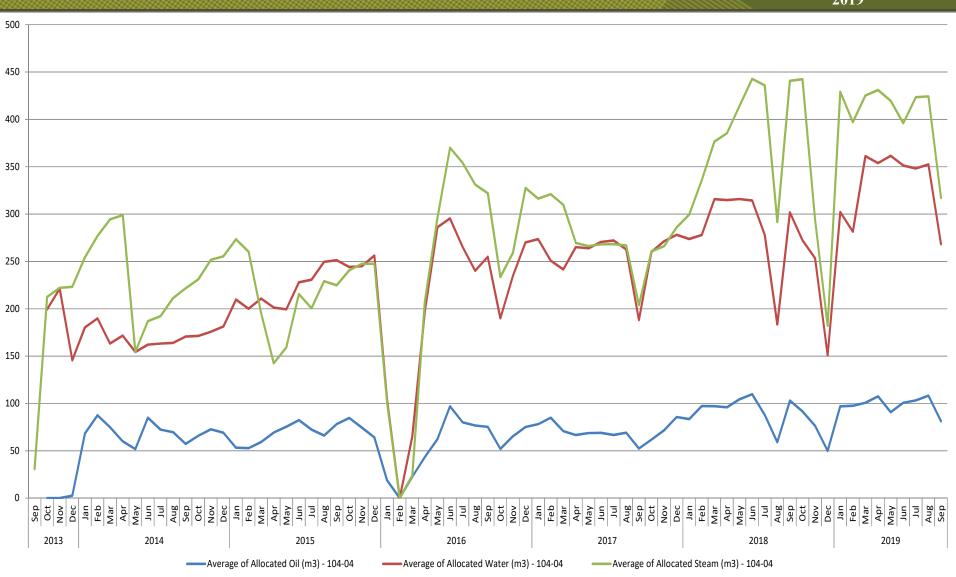




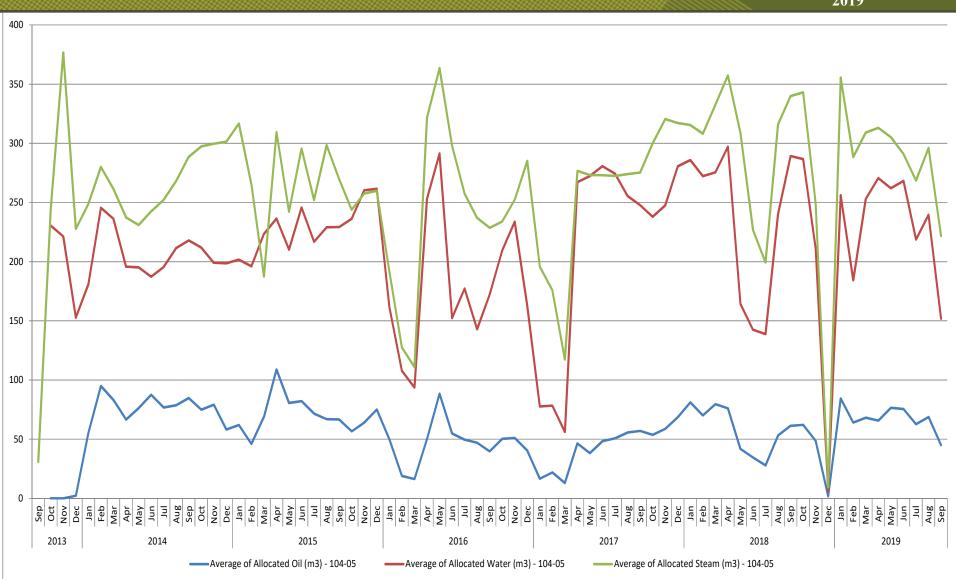




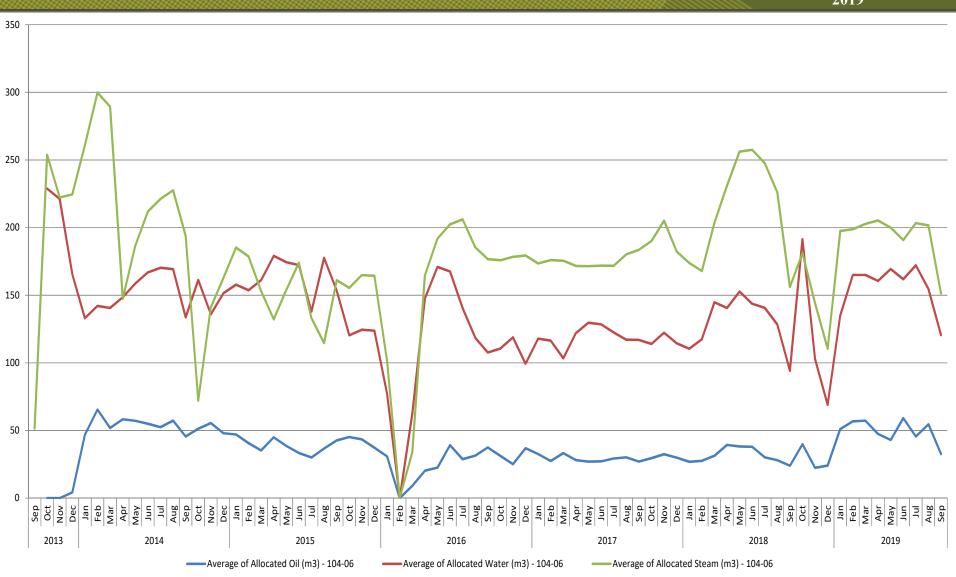




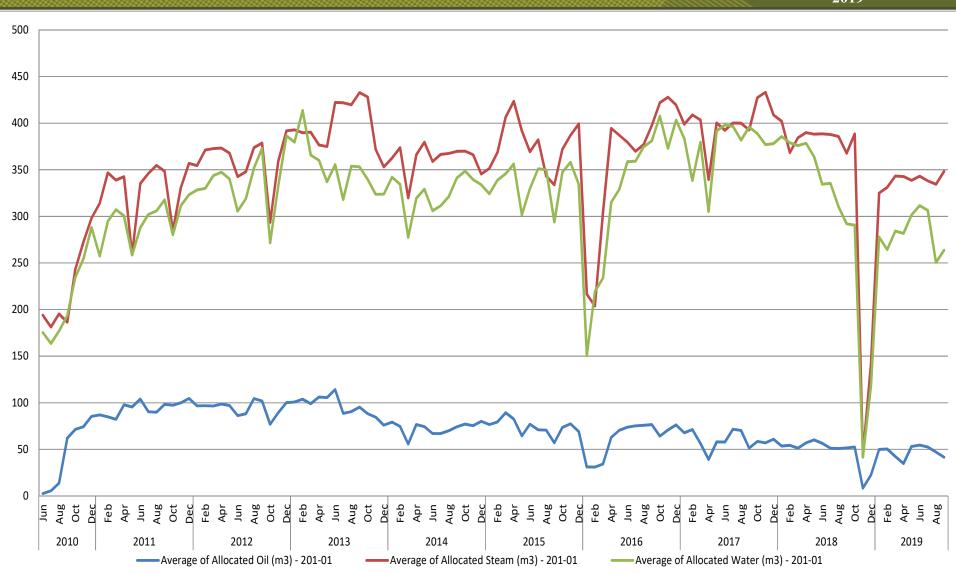




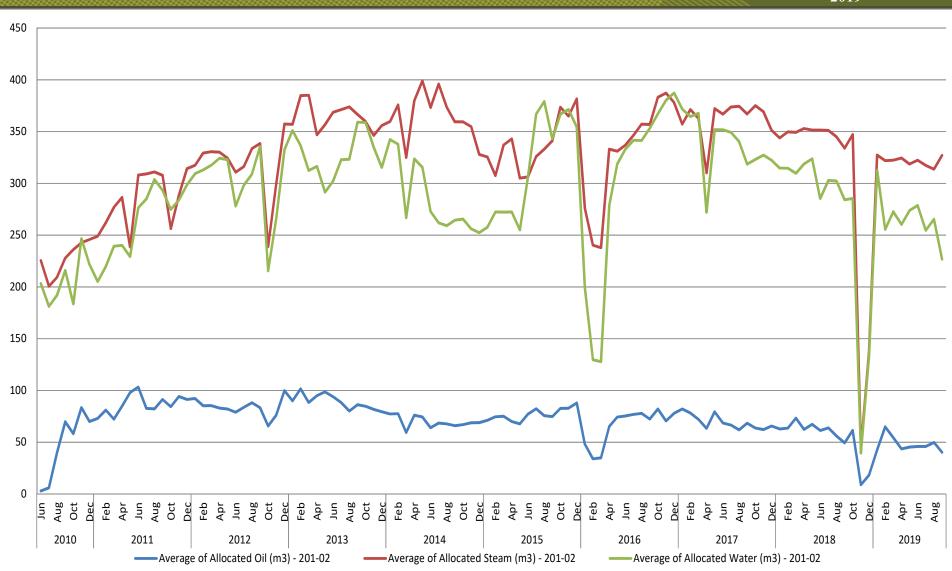




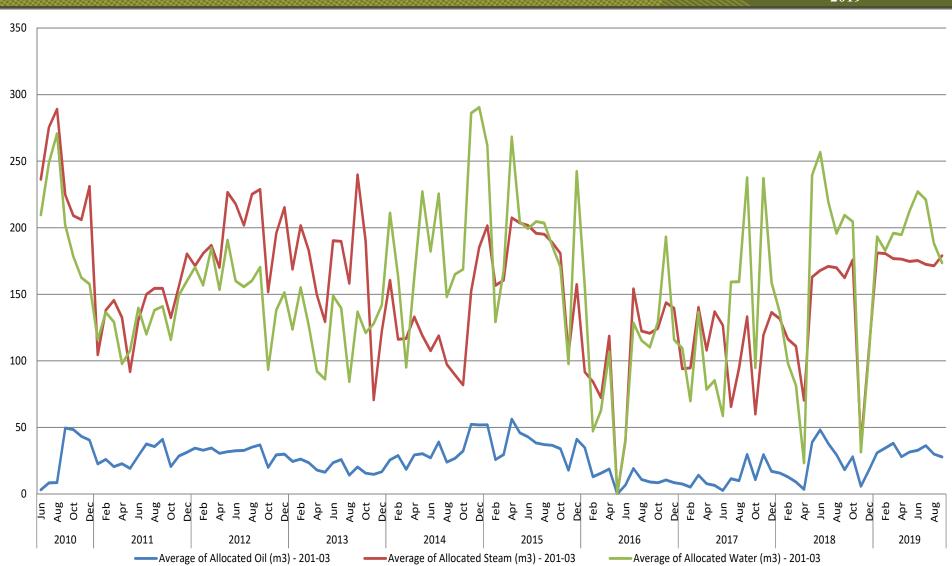




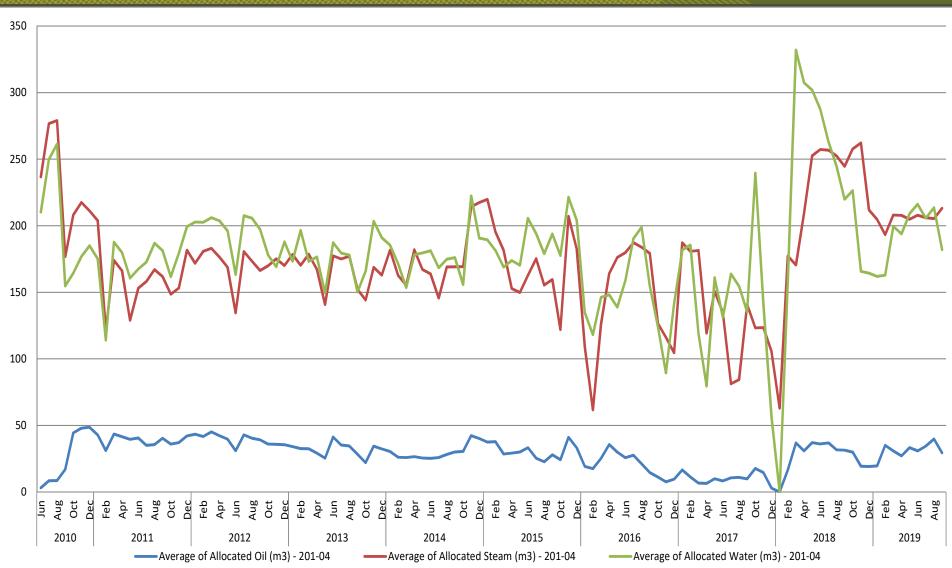




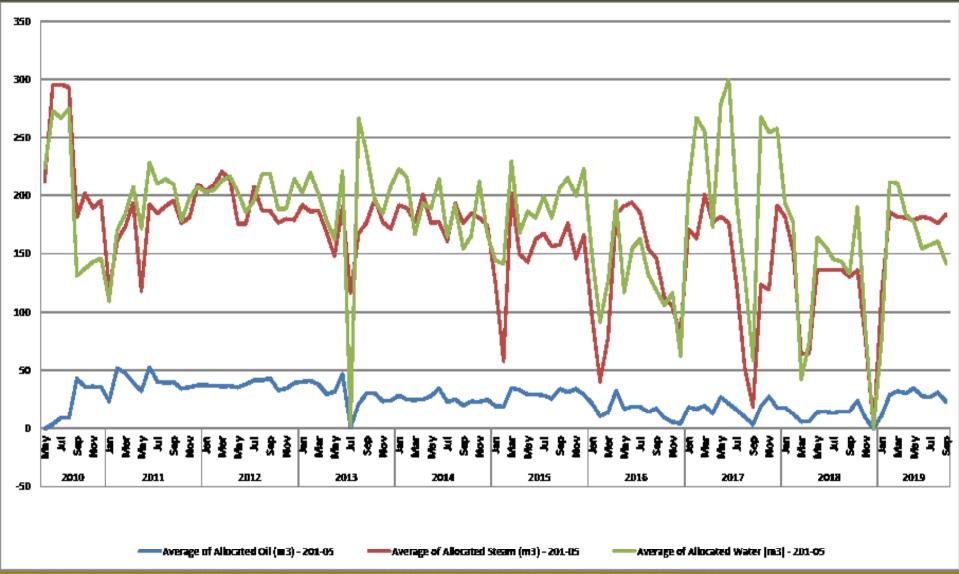




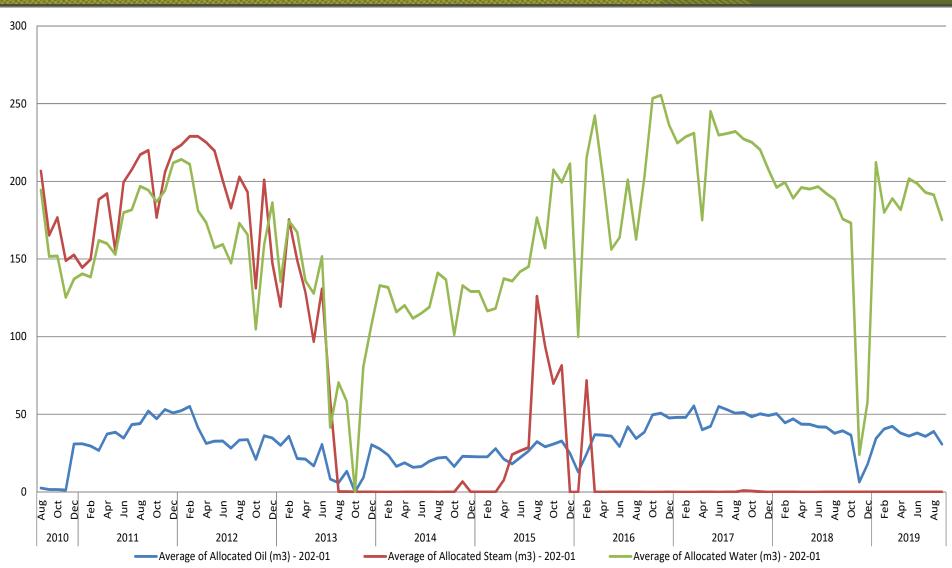












Algar - 202-01-1



