



ATHABASCA OIL CORPORATION

AER HANGINGSTONE PROJECT UPDATE

January 2019

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PROJECT DESCRIPTION AND STATUS

SUBSURFACE

- Geoscience
- Well Design and Instrumentation
- 4-D Seismic and Monitoring
- Scheme Performance
- Future Plans

SURFACE

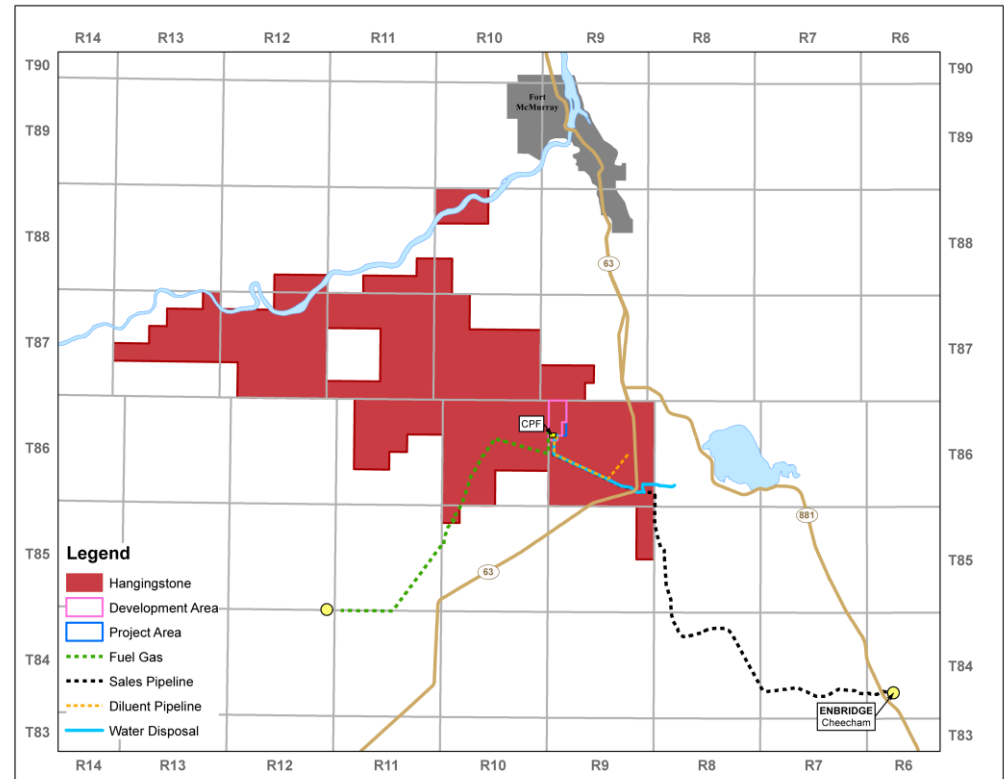
- Facilities
- Measurement and Reporting
- Water Production, Injection and Uses
- Sulphur Production
- Compliance
- Future Plans

PROJECT DETAILS

- Located 20 km south of Fort McMurray, AB
- 5 production pads
- 25 horizontal well pairs (5 well pairs per pad)
- Central Processing Facility (CPF)
- Offsite services and utilities

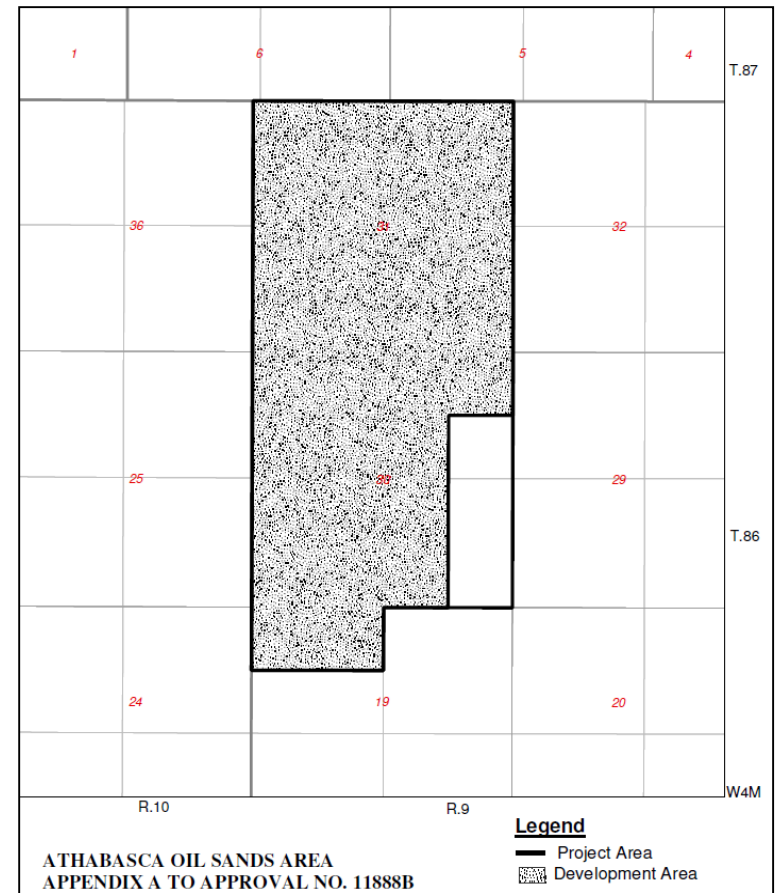
INFRASTRUCTURE

- Fuel gas from TransCanada Pipeline (TCPL)
- Dilbit export to Enbridge Cheecham Terminal
- Diluent from Inter Pipeline (IPL)



HANGINGSTONE PROJECT

- First steam (downhole) achieved March 2015
 - *First oil produced July 2015*
- 24 well pairs in SAGD mode and 1 standing well pair
 - *AA05 converted to SAGD in June 2018*
 - *Last well pair (AA03) to be brought on-stream when steam is available*
- Expansion application submitted in 2013
 - *Environmental Impact Assessment report deemed complete by the AER pursuant to Section 53 of EPEA*
 - *Expands Project Area and Development Area*
 - *Application includes 3 phases (+70,000 bbl/d)*

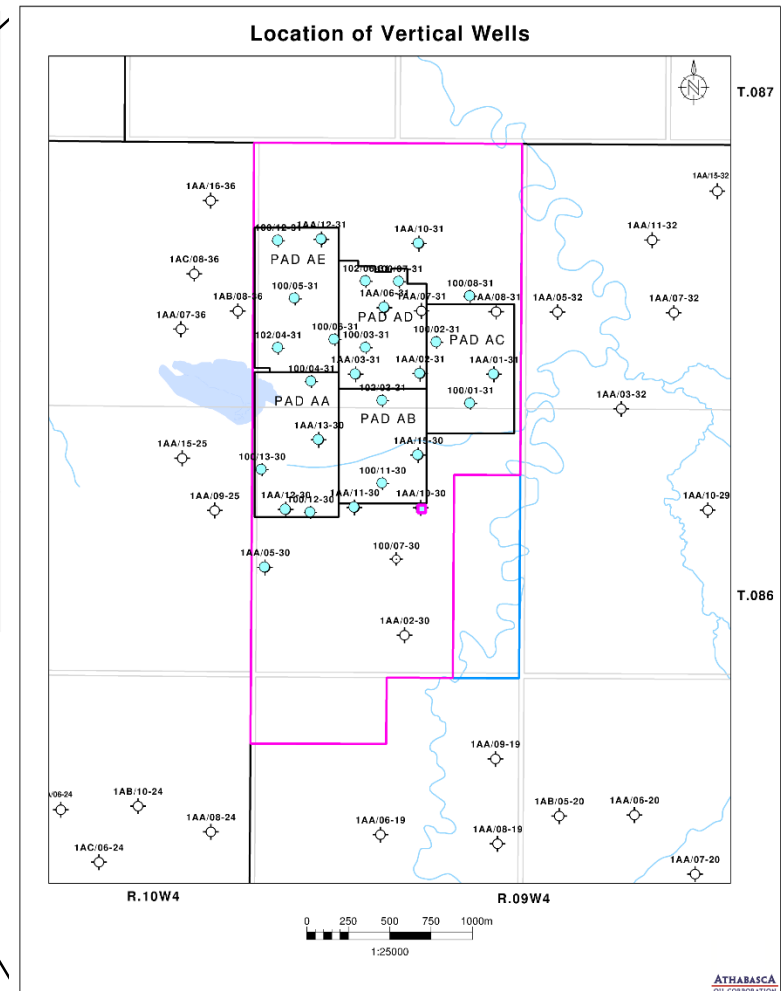
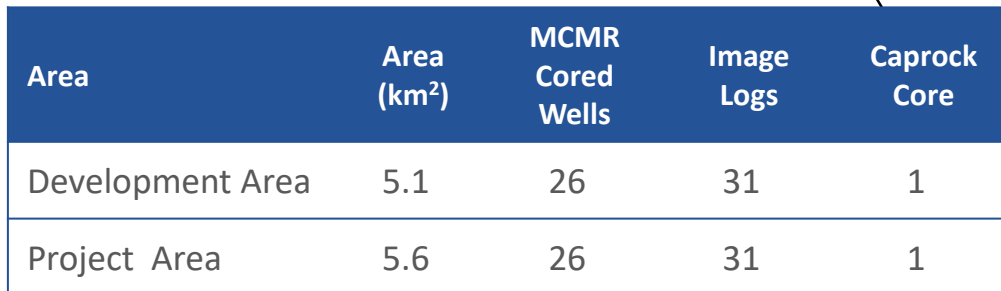




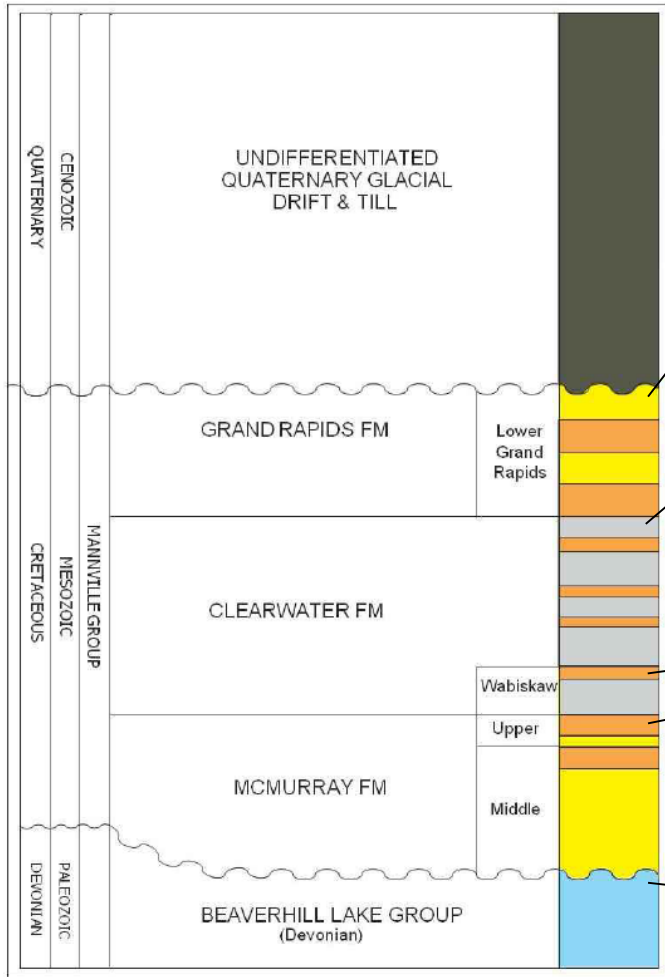
SUBSURFACE
GEOSCIENCES

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- i.e. cores, petrographic, geomechanical or fracture pressure or caprock integrity tests

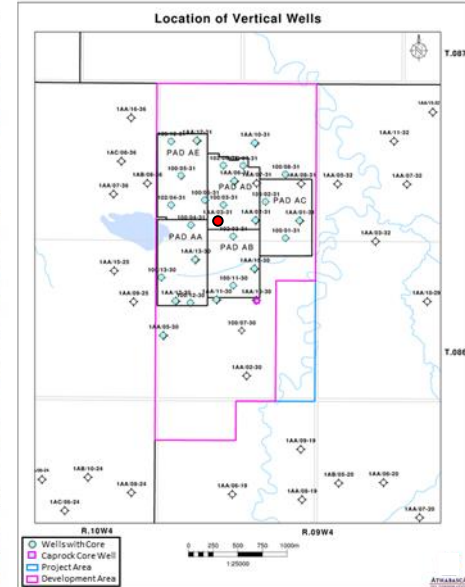
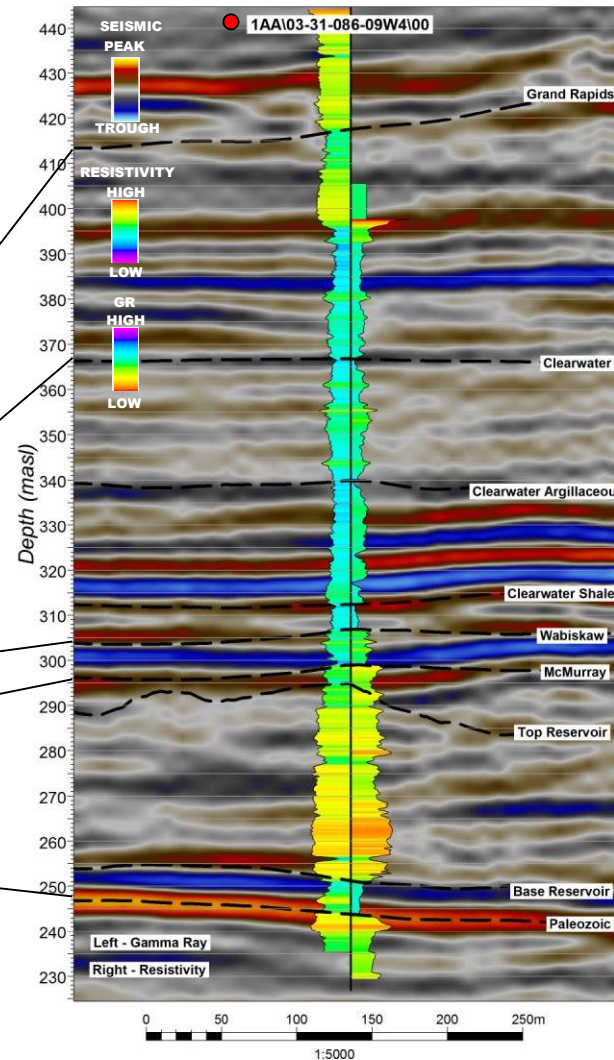


MIDDLE MCMURRAY TARGET RESERVOIR



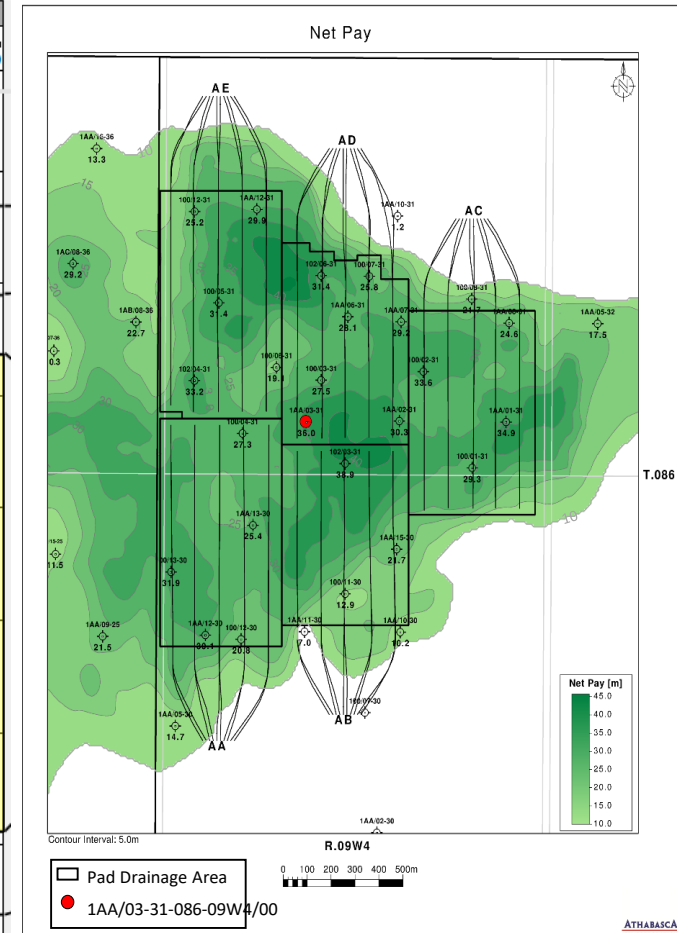
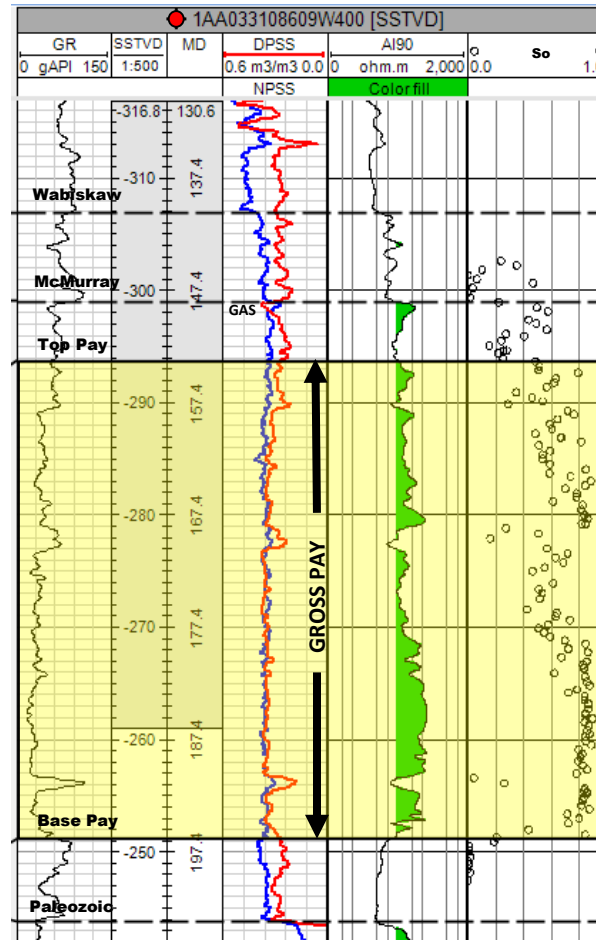
FACIES

Sand	Yellow
Sandy IHS	Orange
Muddy IHS	Grey
Mudstone	Dark Grey
Limestone	Blue



MIDDLE MCMURRAY GROSS PAY DEFINITION

- Thickness ≥ 10 m
- GR < 70 API
- Density $> 27\%$
- Resistivity > 18 ohm-m
- Water Saturation $< 50\%$
- Includes < 1 m thick mud
- Net pay thickness uses gross pay criteria but excludes mud

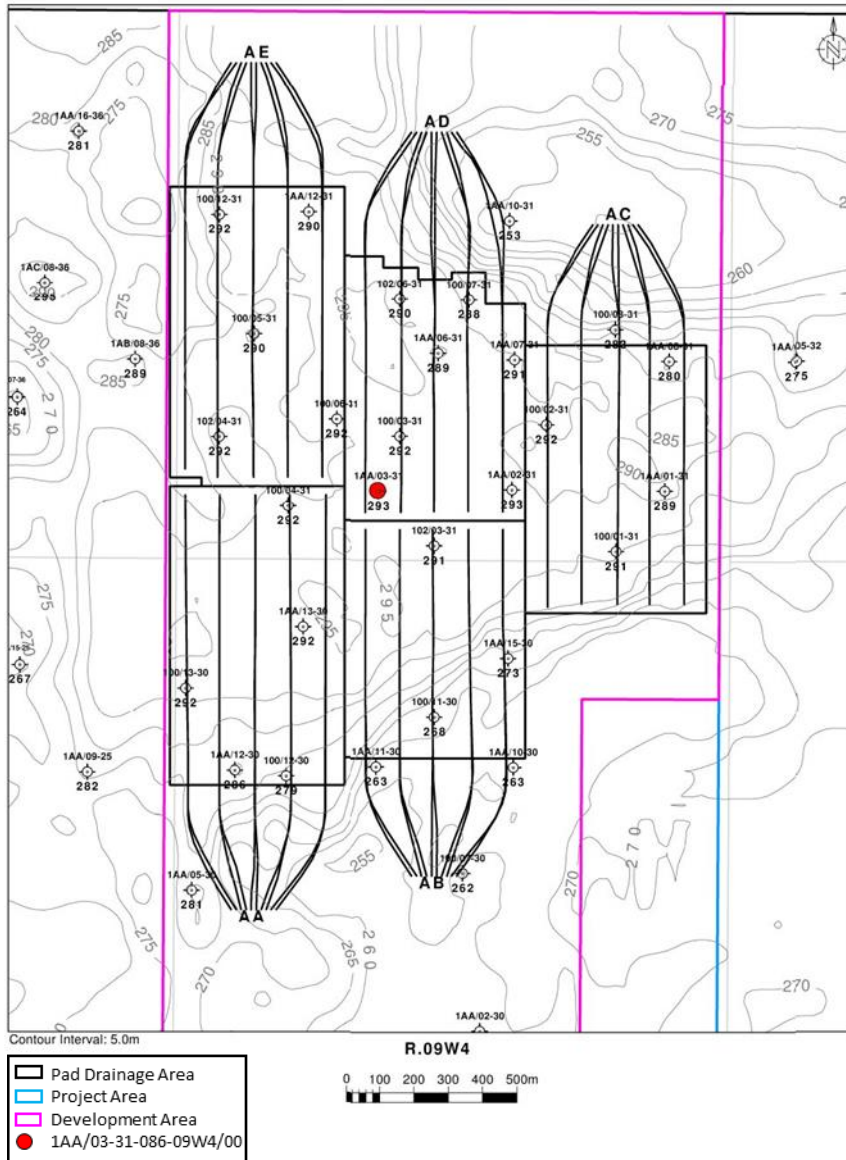


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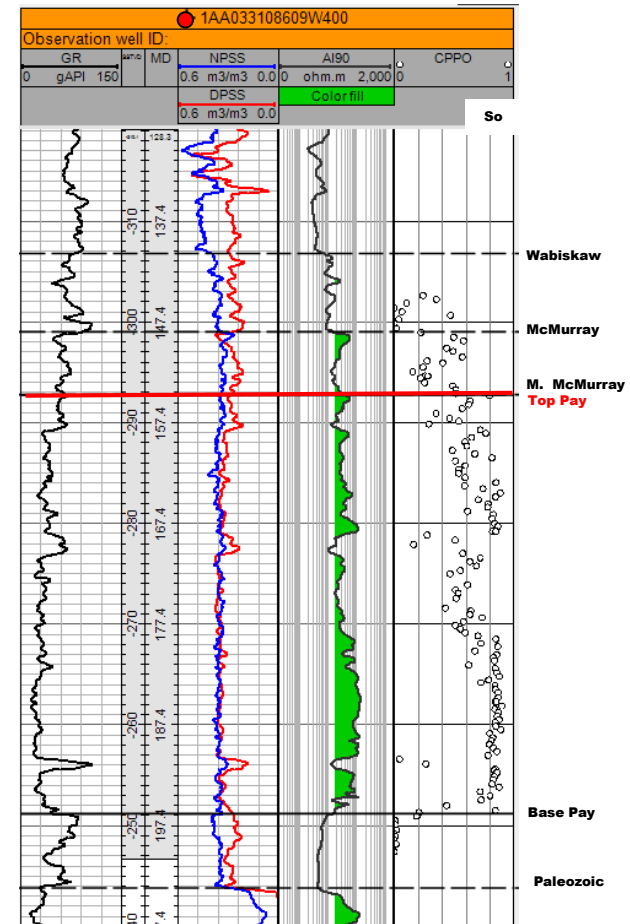
STRUCTURE MAP OF TOP OF BITUMEN PAY

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ELEVATION RANGE

- 262 -301 masl



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Well log plot for well 1AA113008609W400 [SSTVD]. The plot displays several tracks: GR (Gamma Ray), SSTVD (SSTVD), TVD (True Vertical Depth), DPSS (Density Porosity), and AI90 (Acoustic Impedance). The depth scale ranges from -311.3 to -250 meters. Key geological features and labels include Wabiskaw, McMurray, M. McMurray, Top Pay, Base Pay, Basal Mud, Basal Water Zone, and Paleozoic. A red arrow points to the depth of -250 meters.

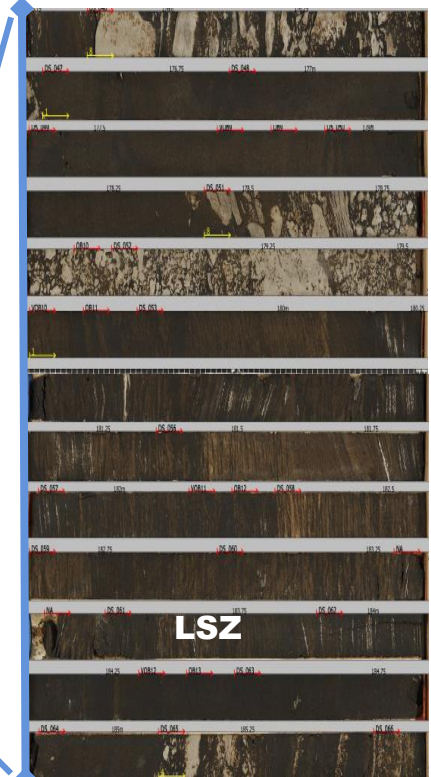
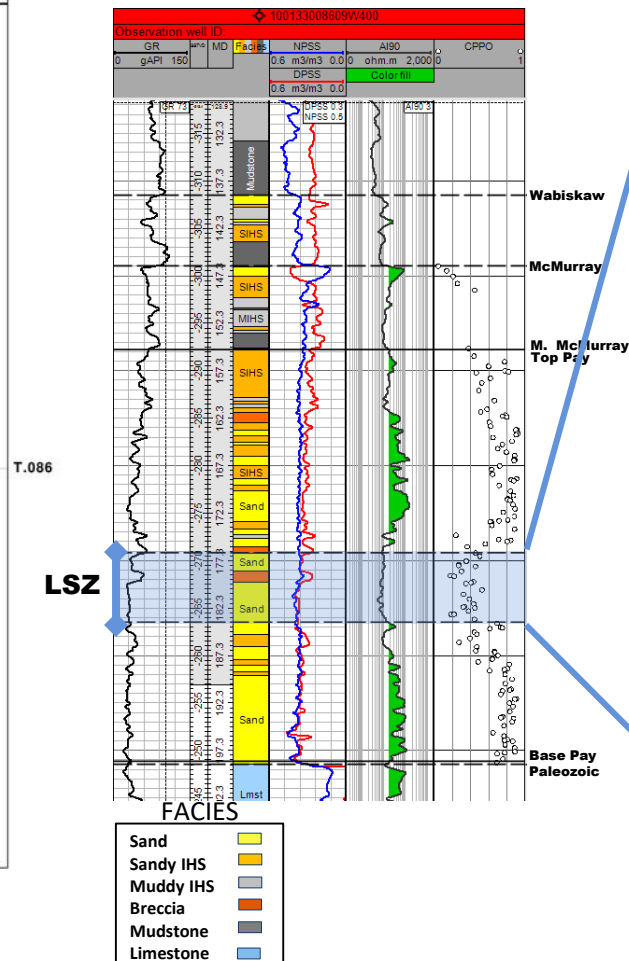
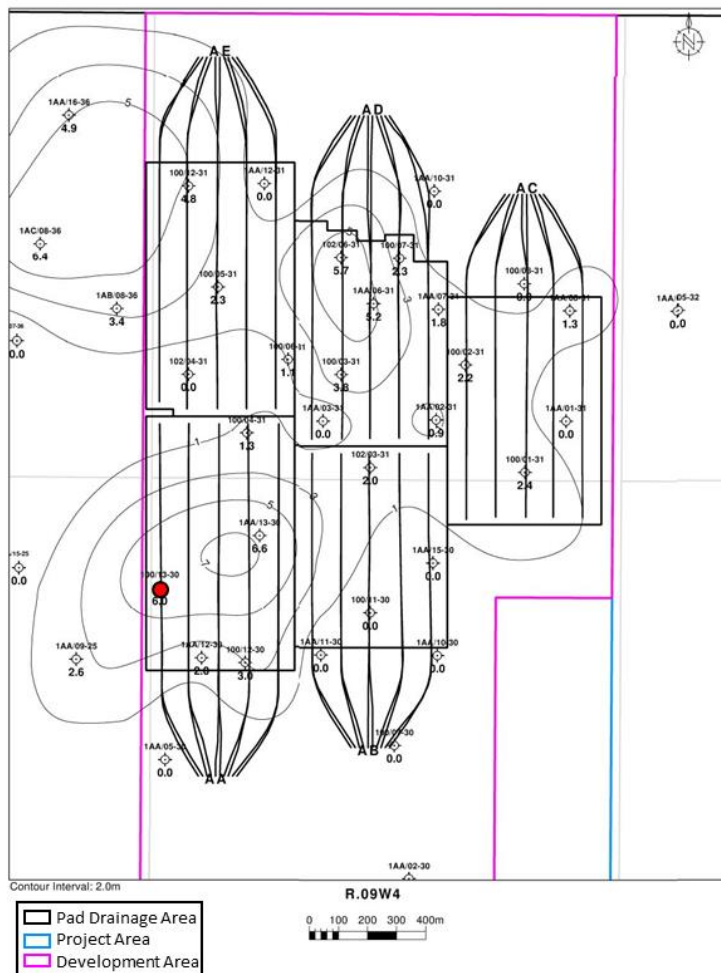
ISOPACH MAP OF MIDDLE MCMURRAY LOW BITUMEN SATURATION

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LOW BITUMEN SATURATION ZONE (LSZ)

- GR<60 API, density porosity >0.27 and resistivity 10-18 ohm-m and core water saturation >50%
- Core $S_o = 0.36$ and porosity = 0.37, thus the LSZ will still contribute to the overall bitumen production

Low Saturation Zone Net Thickness

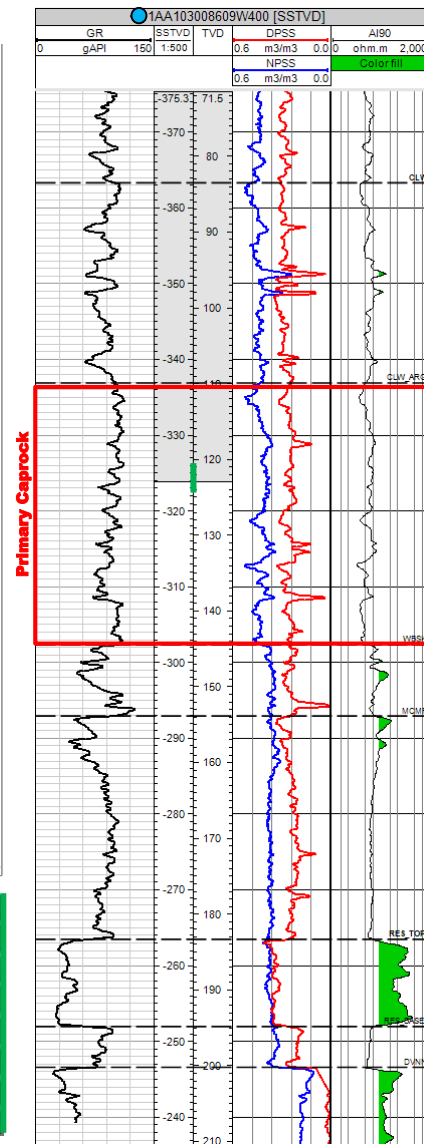
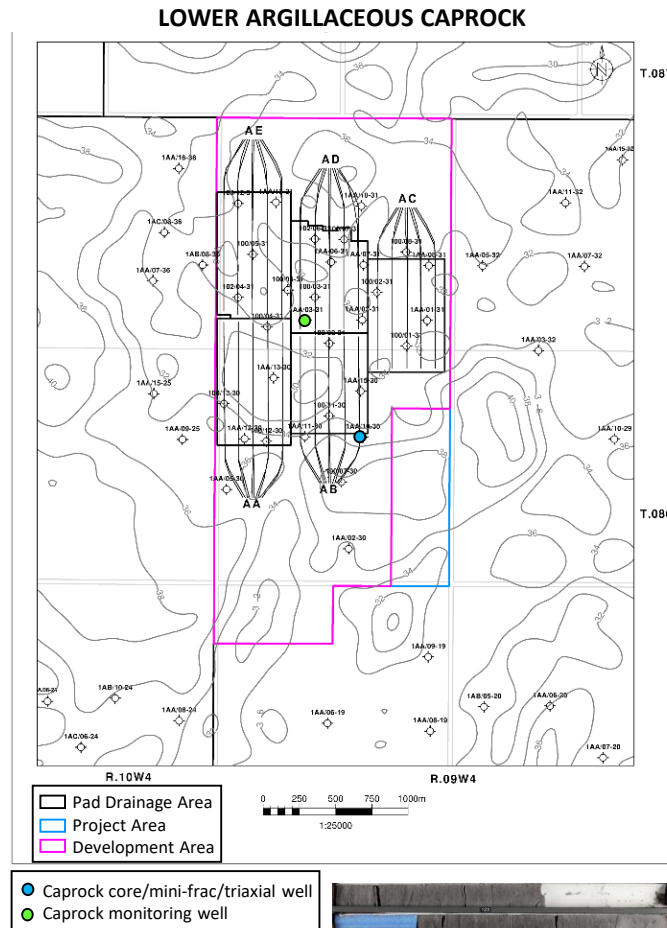


2018

- No pressure or temperature change has been observed in the caprock during the reporting period
- No new caprock core, mini-frac or tri-axial testing completed during the reporting period

HISTORICAL

- Caprock is defined as the unit between the top of the Clearwater and Wabiskaw
- One observation well has one piezometer and two thermocouples in the caprock



RESERVOIR PROPERTIES AND OBIP ABOVE PRODUCER

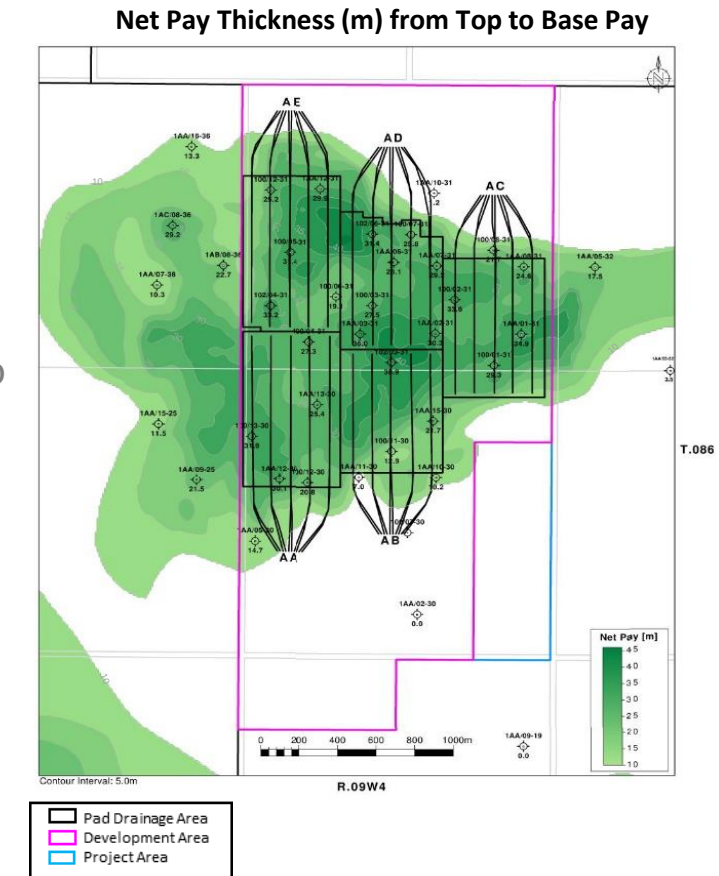
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RESERVOIR PROPERTIES

- Typical Producer Depth: 191 TVD (258 masl)
- Initial Reservoir Pressure @ 190m TVD: 600 kPaa
- Initial Reservoir Temperature: 8°C
- Horizontal Permeability: 3,500-4,300 mD
- Vertical Permeability: 2,800-3,600 mD
- Bitumen Viscosity @ initial reservoir temperature: >1mN cP

Gross OBIP = Thickness from Top to Base Pay x Area x Porosity x So

	Avg Por (frac)	Avg So (frac)	OBIP (mln m ³)
Drainage Areas	0.36	0.72	15.6
Development Area	0.36	0.72	18.6
Project Area	0.36	0.72	18.6





SUBSURFACE
WELL DESIGN AND INSTRUMENTATION

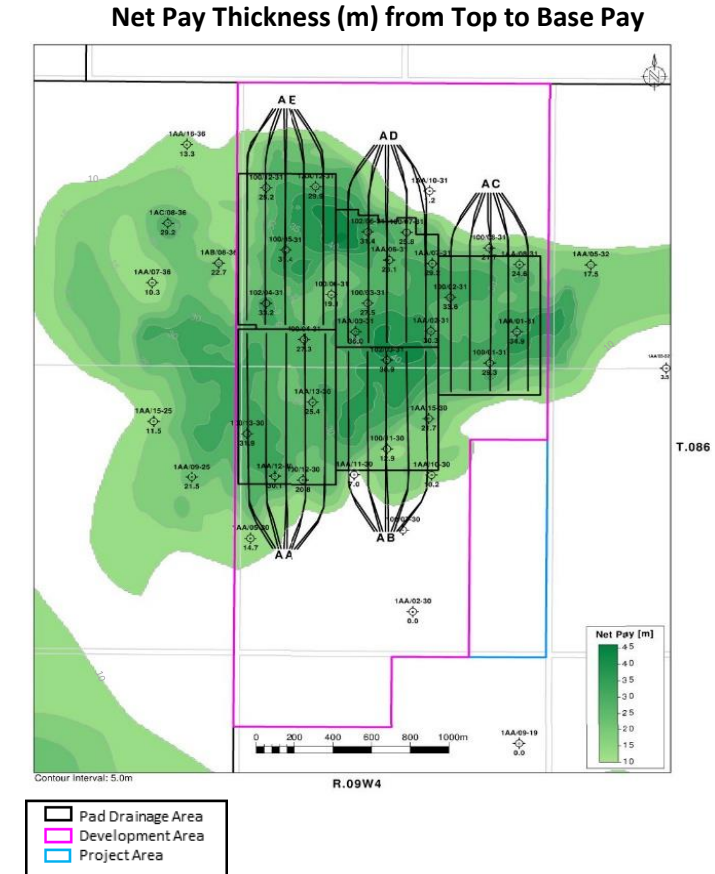
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2018

- No new wells were drilled during this reporting period

HISTORICAL

- 5 well pads with 25 well pairs



TYPICAL COMPLETION & ARTIFICIAL LIFT

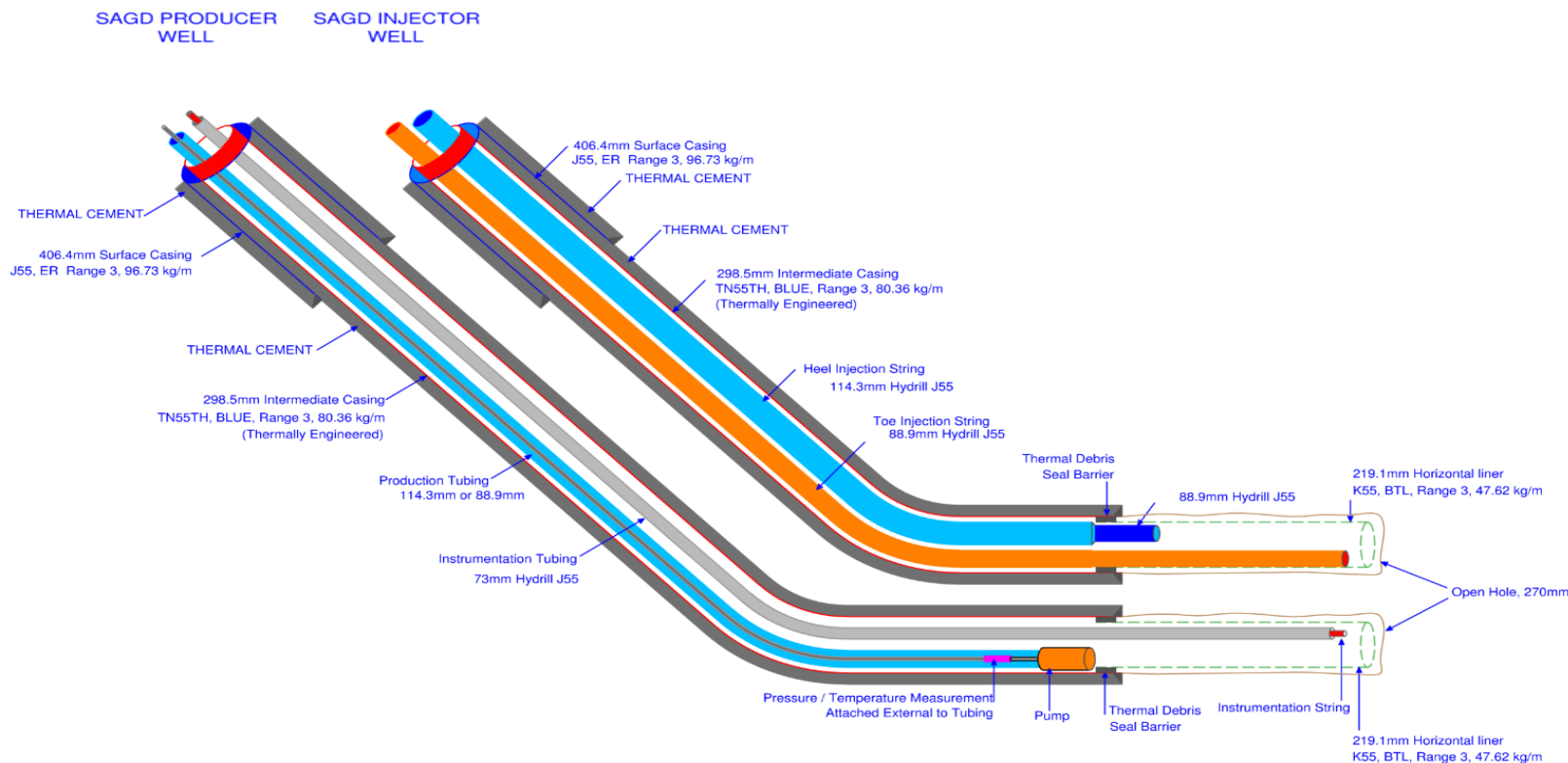
19

- All wells initially completed with all-metal PCP
- Wells and facilities built with flexibility to convert from PCPs to ESPs
- Converted from PCPs to ESPs as rates improved and the wells matured
- Typical pump operating conditions:
 - Average bottomhole pressure = 1,800 kPag
 - Average bottomhole temperature = 180 °C

Artificial Lift Performance	PCP	ESP
Typical Minimum Rate (m ³ /d)	100	125
Typical Maximum Rate (m ³ /d)	600	825

Well	Type
AA1	ESP
AA2	ESP
AA3	PCP*
AA4	ESP
AA5	PCP
AB1	ESP
AB2	ESP
AB3	ESP
AB4	ESP
AB5	ESP
AC1	ESP
AC2	PCP
AC3	ESP
AC4	ESP
AC5	ESP
AD1	ESP
AD2	ESP
AD3	ESP
AD4	PCP
AD5	ESP
AE1	ESP
AE2	ESP
AE3	ESP
AE4	ESP
AE5	ESP

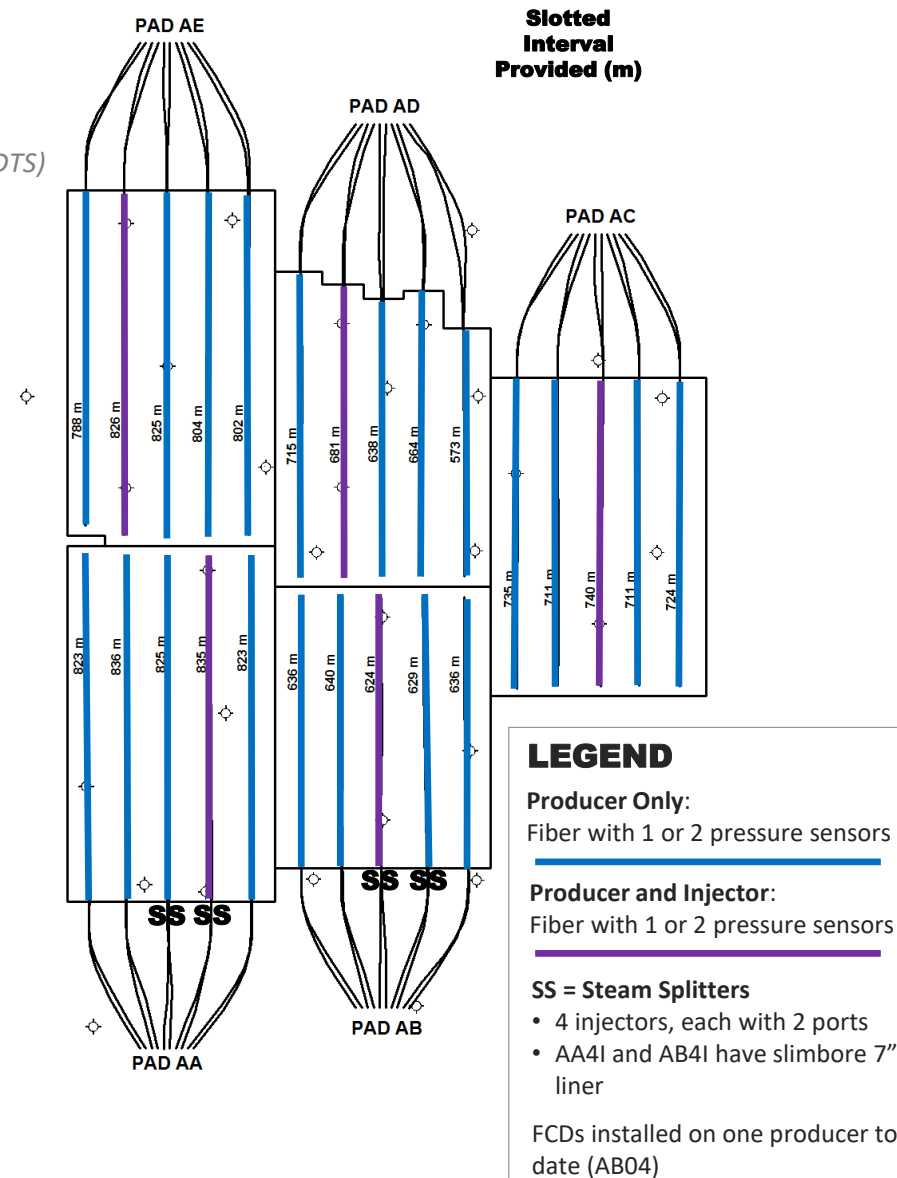
*Production assurance well



- Two types of fiber for temperature measurements
 - *Fiber Bragg Grating (FBG) and Distributed Temperature Sensing (DTS)*
- Both systems adequate for temperature management along the wellbore

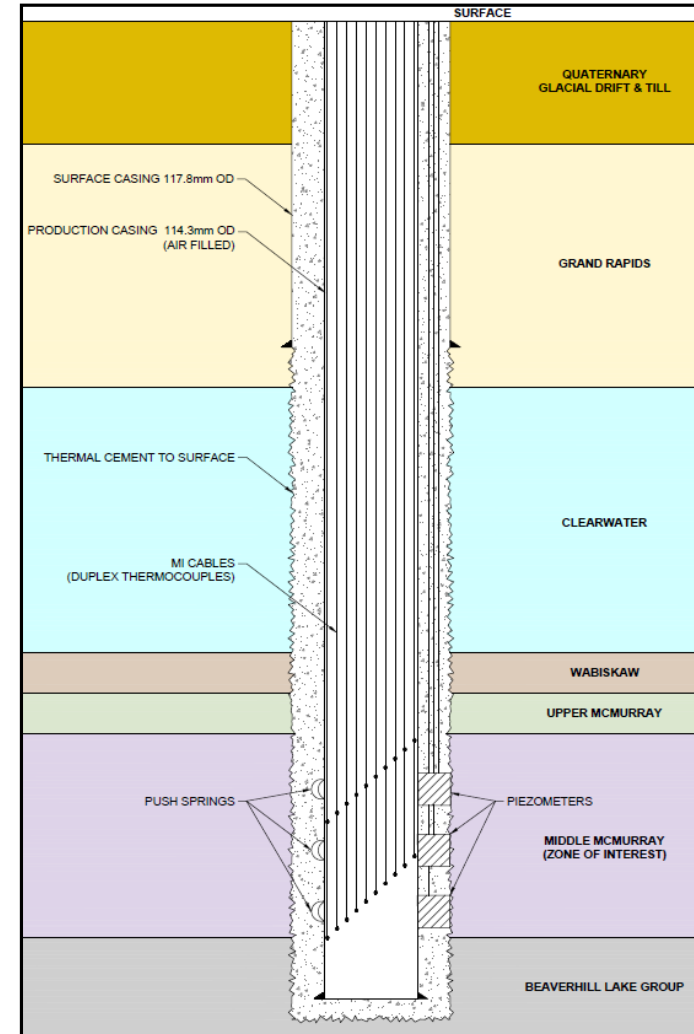
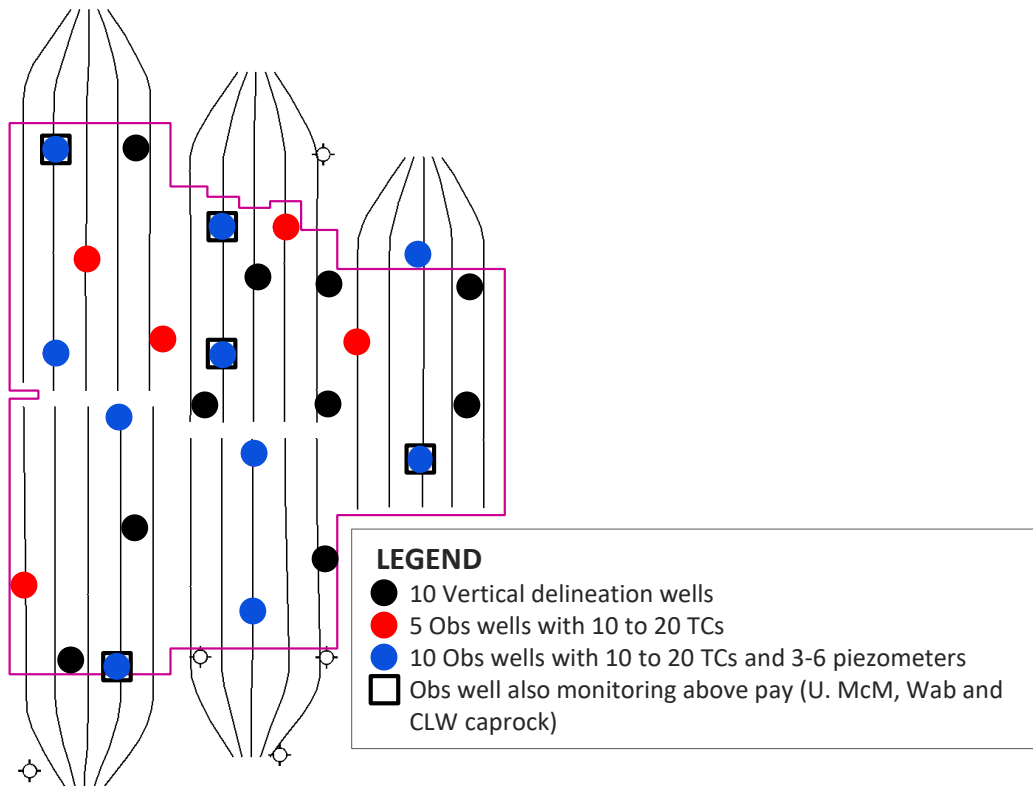
- Injector BHP is measured with blanket gas
- Producer BHP is measured using optical gauges and/or bubble tubes

- FCD installed in well AB04, March 2018
- Evaluation of performance is on-going



OBSERVATION WELLS

- Some pressure sensors have failed (typically after steam conditions observed)
- Instrumentation used to monitor reservoir pressure and temperature growth





SUBSURFACE

4D SEISMIC AND MONITORING

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RESERVOIR SATURATION TOOL (RST)

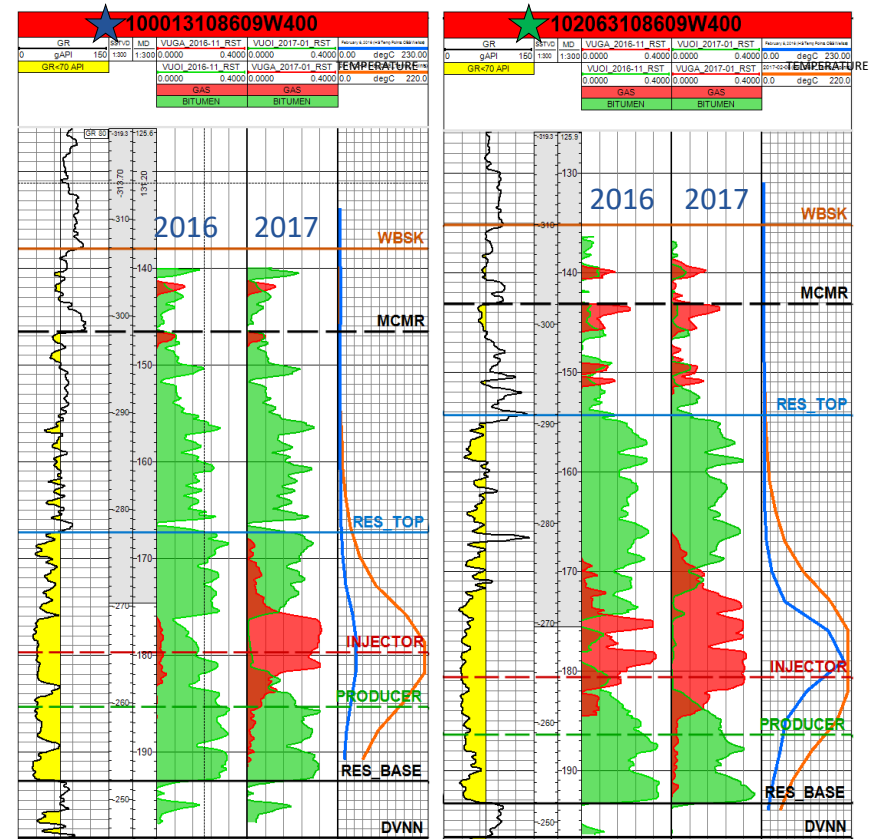
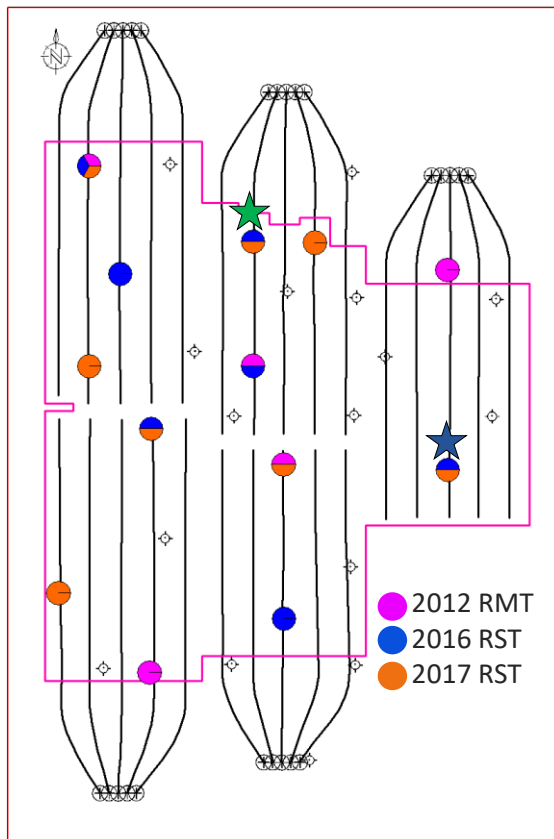
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2018

- No new data acquired in reporting period

HISTORICAL

- Baseline acquired in 2012
- 2016 acquired 7 saturation logs; 2017 acquired 8 saturation logs
- RST results show steam chamber thickness correlates with observation well temperature profiles



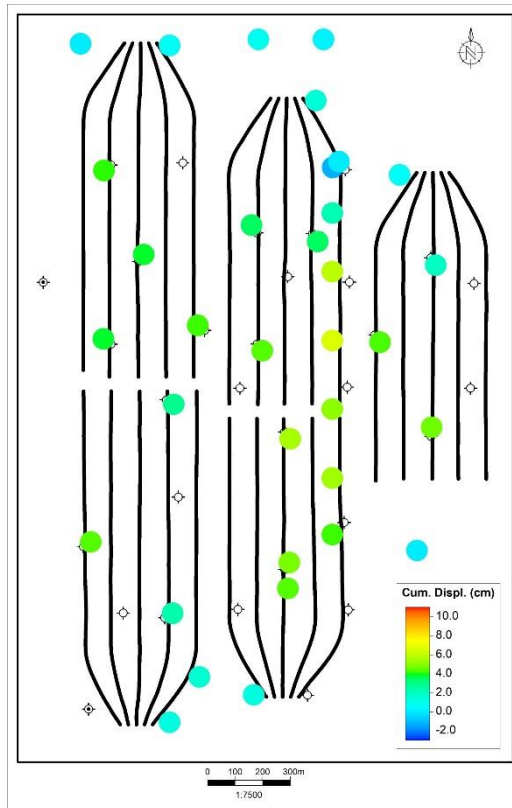
PROGRAM DESIGN

- 31 permanent surface heave monuments (0.30 x 0.30 m plate)
- Real-time Kinematic (RTK) survey method was used, survey tolerance range is +/- 2 cm

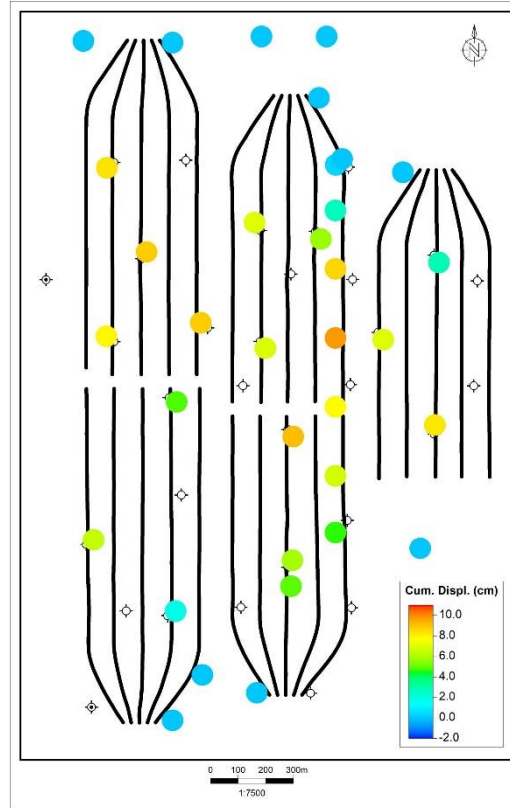
SURVEY/RESULTS

- During 2018 the maximum change observed was 7 cm over Pad AD
- The maximum change observed between February 2015 and January 2018 was 9 cm

2017-18 Cumulative Displacement, cm



2015-18 Cumulative Displacement, cm



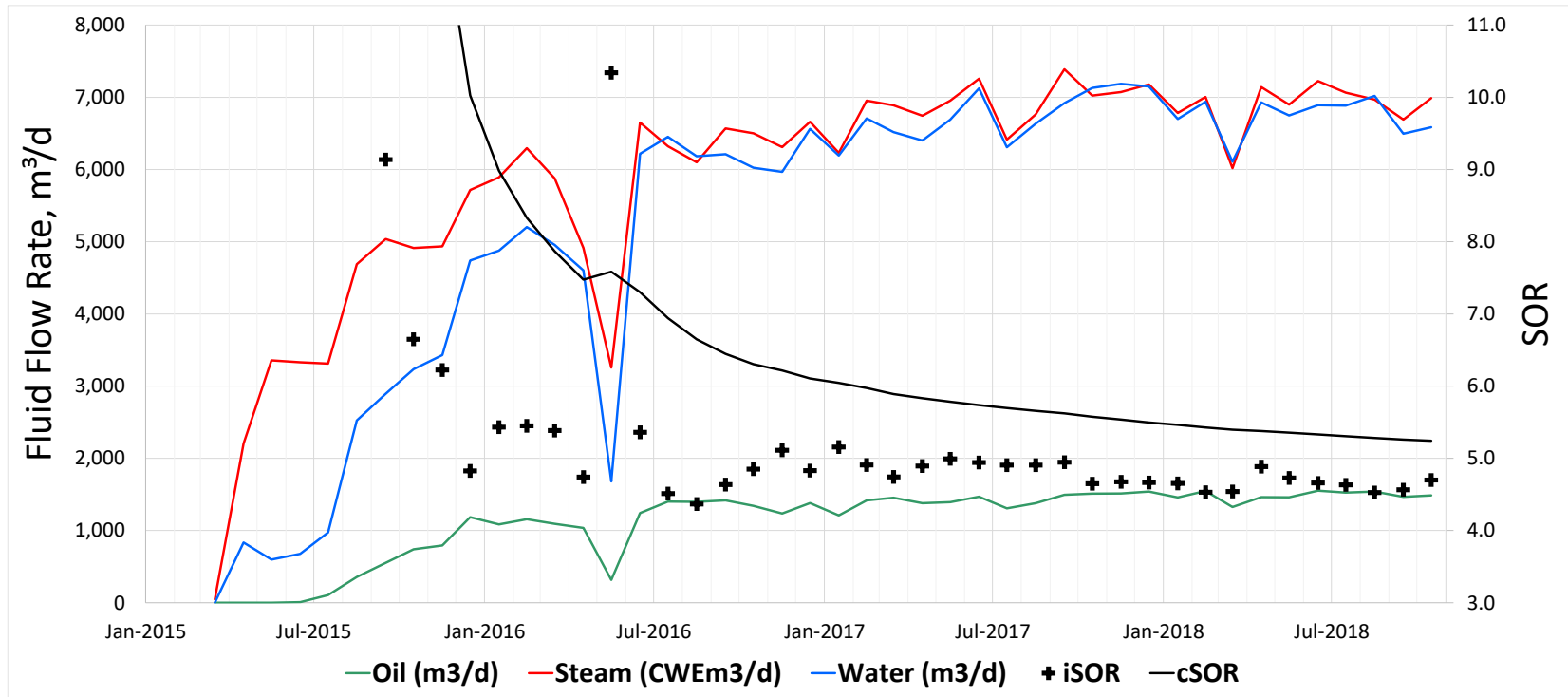
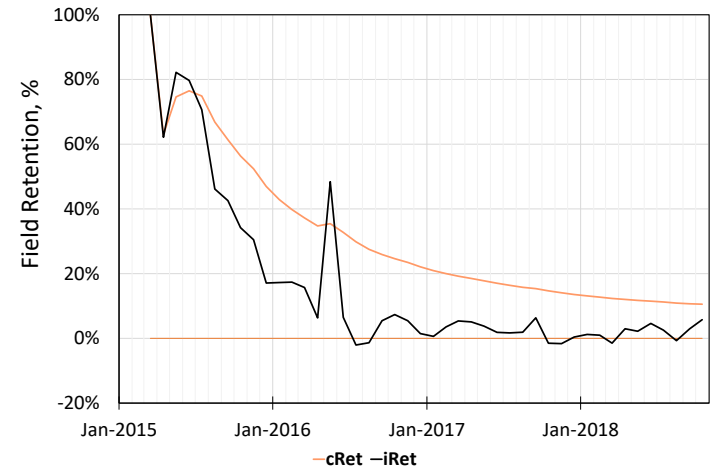


SUBSURFACE

SCHEME PERFORMANCE

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- Field continuing to ramp-up
 - Currently 24 of the 25 SAGD well pairs on production
 - Injectors have reached target operating pressure
 - SOR declining as upper portions of the reservoir begin to drain
 - FCD installed on AB04
 - AA05 brought on-stream
- Maximum monthly bitumen rate 1,551 m³/d (9,754 bbl/d) with SOR of 4.7 (Jun 2018)



Pad	Well Pairs	Average Lateral Length (m)	Average Net Pay above Producer (m)	Oil Saturation (frac)	Total Net Pay Porosity (frac)	OBIP (10 ⁶ m ³)	Current Recovered ¹ (10 ⁶ m ³)	Current Recovery Factor (%)	Predicted Recovery Factor (%)
AA	4/5	850	23.7	0.71	0.35	3.3	0.21	6.5	50-70
AB	5/5	640	22.4	0.73	0.37	2.9	0.54	18.7	50-70
AC	5/5	750	24.3	0.70	0.36	3.0	0.20	6.7	50-70
AD	5/5	670	26.2	0.71	0.35	3.2	0.26	8.2	50-70
AE	5/5	830	22.6	0.70	0.35	3.2	0.29	9.1	50-70
TOTAL	24/25					15.6	1.51	9.7	50-70

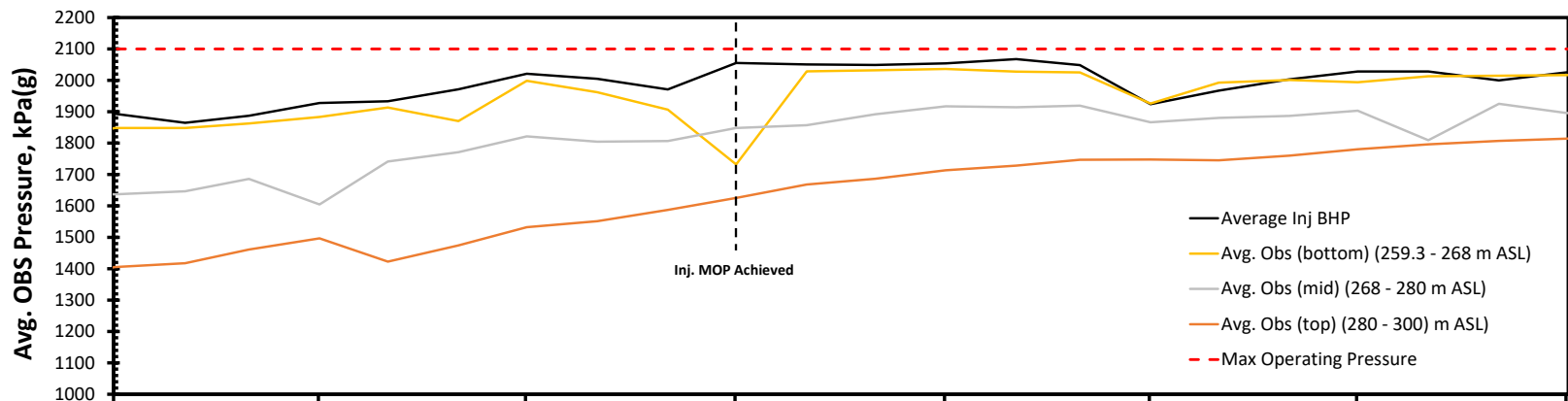
¹ Recovery Factor based on cumulative oil production in Oct 2018

Notes:

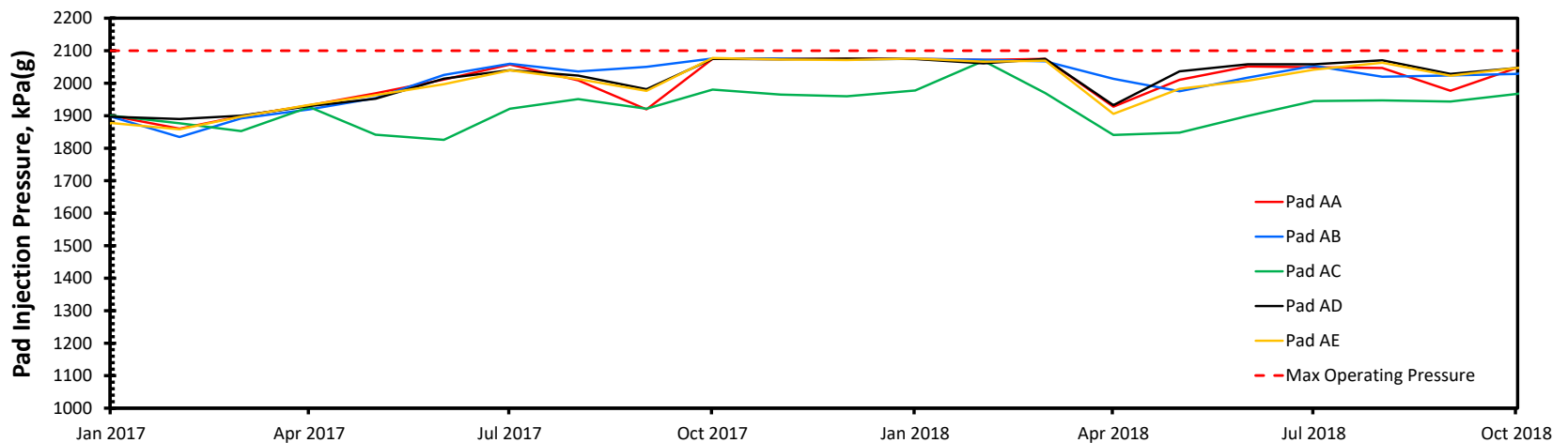
- Well Spacing: 100 m, Spacing between pads: 130 m
- Volumetrics include 25 m at heel and toe of the well pair
- OBIP is gross oil volume between base and top of pay
- Predicted recovery factor accounts for drainage through the low bitumen saturation zone and from the IHS

- Approved Maximum Operating Pressure is 2,100 kPag
- Throughout the reporting period, the reservoir continues pressuring up
 - *Pressure data shows vertical and horizontal pressure communication throughout the entire pay interval across entire field*
- No pressure change in caprock

Average daily field pressure at base, middle and top of reservoir



Average daily injection pressure in each Pad

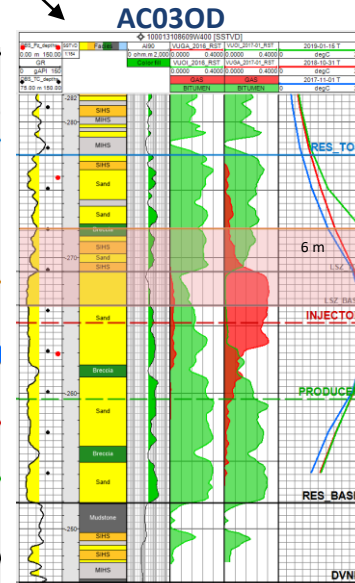
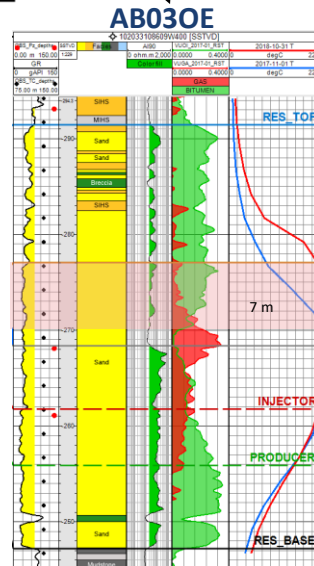
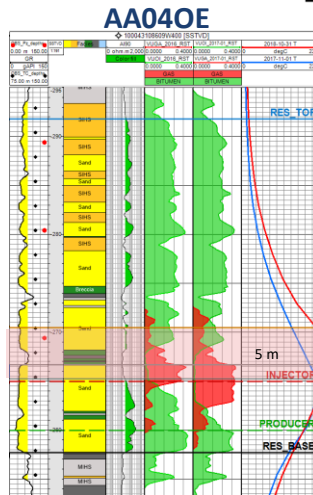
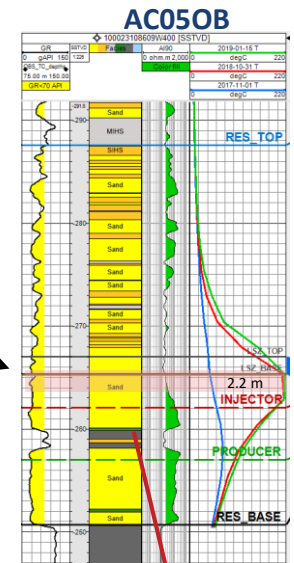
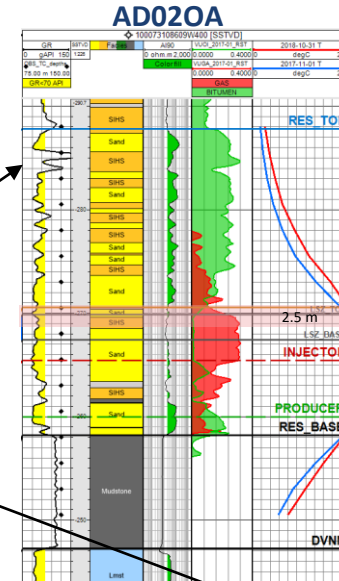
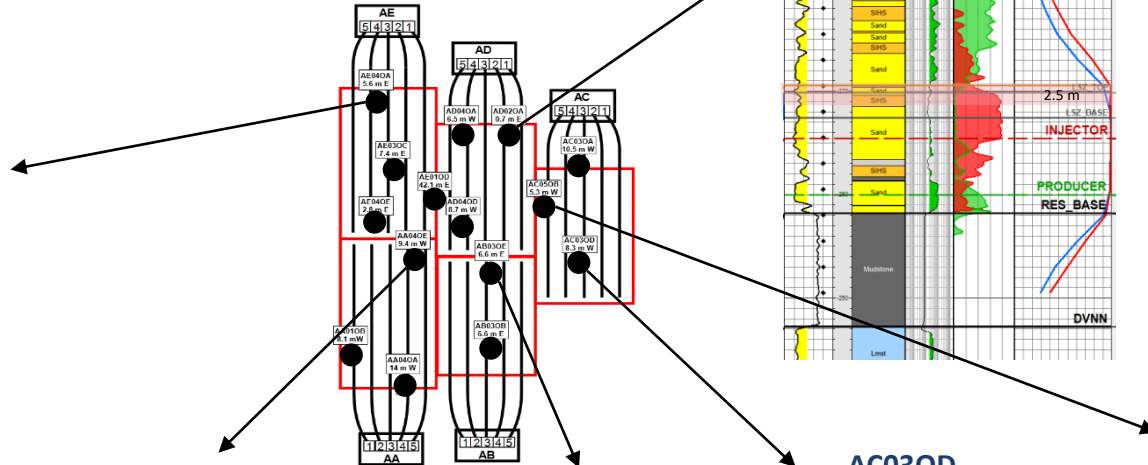
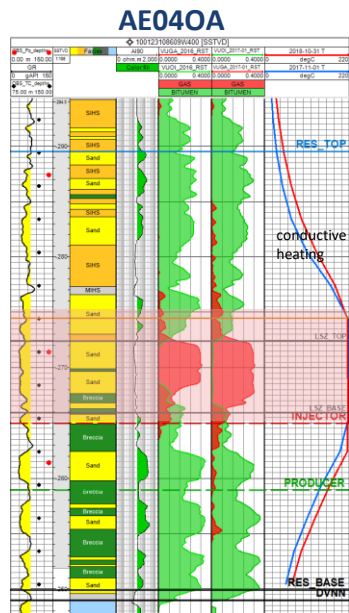


STEAM CHAMBER PROGRESSION IN OBSERVATION WELLS

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PROGRESSING THROUGH IHS

- Significant steam chamber growth through the Low Bitumen Saturation Zone and into the IHS across all pads in 2018
- Conductive heating into IHS observed in all OBS wells



Temperature Plots

- Nov 1, 2017
- Oct 31, 2018
- Jan 15, 2019
- Low Saturation Zone
- Top of Steam Chamber
- Steam chamber growth

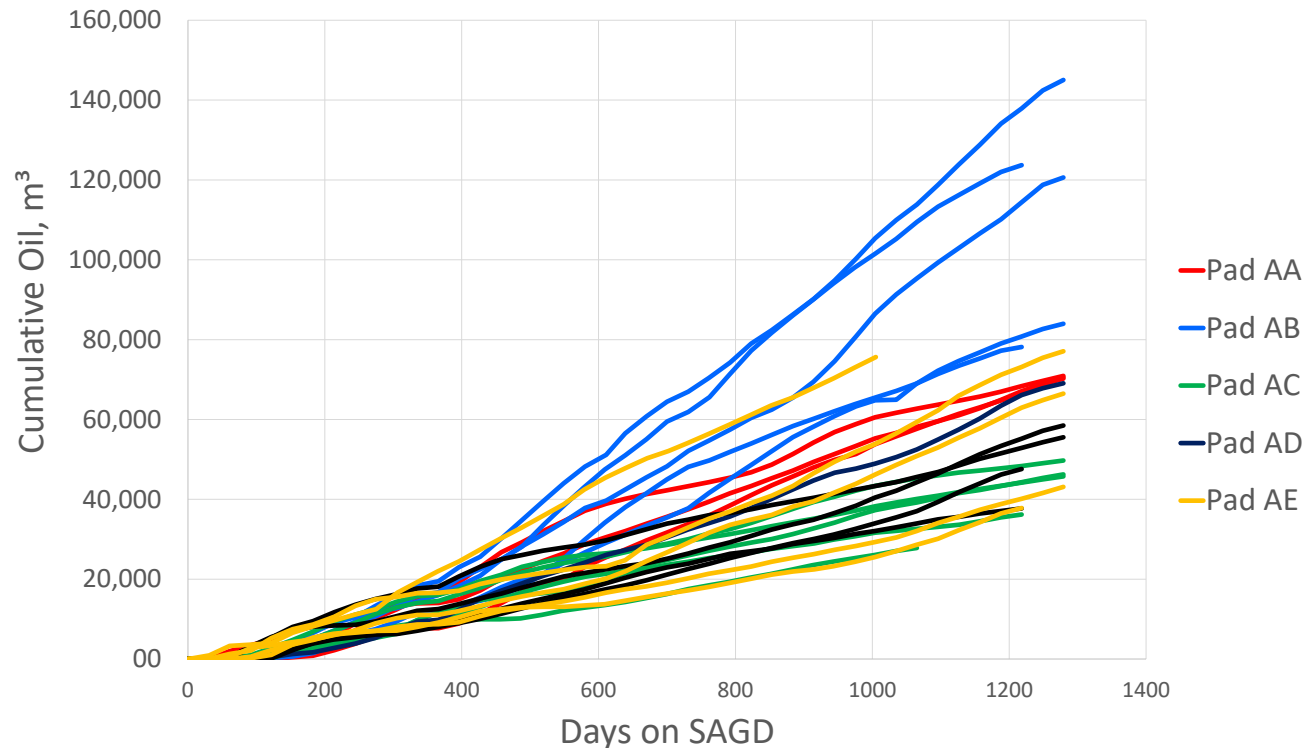
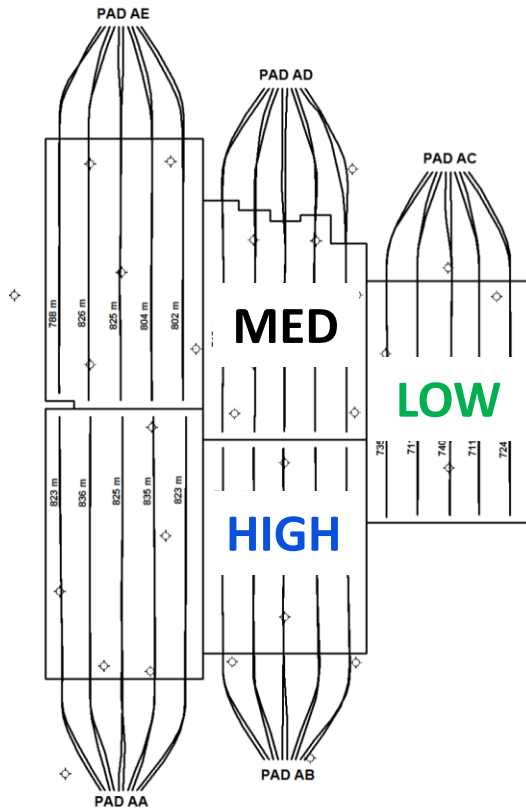
FACIES

Sand	
SHS	
MHS	
Breccia	
Mudstone	
Lmst	



AC050B: Steam chamber development above mudstone in September; 1 to 2 m mudstone acted as a baffle, not barrier, to flow

- Variation of pad performance depends on geology, pad boundary, well pair trajectories, pump performance and subcool conformance
 - *Pads AB, AD and AE selected as examples of high/medium/low performing pads*
 - *Selection based on cumulative oil recovery and cSOR*
 - *Differences in the productivity of the wells primarily due to geological variability*



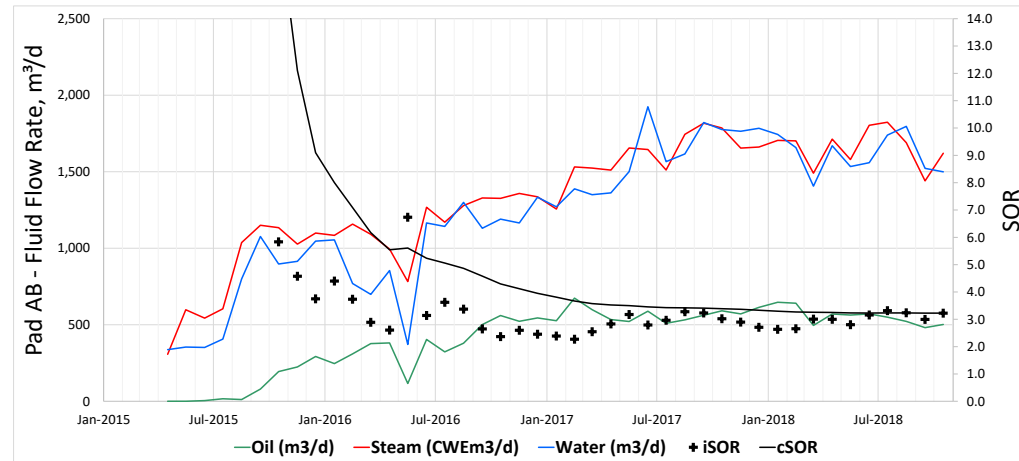
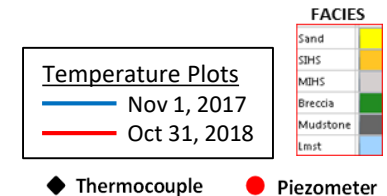
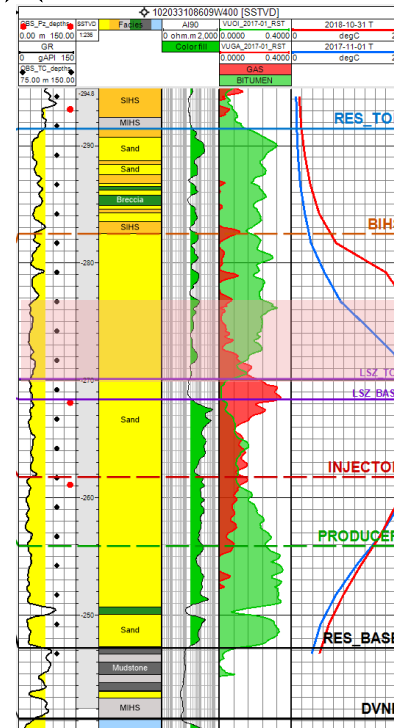
PAD AB

- Cumulative production: 543,061 m³
- Highest reservoir quality
 - Mostly sandy reservoir
 - High oil saturation around well pairs
 - Thin low bitumen saturation zone
- Highest average effective wellbore (97%)
- Peak well pair monthly rates >1,000 bbl/d

CHANGES SINCE LAST REPORTING PERIOD¹

- Oil: relatively constant at 3,523 bbl/d (+0.4%)
- Oil Cut: decreased from 27% to 25.5% (-6%)
- cSOR: decreased from 3.4 to 3.2 (-6%)
- Significant steam chamber development
 - Well AB03OE shows 7 m steam chamber rise near toe of AB03
- Pressure increase at top of reservoir through IHS

AB03OE, 102/03-31-86-09W4 TOE (6.6m OFFSET)



¹ Annualized: (Nov 2016 – Oct 2017) to (Nov 2017 – Oct 2018)

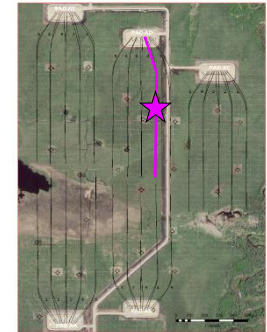
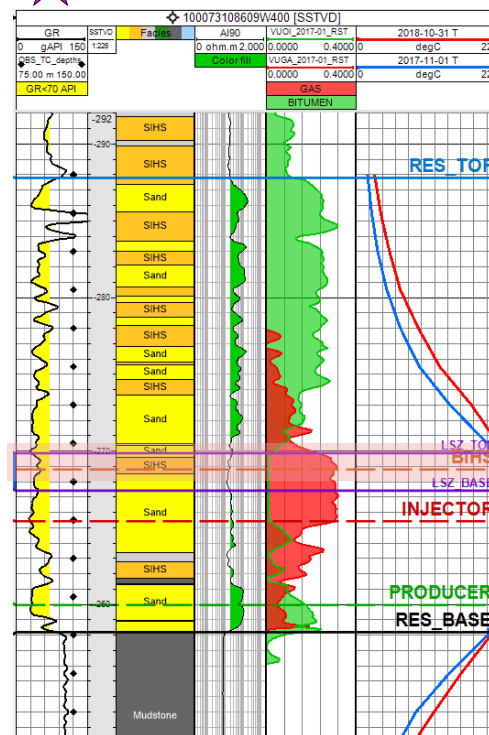
PAD AD

- Cumulative production: 262,614 m³
- Average reservoir quality
 - Thickest net pay (26.2 m)
 - IHS with high oil saturation in upper reservoir
 - Thick low bitumen saturation zone above injection well
- Shortest wells
- Most bounded pad
- High average effective wellbore (96%)

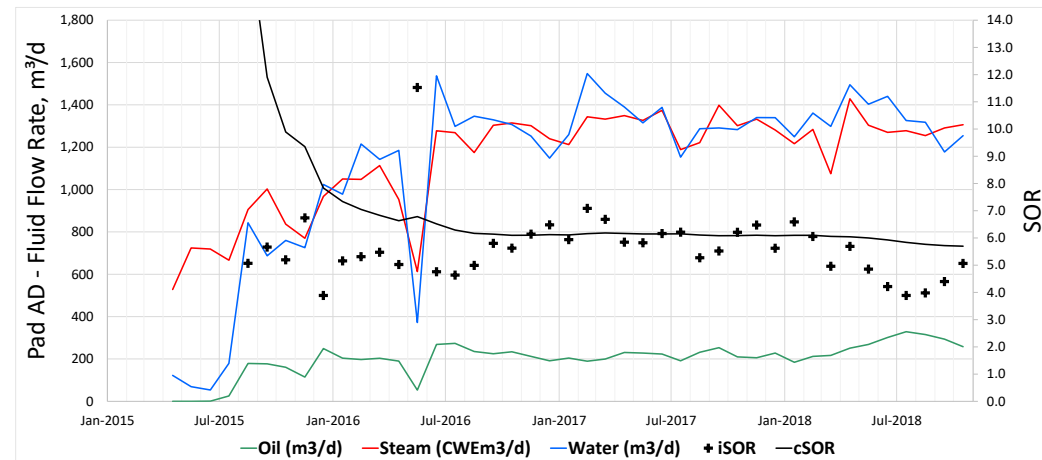
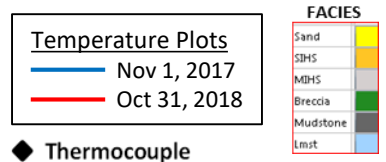
CHANGES SINCE LAST REPORTING PERIOD¹

- Oil: increased from 1,344 to 1,607 bbl/d (+20%)
- Oil Cut: increased from 14.0% to 16.1% (+15%)
- cSOR: decreased from 6.1 to 5.7 (-7%)
- Well AD02OA shows 2.5m steam chamber development at heel of AD02
 - Temperature increase through IHS
 - Steam chamber advancing through LSZ
- Increased contribution from upper reservoir (IHS) resulting in improved rates and oil cut

AD02OA, 100/07-31-86-09W4 HEEL (0.7 m OFFSET)



2.5 m steam growth



* Annualized: (Nov 2016 – Oct 2017) to (Nov 2017 – Oct 2018)

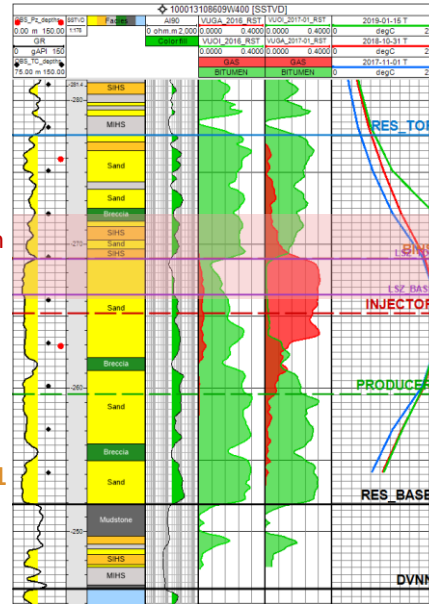
PAD AC

- Cumulative production: 201,960 m³
- Heterogeneous reservoir
 - IHS dominated
 - Thin low bitumen saturation zone above injection well
- Bounded at east of pad
- Sharing west boundary with pads AB and AD

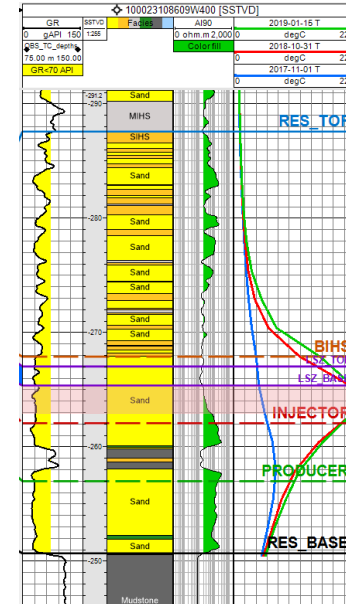
CHANGES SINCE LAST REPORTING PERIOD¹

- Oil: relatively constant at 978 bbl/d (-2%)
- Oil Cut: unchanged from 14.2%
- cSOR: increased from 6.0 to 6.4 (+6%)
- OBS wells AC03OD and AC05OB show appreciable steam chamber progression over the year
 - AC03OD passed through LSZ and is now advancing through SIHS and Breccia
 - AC05OB shows drainage around a thick mudstone between the Producer and Injector, proving its limited lateral extent.

★ AC03OD, 100/01-31-86-09W4
TOE (8.3 m OFFSET)



★ AC05OB, 100/02-31-86-09W4
MID (5.3 m OFFSET)

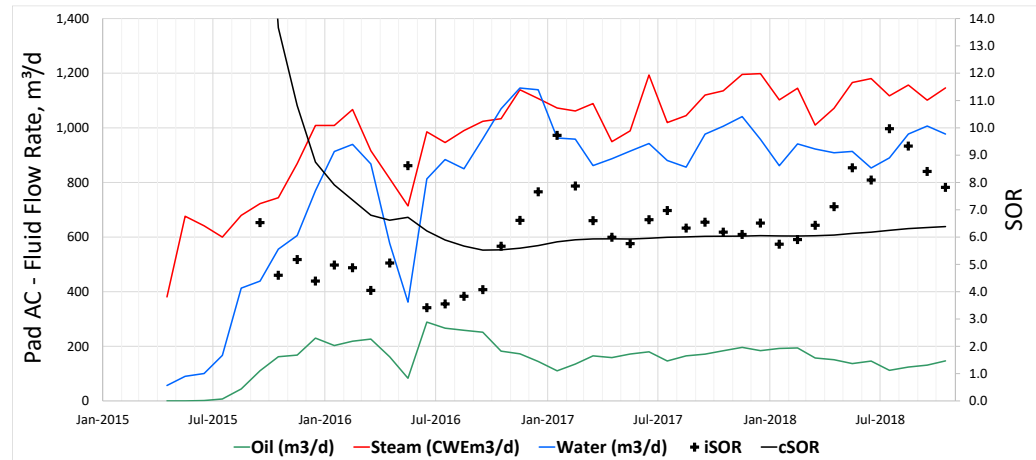


FACIES	
Sand	Yellow
SIHS	Light Green
MHHS	Dark Green
Breccia	Dark Grey
Mudstone	Light Blue
Limit	Blue

Temperature Plots

- Nov 1, 2017 (Blue line)
- Oct 31, 2018 (Red line)
- Jan 15, 2019 (Green line)

◆ Thermocouple ● Piezometer



¹ Annualized: (Nov 2016 – Oct 2017) to (Nov 2017 – Oct 2018)

STEAM QUALITY

- Steam quality leaving the plant is approximately 98% (incl. Continuous Blow Down (CBD) at typically 6,000 kPag
- Steam quality decreases to wellheads and is not measured but is modeled to be ~95%
- These conditions align with the original design

WELL INTEGRITY

- Well integrity is addressed by using thermally engineered casing, thermal cement and completing cement bond logs in accordance with Directive 051
 - No wellbore integrity failures during the reporting period
 - No non-compliances of reporting and repairing wellbore integrity issues during the reporting period
- AOC has in place a wellhead valve maintenance program to prevent wellhead valve failures
 - No wellhead failures during the reporting period

ABANDONMENTS

- No wells have been abandoned or suspended within the project area to date

- No plans for the drilling of any new SAGD well pairs for next reporting period
- No abandonments planned in the next 5 years
- Production assurance well AA03 to be brought online pending steam availability
- Expect to convert remaining active PCP wells to ESPs as required
- Evaluating opportunities for Flow Control Devices (FCDs) into producer wells



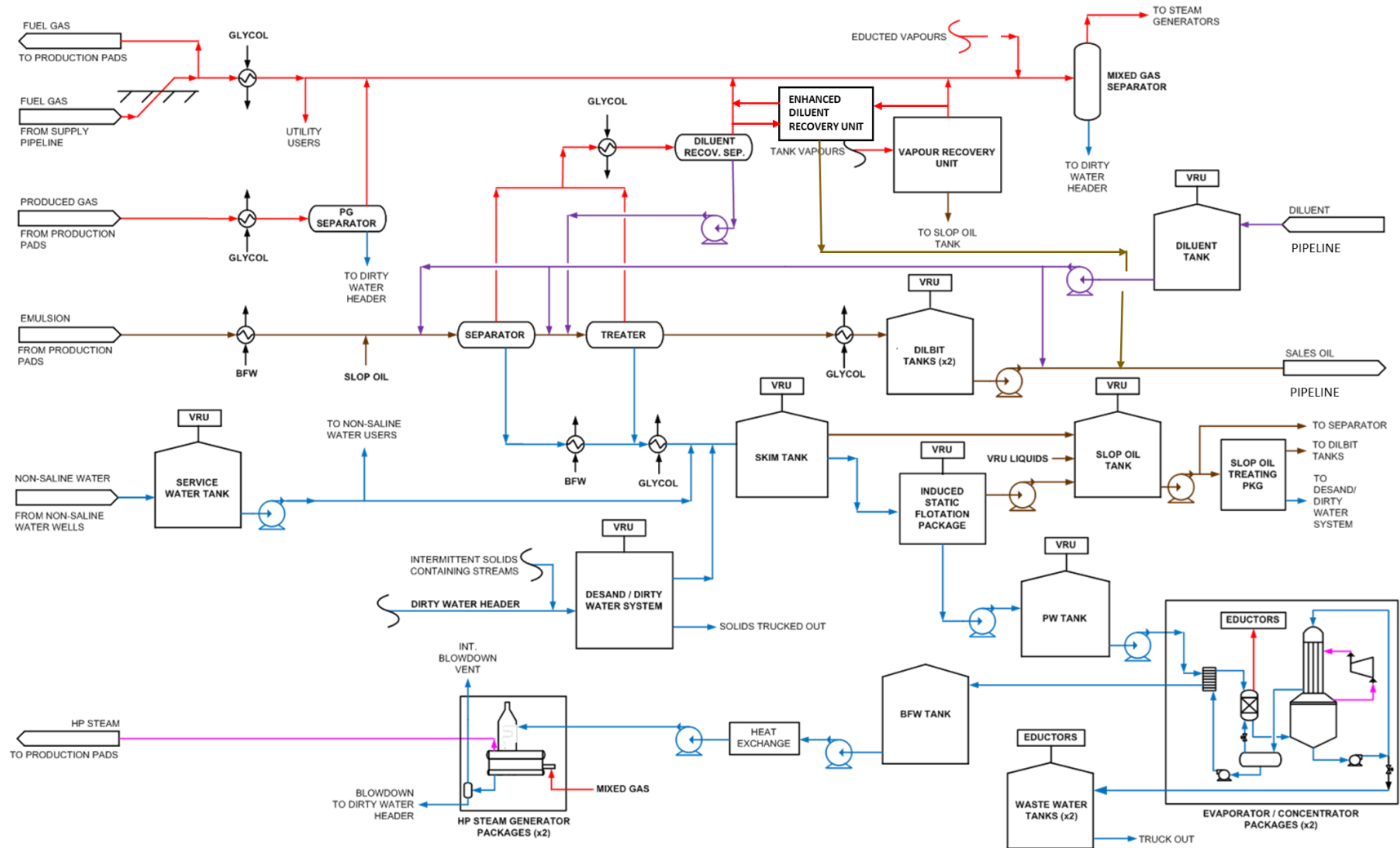
SURFACE OPERATIONS

FACILITIES

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- [illegible]

- No modifications during this reporting period





SURFACE

MEASUREMENT, ACCOUNTING AND REPORTING PLAN (MARP)

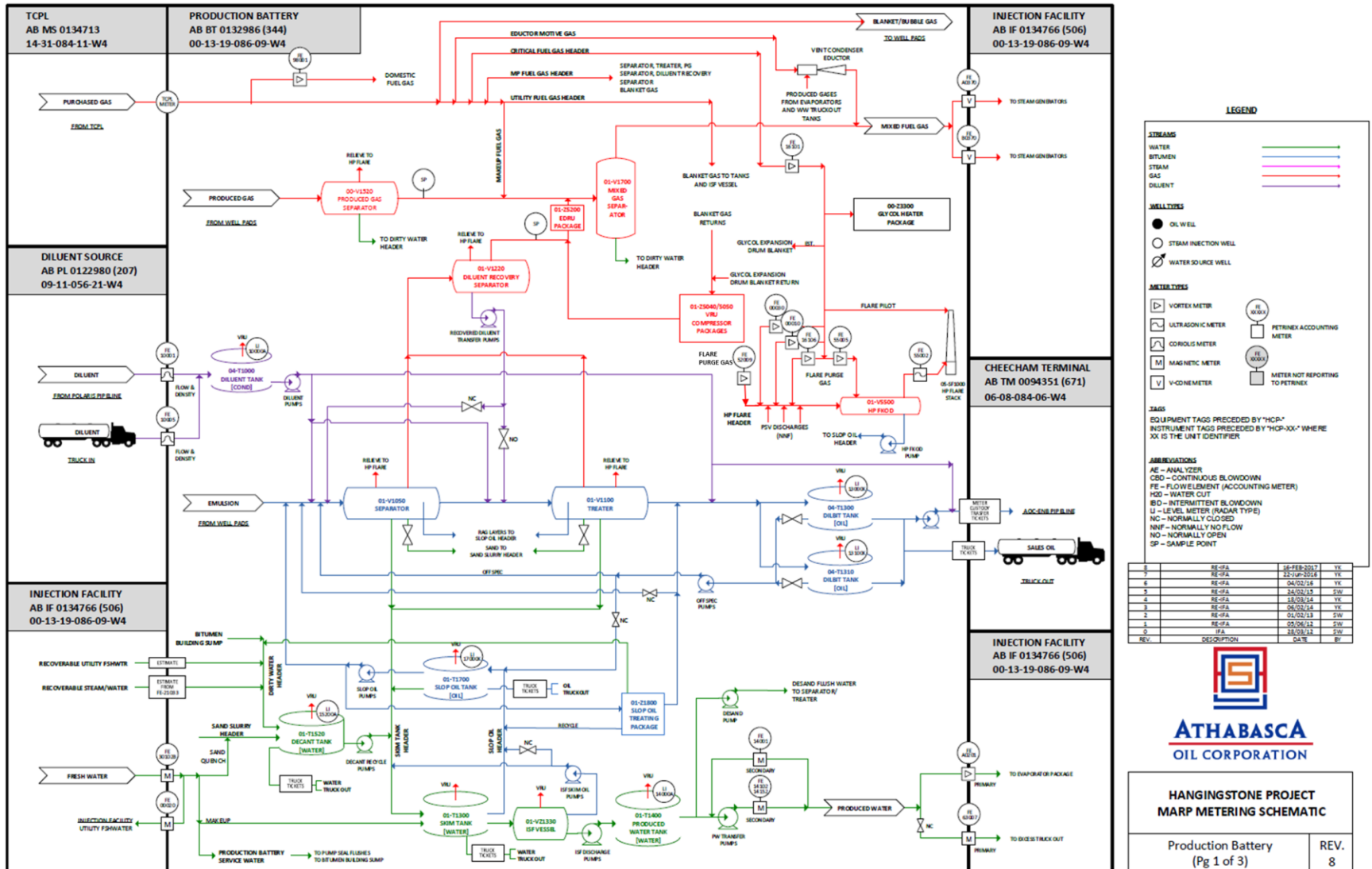
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OIL CORPORATION

MEASUREMENT, ACCOUNTING AND REPORTING PLAN (MARP)

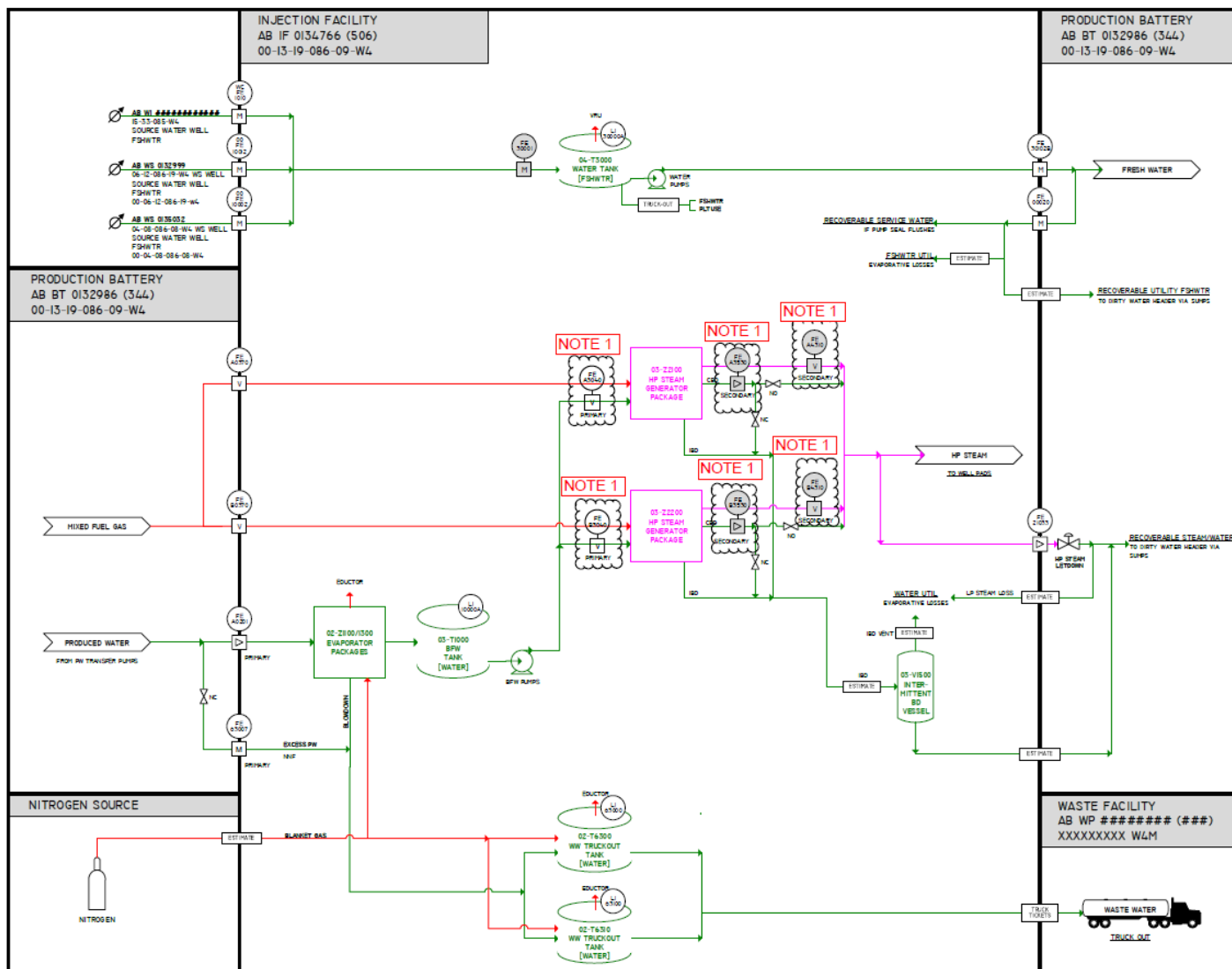
- MARP approved October 5, 2012
- MARP variance for steam measurement meters approved in 2017
- No changes or alterations made during the 2018 reporting period

MEASUREMENT SCHEMATICS – BATTERY

43



MEASUREMENT SCHEMATICS – INJECTION FACILITY 44



NOTES:

1. NAMING OF PRIMARY & SECONDARY METERS HAS CHANGED

LEGEND

STREAMS			
WATER			
STEAM			
GAS			
DILUENT			
WELL TYPES			
METER TYPES			
TAGS			
EQUIPMENT TAGS PRECEDED BY "HOP" INSTRUMENT TAGS PRECEDED BY "HOP-XX" WHERE XX IS THE UNIT IDENTIFIER			
ABBREVIATIONS			
AE	- ANALYZER		
CBO	- CONTINUOUS BLOWDOWN		
FE	- FLOW ELEMENT (ACCOUNTING METER)		
HO	- WATER OUT		
BO	- INTERMITTENT BLOWDOWN		
U	- LEVEL METER (RIGHT TYPE)		
NC	- NORMALLY CLOSED		
NNF	- NORMALLY NO FLOW		
NO	- NORMALLY OPEN		
SP	- SAMPLE POINT		
REV.	DESCRIPTION	DATE	BY
1	RE-FA	16-FEB-2017	YN
2	RE-FA	22-JUN-2016	YN
3	RE-FA	06-02/16	YN
4	RE-FA	24-02/16	SW
5	RE-FA	08-02/16	YN
6	RE-FA	06-02/16	YN
7	RE-FA	07-02/15	SW
8	RE-FA	08-09-15	SW
9	FA	28-03/10	SW



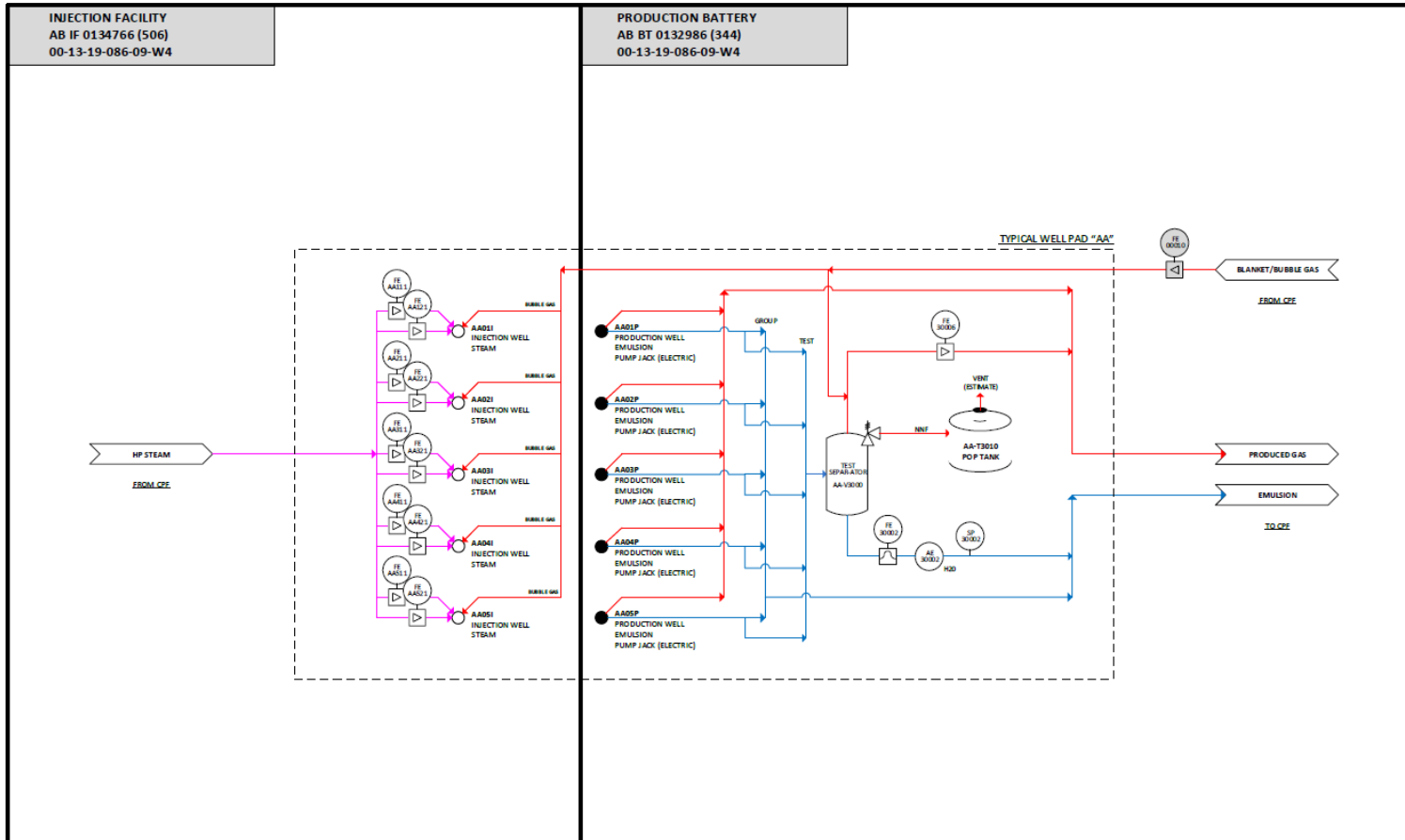
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HANGINGSTONE PROJECT
MARF METERING SCHEMATIC

INJECTION FACILITY (PG 2 OF 3) REV. 8

MEASUREMENT SCHEMATICS – WELL PADS

45



LEGEND

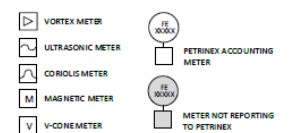
STREAMS



WELL TYPES



METER TYPES



TAGS

EQUIPMENT TAGS PRECEDED BY "HCP-"
 INSTRUMENT TAGS PRECEDED BY "HCP-JK-" WHERE
 XX IS THE UNIT IDENTIFIER

ABBREVIATIONS

AE - ANALYZER
 CBO - CONTINUOUS BLOWDOWN
 FE - FLOW ELEMENT (ACCOUNTING METER)
 H2O - WATER CUT
 IBD - INTERMITTENT BLOWDOWN
 LI - LEVEL METER (RADAR TYPE)
 NC - NORMALLY CLOSED
 NNF - NORMALLY NO FLOW
 NO - NORMALLY OPEN
 SP - SAMPLE POINT

8	RE-FA	16-FEB-2017	YK
7	RE-FA	22-JUN-2016	YK
6	RE-FA	04-02-14	YK
5	RE-FA	24-02-13	SW
4	RE-FA	18-03-14	YK
3	RE-FA	05-02-14	YK
2	RE-FA	05-02-13	SW
1	RE-FA	05-06-12	SW
0	FA	23-03-12	SW
REV	DESCRIPTION	DATE	BY

AOC WELL NAMES AND UNIQUE IDs

PAD AA		PAD AB		PAD AC		PAD AD		PAD AE	
AA01I	105/04-31-086-09W4/0	AB01I	106/03-31-086-09W4/0	AC01I	103/16-30-086-09W4/0	AD01I	109/02-31-086-09W4/0	AE01I	116/03-31-086-09W4/0
AA02I	106/04-31-086-09W4/0	AB02I	107/03-31-086-09W4/0	AC02I	100/16-30-086-09W4/0	AD02I	108/02-31-086-09W4/0	AE02I	114/04-31-086-09W4/0
AA03I	107/04-31-086-09W4/0	AB03I	108/03-31-086-09W4/0	AC03I	102/16-30-086-09W4/0	AD03I	118/03-31-086-09W4/0	AE03I	113/04-31-086-09W4/0
AA04I	108/04-31-086-09W4/0	AB04I	103/02-31-086-09W4/0	AC04I	102/15-30-086-09W4/0	AD04I	117/03-31-086-09W4/0	AE04I	112/04-31-086-09W4/0
AA05I	103/03-31-086-09W4/0	AB05I	104/02-31-086-09W4/0	AC05I	100/15-30-086-09W4/0	AD05I	105/03-31-086-09W4/0	AE05I	104/04-31-086-09W4/0
AA01P	103/04-31-086-09W4/0	AB01P	109/03-31-086-09W4/0	AC01P	106/16-30-086-09W4/0	AD01P	102/02-31-086-09W4/0	AE01P	104/03-31-086-09W4/0
AA02P	109/04-31-086-09W4/0	AB02P	110/03-31-086-09W4/0	AC02P	105/16-30-086-09W4/0	AD02P	107/02-31-086-09W4/0	AE02P	117/04-31-086-09W4/0
AA03P	110/04-31-086-09W4/0	AB03P	111/03-31-086-09W4/0	AC03P	104/16-30-086-09W4/0	AD03P	115/03-31-086-09W4/0	AE03P	118/04-31-086-09W4/0
AA04P	111/04-31-086-09W4/0	AB04P	105/02-31-086-09W4/0	AC04P	104/15-30-086-09W4/0	AD04P	114/03-31-086-09W4/0	AE04P	116/04-31-086-09W4/0
AA05P	112/03-31-086-09W4/0	AB05P	106/02-31-086-09W4/0	AC05P	103/15-30-086-09W4/0	AD05P	113/03-31-086-09W4/0	AE05P	115/04-31-086-09W4/0



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**HANGINGSTONE PROJECT
 MARP METERING SCHEMATIC**

Well Pads
 (Pg 3 of 3)

REV.
 8

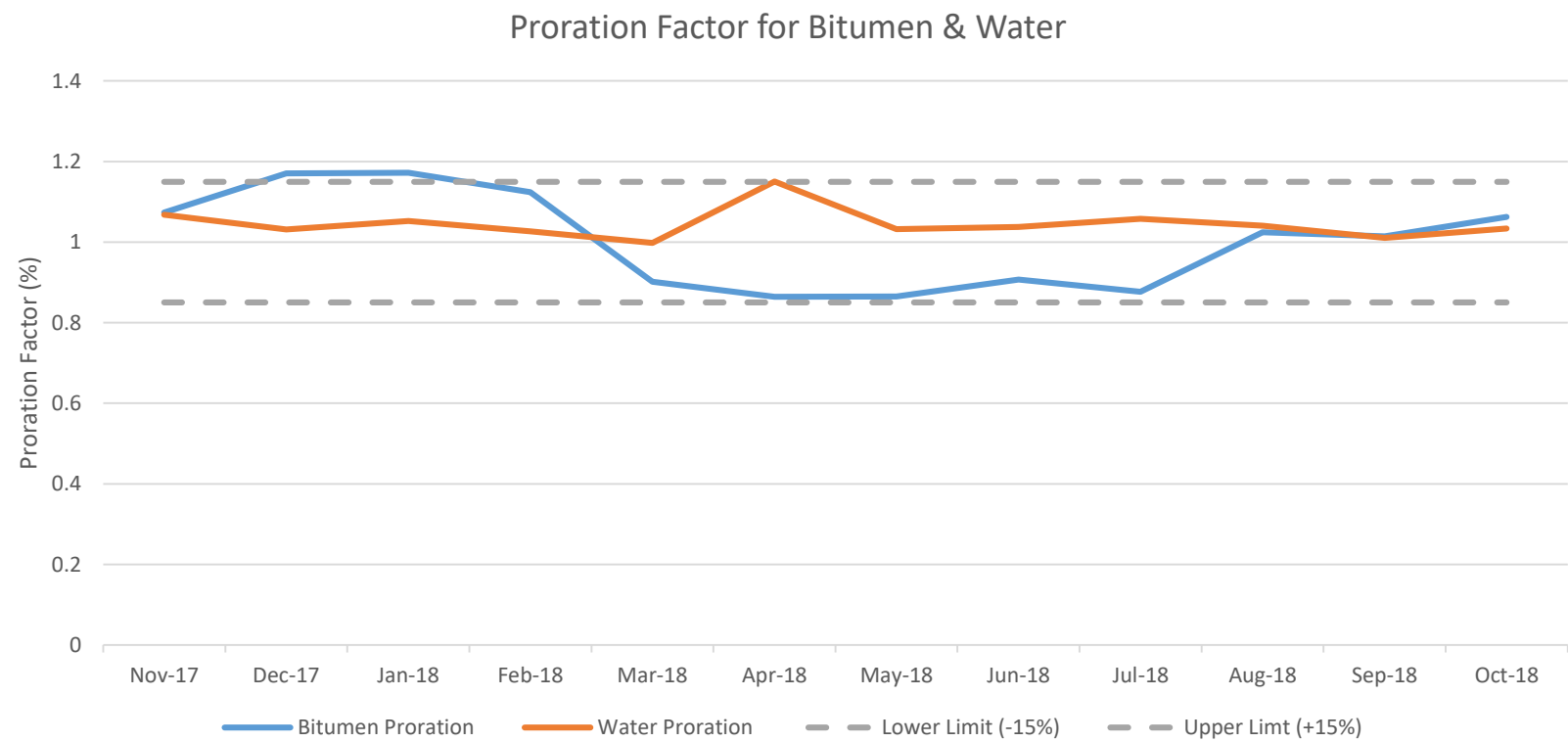
2018

- No changes or alterations made to measurement methodology in reporting period

MEASUREMENT METHODOLOGY

- WELL PRODUCTION AND INJECTION VOLUMES
 - *Each well pad has a dedicated test separator with liquid flow meter and water cut analyzer to determine well bitumen and water production*
 - *Wells are individually put on test for one valid testing hour for every 20 hours of operation*
 - *Valid well test criteria per approved MARP*
 - *Well gas production prorated from Battery Level GOR using a proration factor of 1*
 - *Battery Level GOR is updated monthly*
 - *Steam injection is metered at each individual wellhead. Primary and secondary steam production metering available at the central steam plant*
- BATTERY SALES OIL
 - *Sales oil is shipped via pipeline from the Hangingstone Battery. Custody transfer metering is done at receiving facility*
- MEASUREMENT TECHNOLOGY
 - *Well testing uses standard method of test separators with microwave water cut analyzers*
- STEAM VOLUMES
 - *Steam quality leaving the plant is approximately 98%*
 - *A continuous blowdown (CBD) of approximately 2% is added to the steam of each boiler and is injected into the wells*
 - *Intermittent blow down (IBD) flow is estimated at 0.02% of total water out of the facility using sound engineering practices*
- PRODUCED WATER VOLUMES
 - *Calculated using the measured Water Disposition to the Injection Facility plus the Water Dispositions from the Plant plus and changes in Water Inventory less any Water Receipts*

PRORATION OF BITUMEN AND WATER





SURFACE OPERATIONS

FACILITY PERFORMANCE

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SITE RELIABILITY > 95%

- Based on steam performance
- Integrity management program and predictive maintenance programs have been implemented to maintain higher site reliability

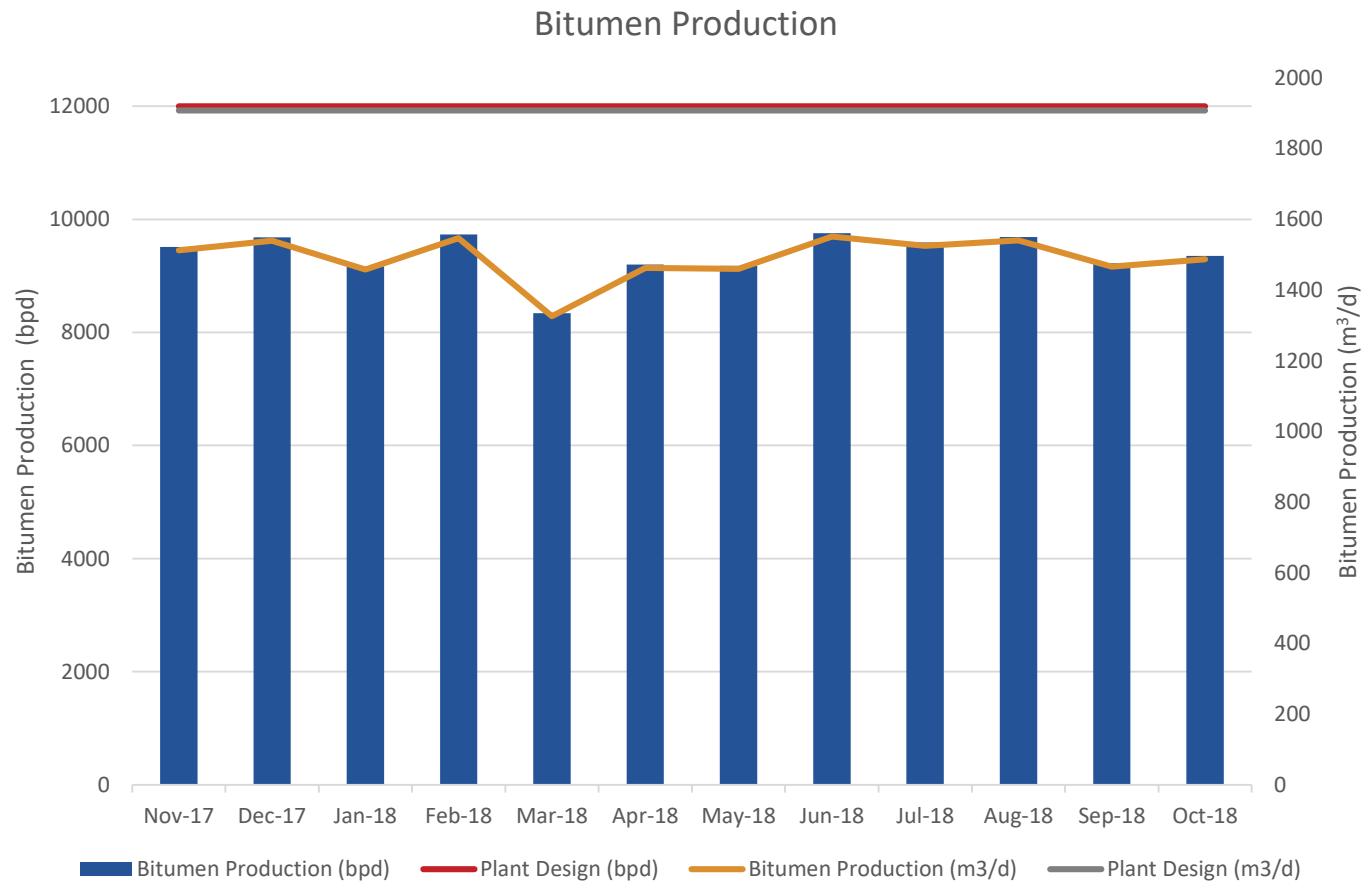
MAJOR ACTIVITIES

- Boiler Mechanical Cleaning
- Evaporator Mechanical Cleaning

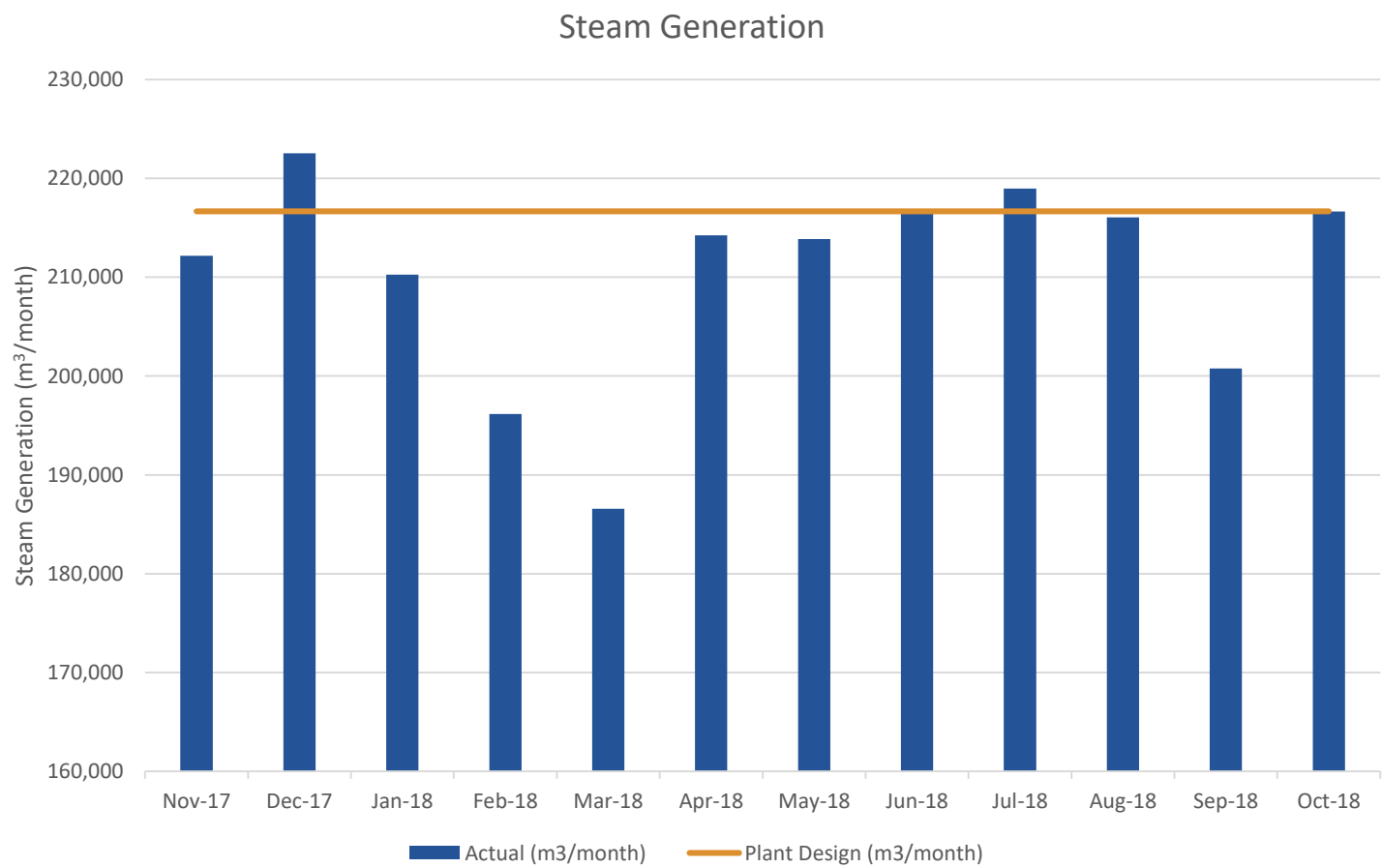
MAJOR CHALLENGES

- De-oiling optimization

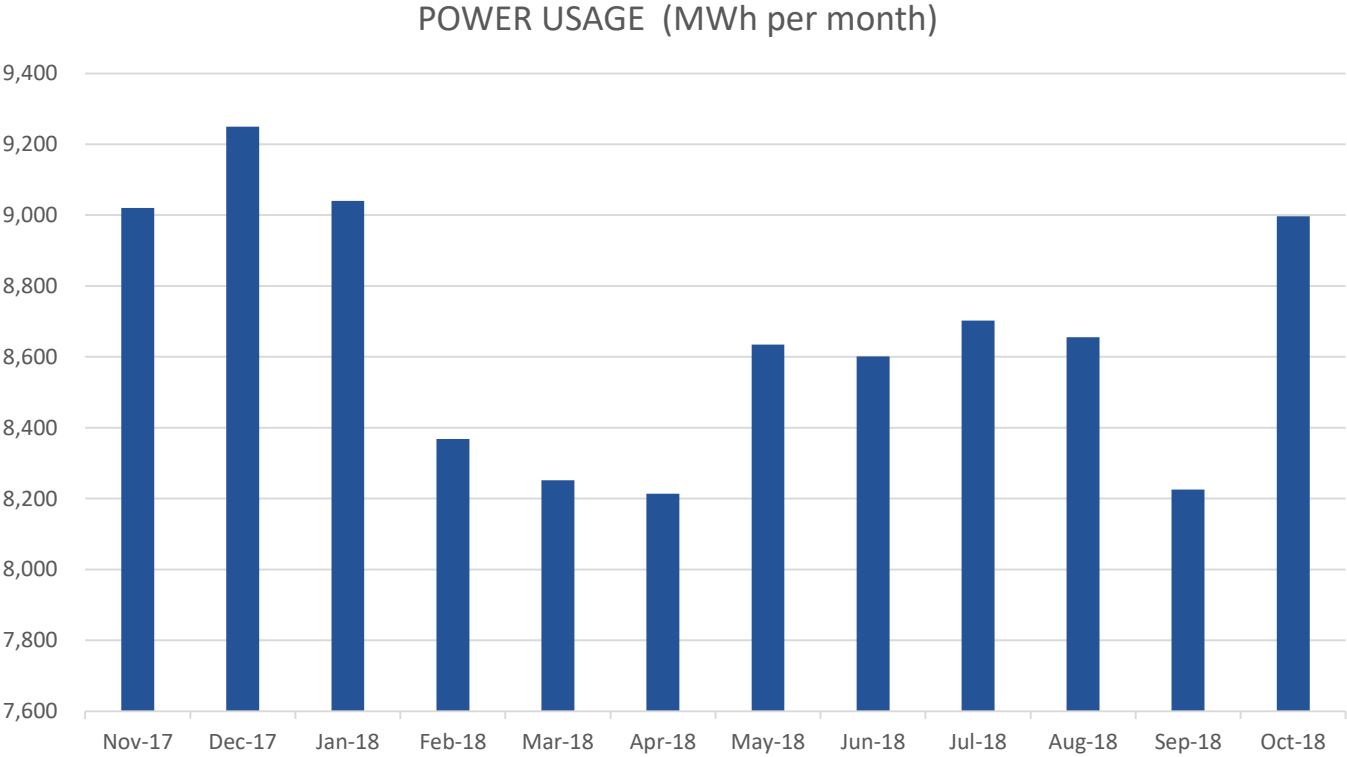
BITUMEN PRODUCTION



STEAM GENERATION

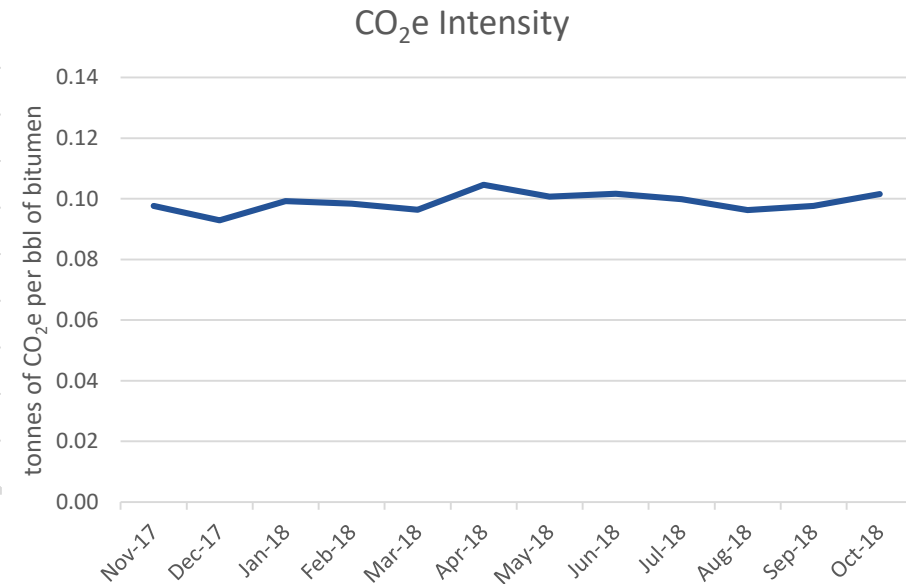
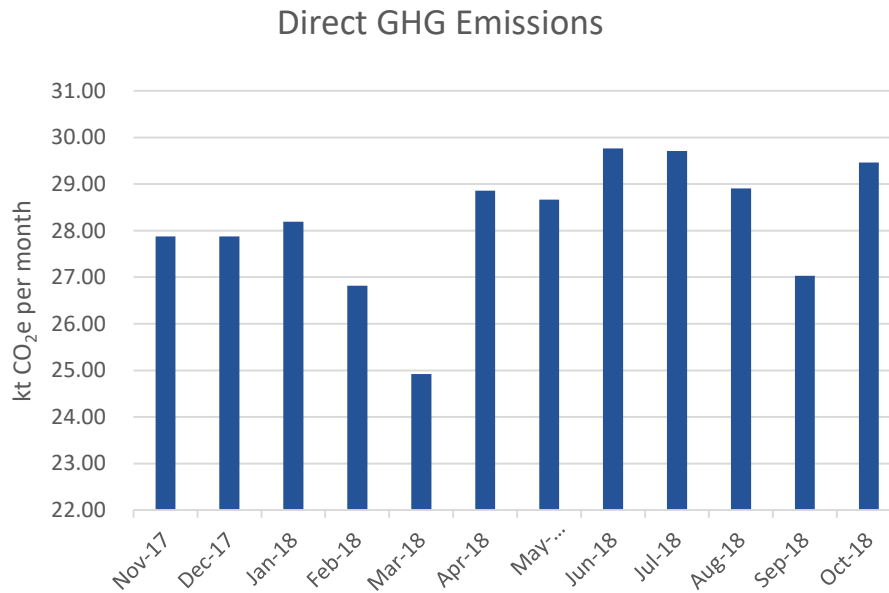


POWER USAGE YTD 103,961 MWH



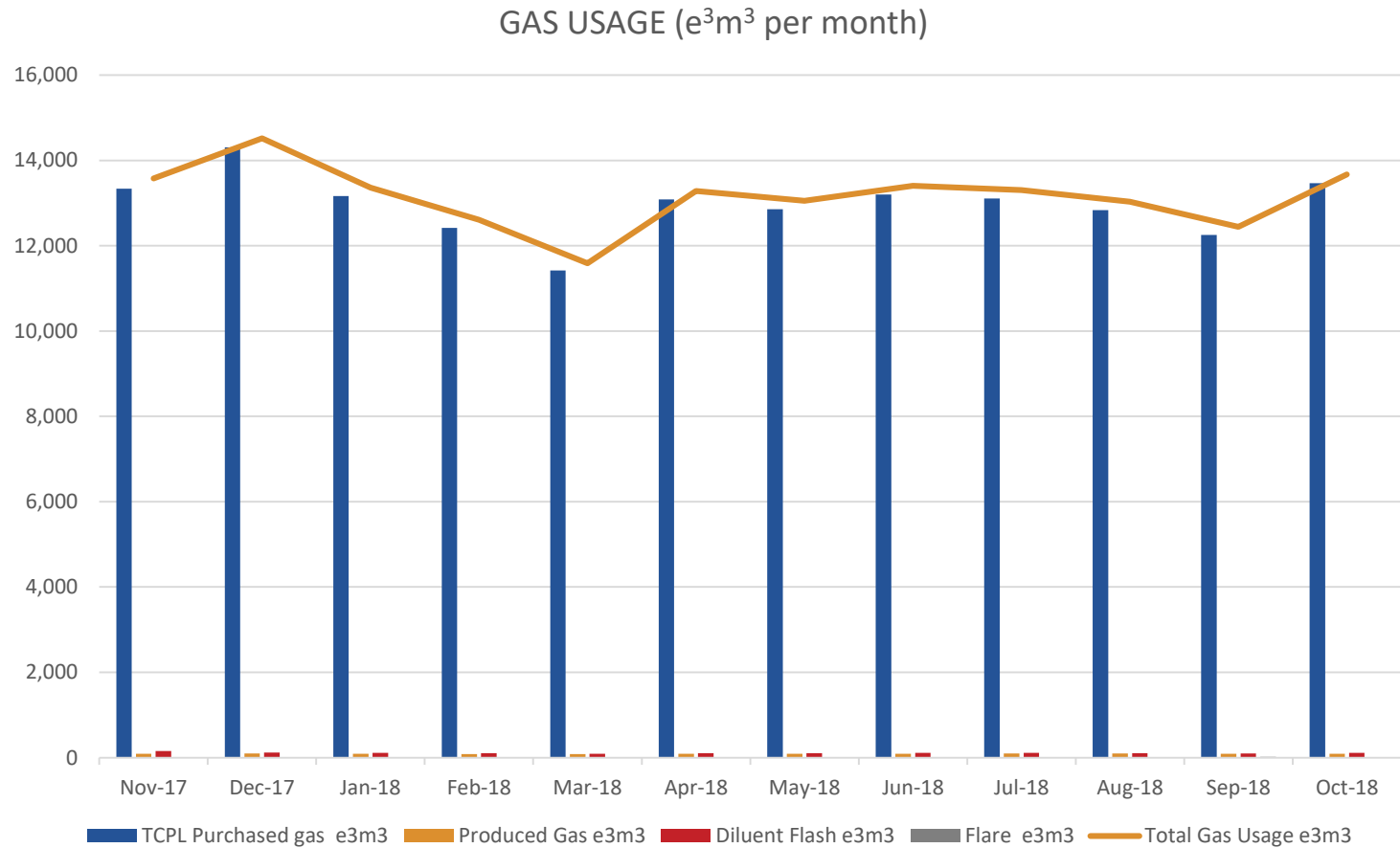
DIRECT GHG EMISSIONS FROM NOVEMBER 2017 – OCTOBER 2018 : 338 KT CO₂e

- Sources: stationary combustion, flaring, venting and fugitives
- Calculated using 2018 CCIR

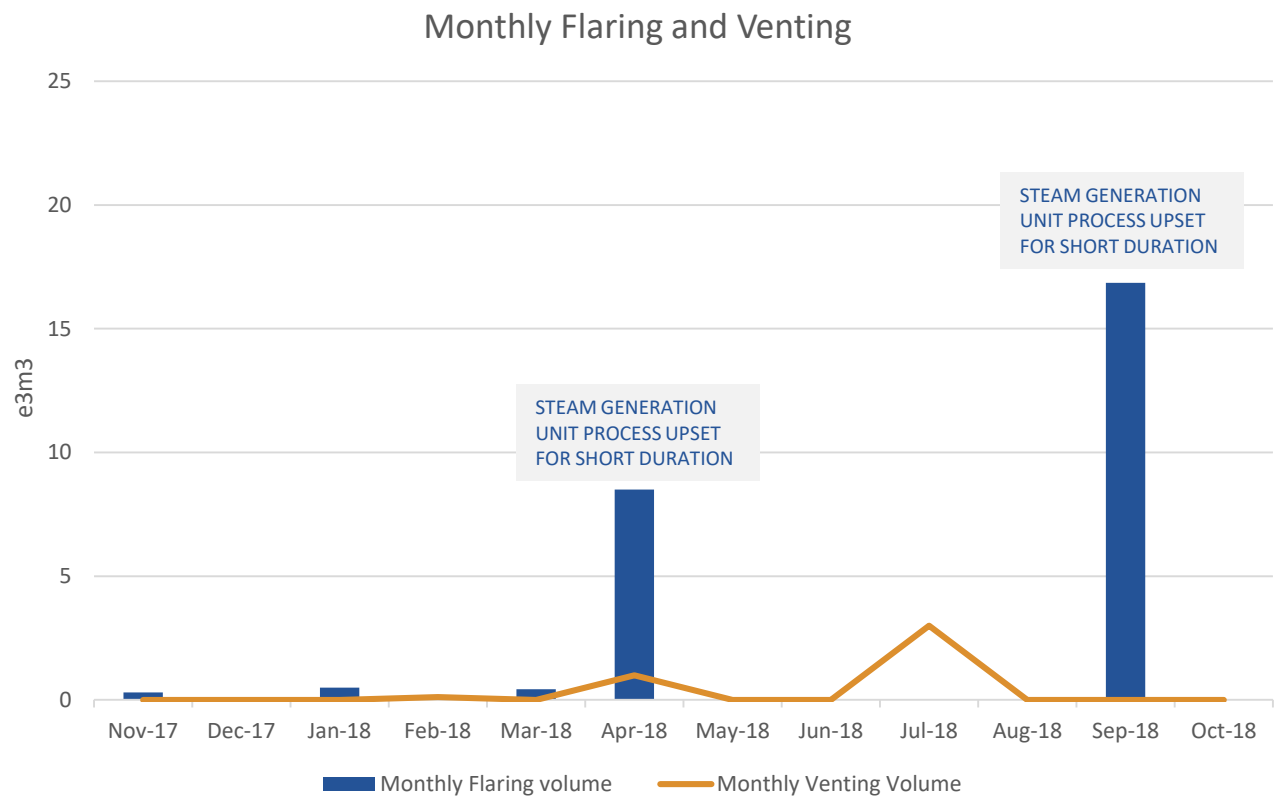


TOTAL GAS USAGE YTD 157,853 e³m³

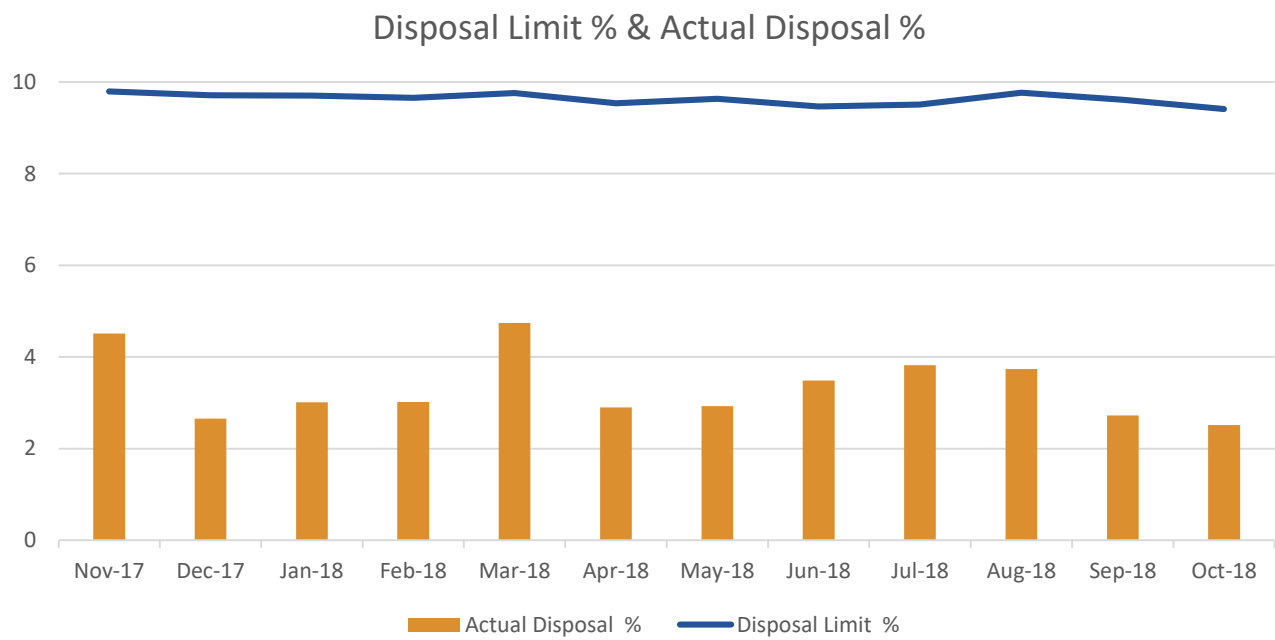
SOLUTION GAS RECOVERY 100%



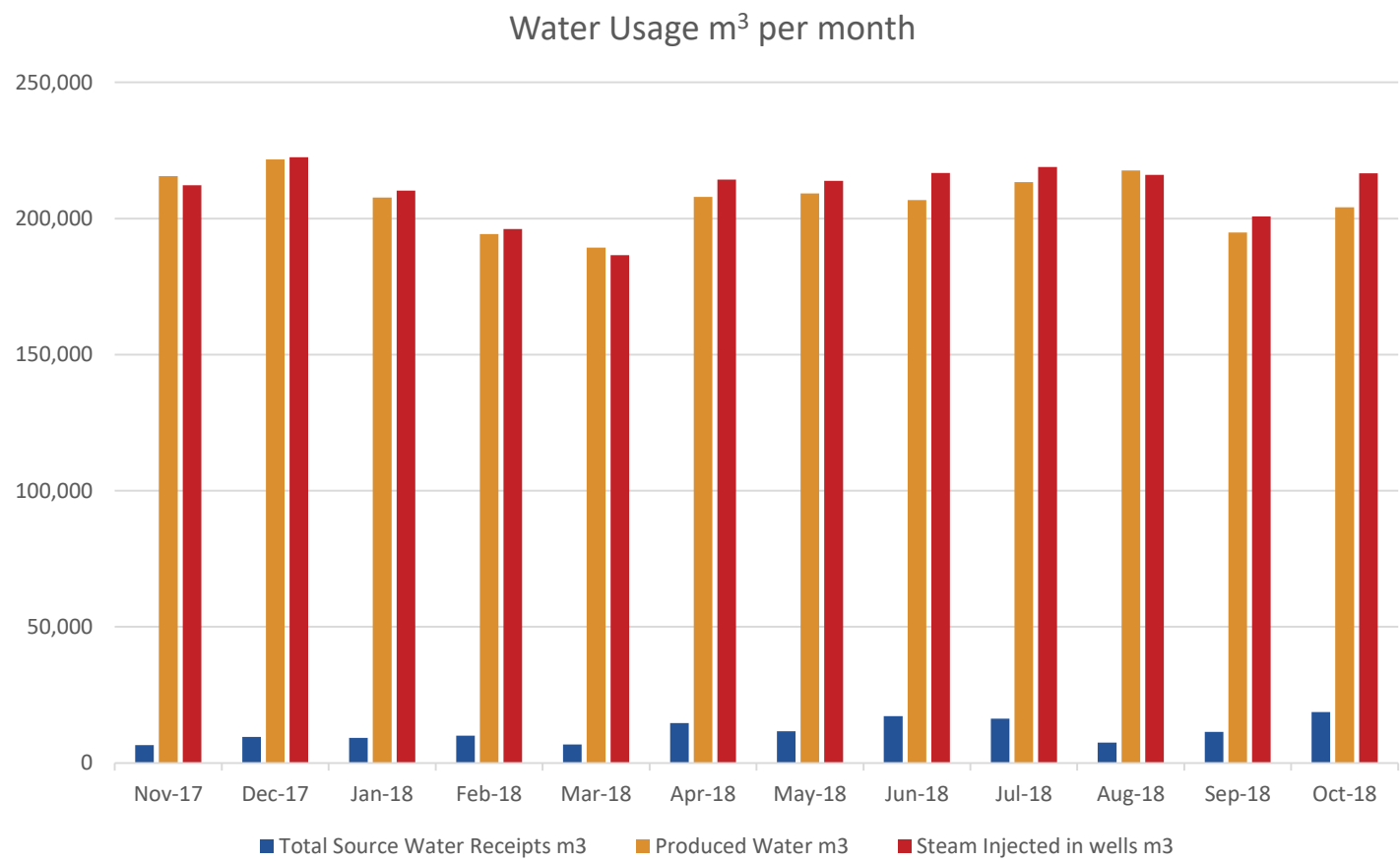
MONTHLY FLARING AND VENTING



- Disposal limit calculated as per Directive 081



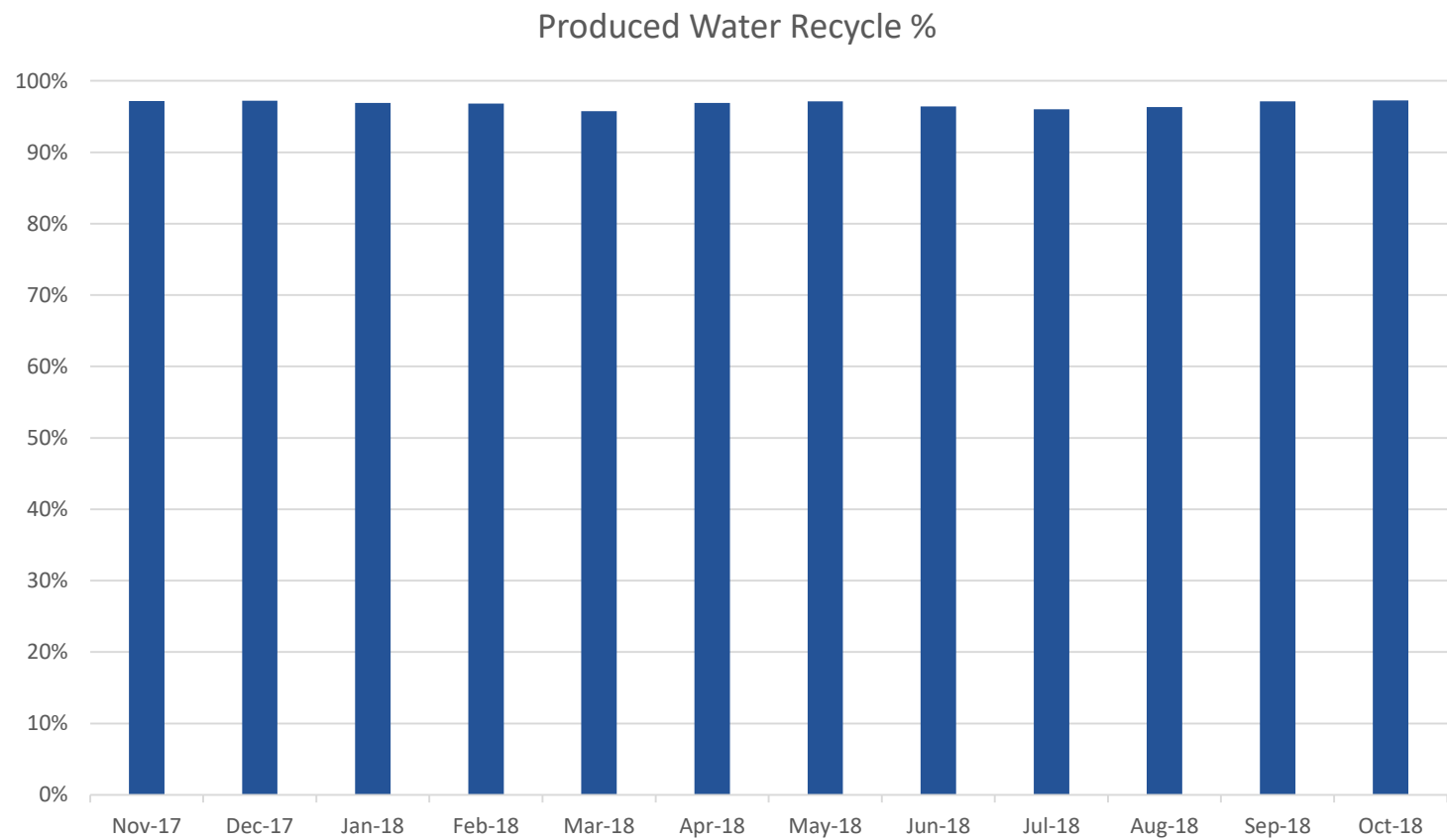
WATER USAGE



PRODUCED WATER RECYCLE (AVG. 97%)

Directive 081 , Appendix H, Equation 6

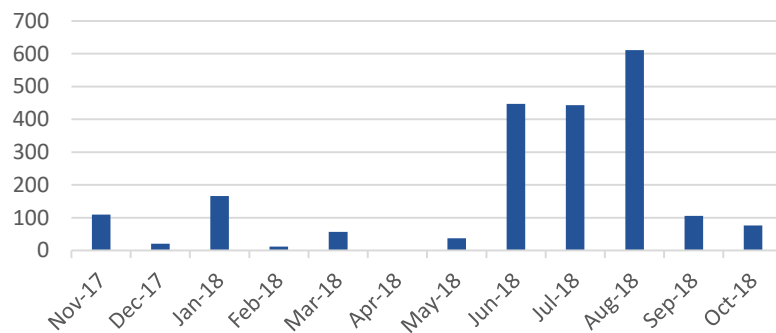
Produced Water Recycle improved by 1%



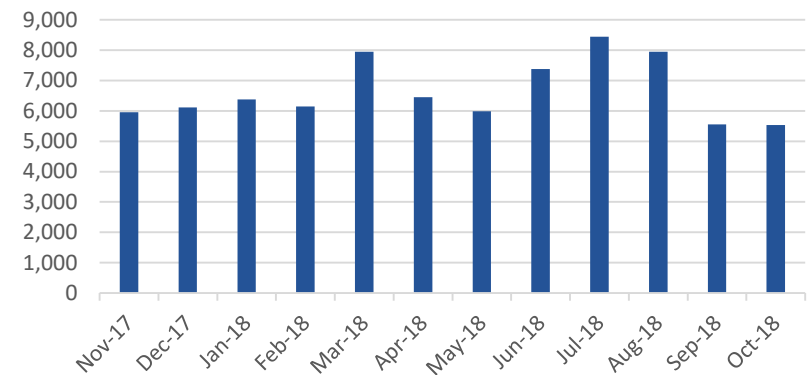
WASTE DISPOSAL

- Waste streams are slop oil, evaporator blowdown and excess produced water
- Evap. Waste disposal volume reduced by 8,908 m³
- Slop oil disposal volume reduced by 3,737 m³

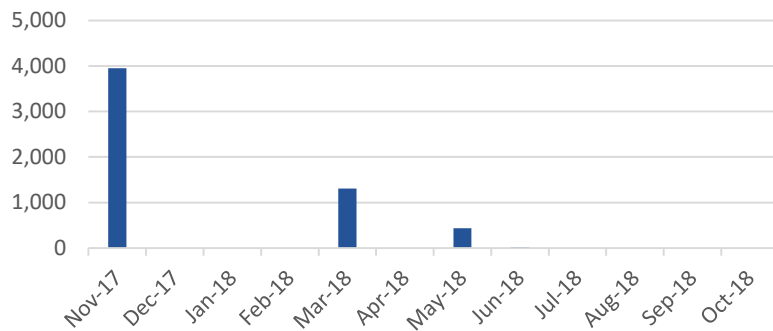
Slop Oil Trucked (m³)



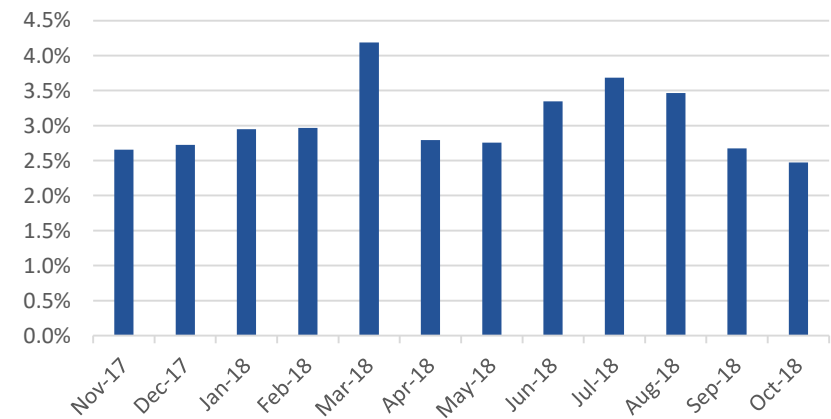
Evap. Waste Trucked (m³)



Excess Produced Water Trucked (m³)

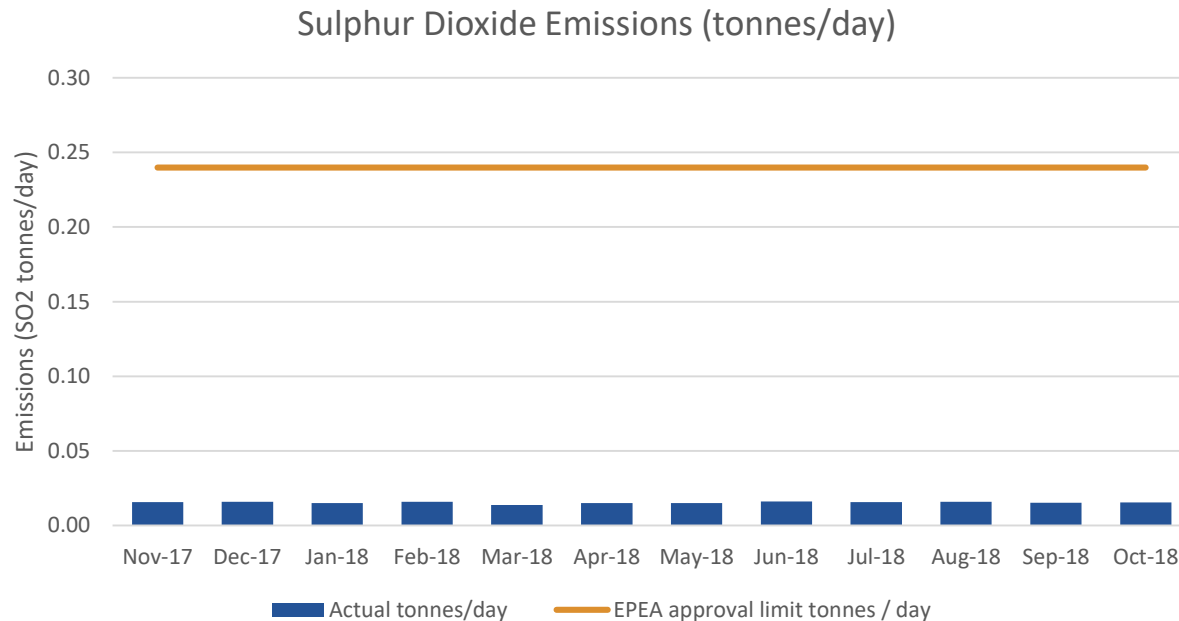


Evap blow-down %



SULPHUR PRODUCTION

- Currently there are no sulphur recovery facilities at the Hangingstone Project



- SO₂ emissions are calculated based on analytical results of produced gas samples



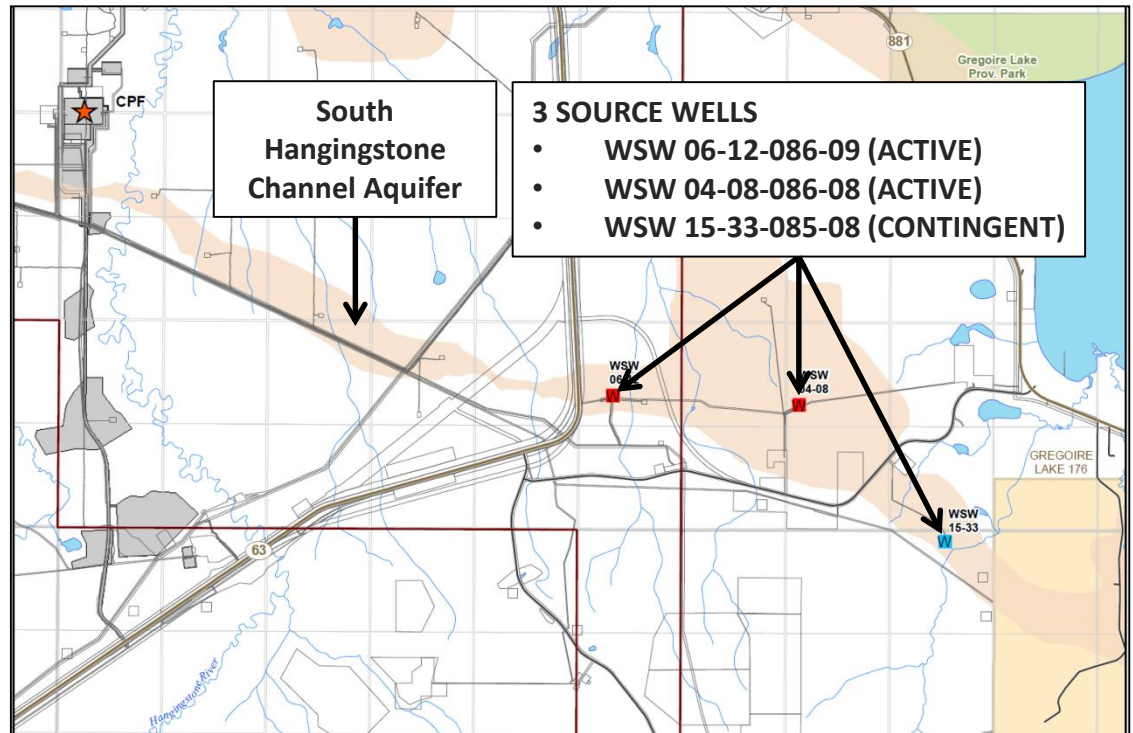
SURFACE

SOURCE WATER AND WATER CHEMISTRY

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NON-SALINE WATER WELLS

- Hangingstone Water Act License 00316166-01-00 annual allocation is 479,975 m³
- During Nov. 1, 2017 to Oct. 31, 2018 AOC diverted 139,671 m³
- Aquifer drawdown is stable and within the allowable as specified in the *Water Conservation and Allocation Guideline for Oilfield Injection* (AENV 2006)



Well ID	Location	Formation	TDS (mg/L)	Maximum Rate of Diversion (m ³ /d)
WSW153308508W400	15-33-085-08-W4	Quaternary	286	3,000
WSW061208609W400	06-12-086-09-W4	Quaternary	310*	3,000
WSW040808608W400	04-08-086-08-W4	Quaternary	320*	3,000

Wells are less than 150 m in depth and not licenced with the AER.

Well IDs are AOC internal identifiers, not UWIs.

* 2018 Analysis

TYPICAL WATER ANALYSIS

Parameter	Non-Saline Make-up Water (mg/L)	Produced Water (mg/L)	Disposal Water (Evap blow-down) (mg/L)
pH	7.97	7.36	11.8
Total Dissolved Solids (TDS)	320	2,300	130,000
Chlorides	7.4	1,200	49,000
Hardness as CaCO ₃	220	14.5	550
Alkalinity as CaCO ₃	270	320	25,000
Silica	5	150	7,000
Total Organic Carbon	<1	180	6,000
Oil Content	<1	20	500



COMPLIANCE
ENVIRONMENTAL

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APPROVALS AND AMENDMENTS

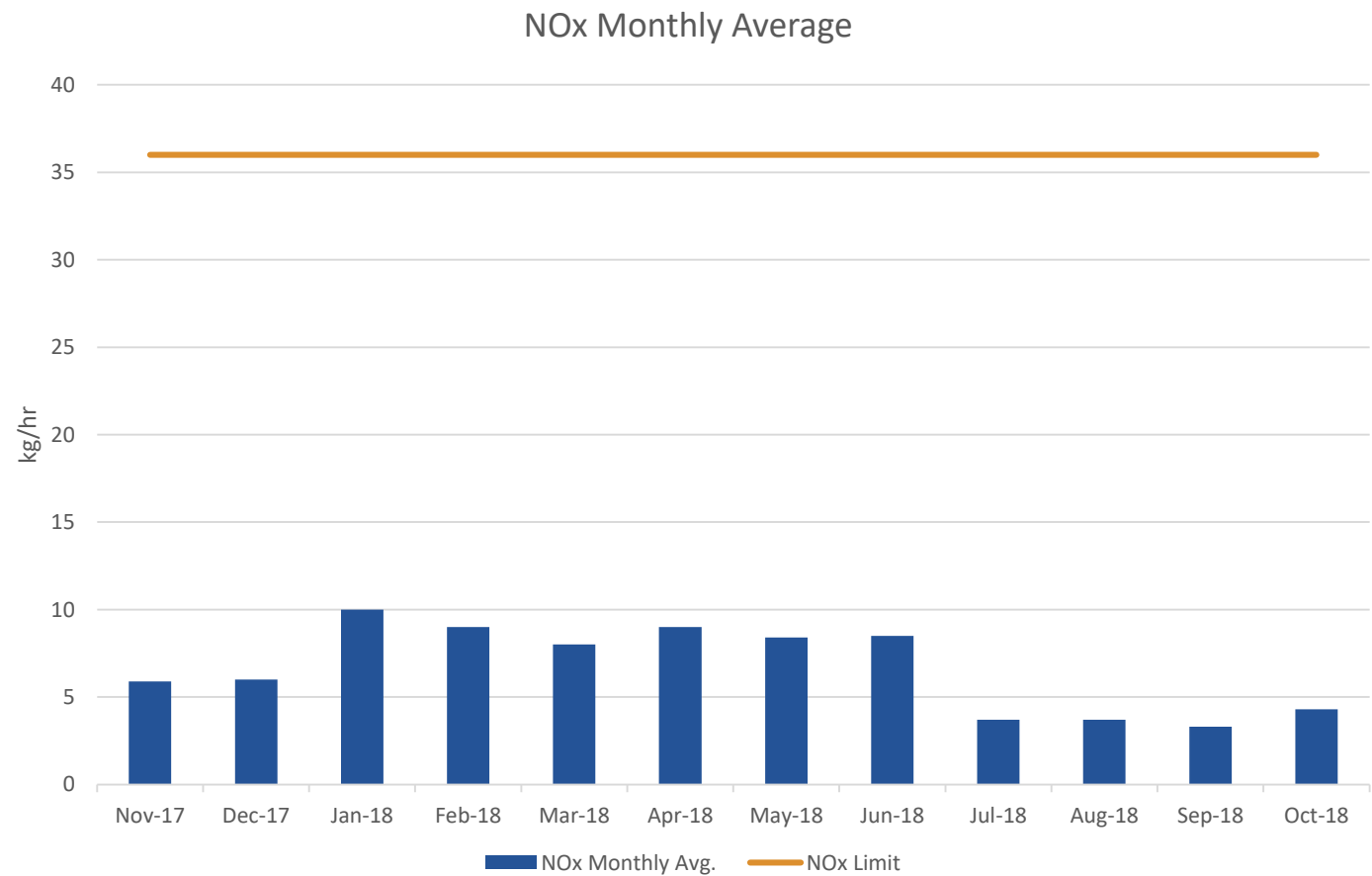
- November 2017, AOC received approval for the short-term exceedance of Maximum Operating Pressure to 2,500 kPag.

MONTHLY AND ANNUAL MONITORING PROGRAMS

- Passive air monitoring stations— no exceedances (SO_2 , NO_2 , H_2S) of the Alberta Ambient Air Quality Objectives
- A continuous air monitoring station **is not** an EPEA approval requirement
- Continuous NO_2 emissions monitored using a Continuous Emissions Monitoring System (CEMS) as required under the EPEA approval (Boiler A)
- SO_2 and NO_2 emissions were summarized in monthly and annual EPEA Air Emissions Reports
- Industrial wastewater and runoff – all releases monitored with no exceedances
- Groundwater water monitoring completed (2 events)
 - *Completed thermal groundwater screening assessment (well pad) new requirement June 2018*
- No soil management or monitoring events were required in the reporting period
- Water Act Licenses (term & surface) all conditions met and reporting completed

NO_x MONTHLY AVERAGE

- Boiler A NO_x calculated using AER approved Method 4 during CEMS unit repair (July-Nov.)



AUDITS

- AER Compliance Audit for Aboveground Pipeline Wildlife Crossing Directive.
 - *Submitted November 30, 2017*
 - *No further follow-up required*

INSPECTIONS

- AER Inspection of CPF and Pad AD conducted on November 20, 2017
 - *Follow-up action plan submitted January 4, 2018*
 - *Inspection closed out February 3, 2018*

Notices of Non-Compliance and Voluntary Self Disclosures	
Event	Corrective Action
November 26, 2017 - Voluntary Self-Disclosure: MOP Exceedance	Control systems operated as designed, the well was quickly brought into compliance. No further follow-up identified.
January 12, 2018 - Voluntary Self-Disclosure: MOP Exceedance	Root cause investigation resulted in an update to the winter start-up procedure for steam injection. No further follow-up identified.
April 18, 2018 – AER Notice of Non-Compliance: Measurement	AOC responded to the AER May 23, 2018. No further follow-up identified.
August 31, 2018 – CEMS Code violation: unable to meet 90% availability requirement (July to November) (CIC# 343415)	CEMS analyzer was removed for repair and the reinstallation completed in 2018. Method 4 proposal to address interim data management and reporting was approved by the AER.

From November 1, 2017 to October 31, 2018 there were

- 3 reportable spills and
- 4 reportable venting occurrences.

- Completed off disposition reclamation work in response to the 2016 Ft. McMurray wildfire (Temporary Field Authorization 17382)
- OSE reclamation assessment work is ongoing



AOC IS A FUNDING MEMBER OF:

- Oil Sands Environmental Monitoring Program
- Wood Buffalo Environmental Association (WBEA) – air shed monitoring
- Regional Industry Caribou Collaboration (RICC)
- Oil Sands Black Bear Partnership
- Faster Forests – reclamation research industry collaboration
- Industrial Footprint Reduction Options Group (iFROG) – wetland reclamation research industry collaboration

AOC PARTICIPATES IN:

- Various regional CAPP Committees
 - *Oil Sands Environmental Policy and Regulatory Committee*
 - *NE Alberta Caribou Working Group*
 - *Indigenous Affairs Committee*
 - *Air Issues Committee*



ATHABASCA OIL CORPORATION HANGINGSTONE PROJECT IS IN COMPLIANCE WITH AER APPROVALS AND REGULATORY REQUIREMENTS

- For the period of November 1, 2017 to October 31, 2018, AOC has no unaddressed non-compliant events

-
- No new initiatives planned

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